

STORMWATER REPORT

Definitive Subdivision Old Cart Path Lane Ext. (70 Old Cart Path Lane) Pembroke, Massachusetts

Prepared for:

Stephen Saia 70 Old Cart Path Lane Pembroke, MA 02359

January 7, 2020

SUMMARY

This Stormwater Report has been prepared to document compliance with Stormwater Management Standards. The applicant is proposing to subdivide the existing 6.2 acre parcel into 4 lots including a 24-foot wide road and cul-de-sac with sidewalk on both sides.

A drainage system consisting of catch basin and manholes is proposed for the roadway. The closed drainage system discharges to sediment forebays and infiltration basins to the northwest and southeast of the proposed development. The infiltration basin is designed to fully infiltrate the 2 and 10 year storms. Outlet control structures are proposed to reduce peak flows during the 25 and 100 year storms and to provide emergency overflow.

The design as proposed reduces peak runoff rates, improves and promotes infiltration, improves stormwater quality and treatment.

This analysis is divided into the following sections:

- Section ICompliance with Massachusetts Stormwater Management RegulationsSection IIOverall Site Analysis
- Section III Operation and Maintenance Plan

The calculations have been performed for the 2, 10, and 25, 100-year 24 hour storm event, using HydroCAD 10.00 Stormwater Modeling computer program. This computer program is based upon the TR-55 computer models and uses the SCS Curvilinear Unit rainfall distribution. The closed drainage system calculation were performed using the HydroCAD Stormwater Modeling program.

SUMMARY OF STORMWATER FLOWS (cfs)

		Westerly flow towards Northwest Wetland				
Design Storm	l	Existing Condition	Proposed Condition			
e		(Subcat 3)	14L(Subcat 5-9)	W. Surf El. Infil Basin		
2-year	3.4"	0.01	0.00	65.33		
10-year	4.7"	0.09	0.07	66.07		
25-year	5.5"	0.43	0.27	66.72		
100-year	7.0"	1.43	1.13	67.15		
-						
		Westerly flow towards	Southwest We	tland		
Design Storm	L	Existing Condition	Existing Condition Proposed Condition			
C		4L(Subcat 1-2)	12L(Subcat 1-4, 10)	W. Surf El. Infil Basin		
2-year	3.4"	0.08	0.01	64.69		
10-year	4.7"	0.75	0.10	65.82		
25-year	5.5"	1.68	0.93	65.96		
100-year	7.0"	3.89	3.50	66.17		

Infiltration Basin #1 (11P)

			Infiltration Rate = 2.41 in/hr			
Design Storn	n	Max El. (ft)	Storage (cf)	Peak Inflow	Peak Exfiltration	
2-year	3.4"	64.69	1,240	0.88	0.11	
10-year	4.7"	65.82	3,790	1.76	0.14	
25-year	5.5"	65.96	4,157	2.63	0.15	
100-year	7.0"	66.17	4,750	4.27	0.16	

			Infiltration Rate	e = 2.41 in/hr		
Design Storm	ı	Max El. (ft)	Max El. (ft) Storage (cf) Peak In		Peak Exfiltration	
2-year	3.4"	65.33	587	0.49	0.14	
10-year	4.7"	66.07	2,675	1.43	0.17	
25-year	5.5"	66.72	4,826	2.30	0.20	
100-year	7.0"	67.15	6,420	3.83	0.21	

Section I

Compliance with Massachusetts Stormwater Management Regulations



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

A. Introduction

Important: When filling out forms on the computer, use only the tab key to move your cursor - do not use the return key



A Stormwater Report must be submitted with the Notice of Intent permit application to document compliance with the Stormwater Management Standards. The following checklist is NOT a substitute for the Stormwater Report (which should provide more substantive and detailed information) but is offered here as a tool to help the applicant organize their Stormwater Management documentation for their Report and for the reviewer to assess this information in a consistent format. As noted in the Checklist, the Stormwater Report must contain the engineering computations and supporting information set forth in Volume 3 of the Massachusetts Stormwater Handbook. The Stormwater Report must be prepared and certified by a Registered Professional Engineer (RPE) licensed in the Commonwealth.

The Stormwater Report must include:

- The Stormwater Checklist completed and stamped by a Registered Professional Engineer (see page 2) that certifies that the Stormwater Report contains all required submittals.¹ This Checklist is to be used as the cover for the completed Stormwater Report.
- Applicant/Project Name
- Project Address
- Name of Firm and Registered Professional Engineer that prepared the Report
- Long-Term Pollution Prevention Plan required by Standards 4-6
- Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan required by Standard 8²
- Operation and Maintenance Plan required by Standard 9

In addition to all plans and supporting information, the Stormwater Report must include a brief narrative describing stormwater management practices, including environmentally sensitive site design and LID techniques, along with a diagram depicting runoff through the proposed BMP treatment train. Plans are required to show existing and proposed conditions, identify all wetland resource areas, NRCS soil types, critical areas, Land Uses with Higher Potential Pollutant Loads (LUHPPL), and any areas on the site where infiltration rate is greater than 2.4 inches per hour. The Plans shall identify the drainage areas for both existing and proposed conditions at a scale that enables verification of supporting calculations.

As noted in the Checklist, the Stormwater Management Report shall document compliance with each of the Stormwater Management Standards as provided in the Massachusetts Stormwater Handbook. The soils evaluation and calculations shall be done using the methodologies set forth in Volume 3 of the Massachusetts Stormwater Handbook.

To ensure that the Stormwater Report is complete, applicants are required to fill in the Stormwater Report Checklist by checking the box to indicate that the specified information has been included in the Stormwater Report. If any of the information specified in the checklist has not been submitted, the applicant must provide an explanation. The completed Stormwater Report Checklist and Certification must be submitted with the Stormwater Report.

¹ The Stormwater Report may also include the Illicit Discharge Compliance Statement required by Standard 10. If not included in the Stormwater Report, the Illicit Discharge Compliance Statement must be submitted prior to the discharge of stormwater runoff to the post-construction best management practices.

² For some complex projects, it may not be possible to include the Construction Period Erosion and Sedimentation Control Plan in the Stormwater Report. In that event, the issuing authority has the discretion to issue an Order of Conditions that approves the project and includes a condition requiring the proponent to submit the Construction Period Erosion and Sedimentation Control Plan before commencing any land disturbance activity on the site.



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

B. Stormwater Checklist and Certification

The following checklist is intended to serve as a guide for applicants as to the elements that ordinarily need to be addressed in a complete Stormwater Report. The checklist is also intended to provide conservation commissions and other reviewing authorities with a summary of the components necessary for a comprehensive Stormwater Report that addresses the ten Stormwater Standards.

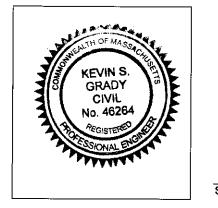
Note: Because stormwater requirements vary from project to project, it is possible that a complete Stormwater Report may not include information on some of the subjects specified in the Checklist. If it is determined that a specific item does not apply to the project under review, please note that the item is not applicable (N.A.) and provide the reasons for that determination.

A complete checklist must include the Certification set forth below signed by the Registered Professional Engineer who prepared the Stormwater Report.

Registered Professional Engineer's Certification

I have reviewed the Stormwater Report, including the soil evaluation, computations, Long-term Pollution Prevention Plan, the Construction Period Erosion and Sedimentation Control Plan (if included), the Longterm Post-Construction Operation and Maintenance Plan, the Illicit Discharge Compliance Statement (if included) and the plans showing the stormwater management system, and have determined that they have been prepared in accordance with the requirements of the Stormwater Management Standards as further elaborated by the Massachusetts Stormwater Handbook. I have also determined that the information presented in the Stormwater Checklist is accurate and that the information presented in the Stormwater Report accurately reflects conditions at the site as of the date of this permit application.

Registered Professional Engineer Block and Signature



Signature and Date

Checklist

Project Type: Is the application for new development, redevelopment, or a mix of new and redevelopment?

New development

Redevelopment

Mix of New Development and Redevelopment



LID Measures: Stormwater Standards require LID measures to be considered. Document what environmentally sensitive design and LID Techniques were considered during the planning and design of the project:

\boxtimes	No disturbance to any Wetland Resource Areas
	Site Design Practices (e.g. clustered development, reduced frontage setbacks)
	Reduced Impervious Area (Redevelopment Only)
\boxtimes	Minimizing disturbance to existing trees and shrubs
	LID Site Design Credit Requested:
	Credit 1
	Credit 2
	Credit 3
	Use of "country drainage" versus curb and gutter conveyance and pipe
	Bioretention Cells (includes Rain Gardens)
	Constructed Stormwater Wetlands (includes Gravel Wetlands designs)
	Treebox Filter
	Water Quality Swale
	Grass Channel
	Green Roof
	Other (describe):

Standard 1: No New Untreated Discharges

- No new untreated discharges
- \boxtimes Outlets have been designed so there is no erosion or scour to wetlands and waters of the Commonwealth
- Supporting calculations specified in Volume 3 of the Massachusetts Stormwater Handbook included.



Standard 2: Peak Rate Attenuation

- Standard 2 waiver requested because the project is located in land subject to coastal storm flowage and stormwater discharge is to a wetland subject to coastal flooding.
- Evaluation provided to determine whether off-site flooding increases during the 100-year 24-hour storm.

Calculations provided to show that post-development peak discharge rates do not exceed predevelopment rates for the 2-year and 10-year 24-hour storms. If evaluation shows that off-site flooding increases during the 100-year 24-hour storm, calculations are also provided to show that post-development peak discharge rates do not exceed pre-development rates for the 100-year 24hour storm.

Standard 3: Recharge

Soil Analysis provided.

- Required Recharge Volume calculation provided.
- Required Recharge volume reduced through use of the LID site Design Credits.
- Sizing the infiltration, BMPs is based on the following method: Check the method used.

\boxtimes	Static
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Dynamic Field¹

Runoff from all impervious areas at the site discharging to the infiltration BMP.

Simple Dynamic

Runoff from all impervious areas at the site is *not* discharging to the infiltration BMP and calculations are provided showing that the drainage area contributing runoff to the infiltration BMPs is sufficient to generate the required recharge volume.

\boxtimes	Recharge BMPs have	e been sized to	infiltrate the	Required I	Recharge \	/olume.

Recharge BMPs have been sized to infiltrate the Required Recharge Volume only to the maximum
extent practicable for the following reason:

- Site is comprised solely of C and D soils and/or bedrock at the land surface
- M.G.L. c. 21E sites pursuant to 310 CMR 40.0000
- Solid Waste Landfill pursuant to 310 CMR 19.000
- Project is otherwise subject to Stormwater Management Standards only to the maximum extent practicable.
- Calculations showing that the infiltration BMPs will drain in 72 hours are provided.

Property	/ includes a	a M.G.L. c.	21E site or	a solid v	waste landf	fill and a i	moundina a	analvsis i	s included.

¹ 80% TSS removal is required prior to discharge to infiltration BMP if Dynamic Field method is used.



Standard 3: Recharge (continued)

- The infiltration BMP is used to attenuate peak flows during storms greater than or equal to the 10year 24-hour storm and separation to seasonal high groundwater is less than 4 feet and a mounding analysis is provided.
- Documentation is provided showing that infiltration BMPs do not adversely impact nearby wetland resource areas.

Standard 4: Water Quality

The Long-Term Pollution Prevention Plan typically includes the following:

- Good housekeeping practices;
- · Provisions for storing materials and waste products inside or under cover;
- Vehicle washing controls;
- Requirements for routine inspections and maintenance of stormwater BMPs;
- Spill prevention and response plans;
- Provisions for maintenance of lawns, gardens, and other landscaped areas;
- Requirements for storage and use of fertilizers, herbicides, and pesticides;
- Pet waste management provisions;
- Provisions for operation and management of septic systems;
- Provisions for solid waste management;
- Snow disposal and plowing plans relative to Wetland Resource Areas;
- Winter Road Salt and/or Sand Use and Storage restrictions;
- Street sweeping schedules;
- Provisions for prevention of illicit discharges to the stormwater management system;
- Documentation that Stormwater BMPs are designed to provide for shutdown and containment in the event of a spill or discharges to or near critical areas or from LUHPPL;
- Training for staff or personnel involved with implementing Long-Term Pollution Prevention Plan;
- List of Emergency contacts for implementing Long-Term Pollution Prevention Plan.
- A Long-Term Pollution Prevention Plan is attached to Stormwater Report and is included as an attachment to the Wetlands Notice of Intent.
- Treatment BMPs subject to the 44% TSS removal pretreatment requirement and the one inch rule for calculating the water quality volume are included, and discharge:
 - is within the Zone II or Interim Wellhead Protection Area
 - is near or to other critical areas
 - is within soils with a rapid infiltration rate (greater than 2.4 inches per hour)
 - involves runoff from land uses with higher potential pollutant loads.
- The Required Water Quality Volume is reduced through use of the LID site Design Credits.
- Calculations documenting that the treatment train meets the 80% TSS removal requirement and, if applicable, the 44% TSS removal pretreatment requirement, are provided.



Massachusetts Department of Environmental Protection Bureau of Resource Protection - Wetlands Program Checklist for Stormwater Report

Standard 4: Water Quality (continued)
The BMP is sized (and calculations provided) based on:
The $\frac{1}{2}$ " or 1" Water Quality Volume or
The equivalent flow rate associated with the Water Quality Volume and documentation is provided showing that the BMP treats the required water quality volume.
☐ The applicant proposes to use proprietary BMPs, and documentation supporting use of proprietary BMP and proposed TSS removal rate is provided. This documentation may be in the form of the propriety BMP checklist found in Volume 2, Chapter 4 of the Massachusetts Stormwater Handbook and submitting copies of the TARP Report, STEP Report, and/or other third party studies verifying performance of the proprietary BMPs.
A TMDL exists that indicates a need to reduce pollutants other than TSS and documentation showing that the BMPs selected are consistent with the TMDL is provided.
Standard 5: Land Uses With Higher Potential Pollutant Loads (LUHPPLs)
 The NPDES Multi-Sector General Permit covers the land use and the Stormwater Pollution Prevention Plan (SWPPP) has been included with the Stormwater Report. The NPDES Multi-Sector General Permit covers the land use and the SWPPP will be submitted <i>prior</i> <i>to</i> the discharge of stormwater to the post-construction stormwater BMPs.
☐ The NPDES Multi-Sector General Permit does <i>not</i> cover the land use.
□ LUHPPLs are located at the site and industry specific source control and pollution prevention measures have been proposed to reduce or eliminate the exposure of LUHPPLs to rain, snow, snow melt and runoff, and been included in the long term Pollution Prevention Plan.
All exposure has been eliminated.
All exposure has <i>not</i> been eliminated and all BMPs selected are on MassDEP LUHPPL list.
The LUHPPL has the potential to generate runoff with moderate to higher concentrations of oil and grease (e.g. all parking lots with >1000 vehicle trips per day) and the treatment train includes an oil grit separator, a filtering bioretention area, a sand filter or equivalent.
Standard 6: Critical Areas
The discharge is near or to a critical area and the treatment train includes only BMPs that MassDEP has approved for stormwater discharges to or near that particular class of critical area.
Critical areas and BMPs are identified in the Stormwater Report.



Standard 7: Redevelopments and Other Projects Subject to the Standards only to the maximum extent practicable

The project is subject to the Stormwater Management Standards only to the maximum Extent Practicable as a:

Limited Project	
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- Small Residential Projects: 5-9 single family houses or 5-9 units in a multi-family development provided there is no discharge that may potentially affect a critical area.
- Small Residential Projects: 2-4 single family houses or 2-4 units in a multi-family development with a discharge to a critical area
- Marina and/or boatyard provided the hull painting, service and maintenance areas are protected from exposure to rain, snow, snow melt and runoff
- Bike Path and/or Foot Path
- Redevelopment Project
- Redevelopment portion of mix of new and redevelopment.
- Certain standards are not fully met (Standard No. 1, 8, 9, and 10 must always be fully met) and an explanation of why these standards are not met is contained in the Stormwater Report.

☐ The project involves redevelopment and a description of all measures that have been taken to improve existing conditions is provided in the Stormwater Report. The redevelopment checklist found in Volume 2 Chapter 3 of the Massachusetts Stormwater Handbook may be used to document that the proposed stormwater management system (a) complies with Standards 2, 3 and the pretreatment and structural BMP requirements of Standards 4-6 to the maximum extent practicable and (b) improves existing conditions.

Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan must include the following information:

- Narrative;
- Construction Period Operation and Maintenance Plan;
- Names of Persons or Entity Responsible for Plan Compliance;
- Construction Period Pollution Prevention Measures;
- Erosion and Sedimentation Control Plan Drawings;
- Detail drawings and specifications for erosion control BMPs, including sizing calculations;
- Vegetation Planning;
- Site Development Plan;
- Construction Sequencing Plan;
- Sequencing of Erosion and Sedimentation Controls;
- Operation and Maintenance of Erosion and Sedimentation Controls;
- Inspection Schedule;
- Maintenance Schedule;
- Inspection and Maintenance Log Form.

A Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan containing the information set forth above has been included in the Stormwater Report.



Standard 8: Construction Period Pollution Prevention and Erosion and Sedimentation Control (continued)

- ☐ The project is highly complex and information is included in the Stormwater Report that explains why it is not possible to submit the Construction Period Pollution Prevention and Erosion and Sedimentation Control Plan with the application. A Construction Period Pollution Prevention and Erosion and Sedimentation Control has *not* been included in the Stormwater Report but will be submitted *before* land disturbance begins.
- The project is *not* covered by a NPDES Construction General Permit.
- The project is covered by a NPDES Construction General Permit and a copy of the SWPPP is in the Stormwater Report.
- The project is covered by a NPDES Construction General Permit but no SWPPP been submitted. The SWPPP will be submitted BEFORE land disturbance begins.

Standard 9: Operation and Maintenance Plan

- The Post Construction Operation and Maintenance Plan is included in the Stormwater Report and includes the following information:
 - Name of the stormwater management system owners;
 - Party responsible for operation and maintenance;
 - Schedule for implementation of routine and non-routine maintenance tasks;
 - Plan showing the location of all stormwater BMPs maintenance access areas;
 - Description and delineation of public safety features;
 - Estimated operation and maintenance budget; and
 - Operation and Maintenance Log Form.
- The responsible party is *not* the owner of the parcel where the BMP is located and the Stormwater Report includes the following submissions:
 - A copy of the legal instrument (deed, homeowner's association, utility trust or other legal entity) that establishes the terms of and legal responsibility for the operation and maintenance of the project site stormwater BMPs;
 - A plan and easement deed that allows site access for the legal entity to operate and maintain BMP functions.

Standard 10: Prohibition of Illicit Discharges

- The Long-Term Pollution Prevention Plan includes measures to prevent illicit discharges;
- An Illicit Discharge Compliance Statement is attached;
- NO Illicit Discharge Compliance Statement is attached but will be submitted *prior to* the discharge of any stormwater to post-construction BMPs.

STANDARD 1. NO NEW STORMWATER CONVEYANCES

The proposed development proposes no new stormwater conveyances that discharge untreated stormwater off-site or cause down gradient erosion.

STANDARD 2. PEAK RATE ATTENUATION

The overall site analysis demonstrates that the stormwater management system has been designed so that the post-development peak discharge rates do not exceed the pre-development discharge rate.

STANDARD 3. STORMWATER RECHARGE

Test holes were excavated on site October 5, 2017. Based on Plymouth County Soil Survey, the consist of Hydrologic Soils Group "Type A", loamy sand for the majority of the site. Test holes performed on site showed the soil textual analysis consistent with the soils survey and an infiltration rate of 2.41 in/hr was used for the analysis.

TABLE 1 REQUIRED RECHARGE VOLUME AND DRAWDOWN

Impervious Area = 43,184 SF Target Depth Factor (F) = 0.6"

Rv = *F x impervious area* = 0.6"x 43,184 SF x 1'/12"= 2,159 CF

Total Required Recharge

=2,159 CF

Proposed: Infiltration Basin #1(10 Year Infiltration) = 3,790 CFInfiltration Basin #2(25 Year Infiltration) = 4,826 CFTotal = 8,616 CF

Drawdown Within 72 Hours

 $Time_{drawdown} = \frac{Rv}{(K)(Bottom \ Area)}$

Where:

Rv = *Storage Volume*

K = Saturated Hydraulic Conductivity For "Static" and "Simple Dynamic" Methods, use Rawls Rate (see Table 2.3.3). For "Dynamic Field" Method, use 50% of the in-situ saturated hydraulic conductivity. Bottom Area = Bottom Area of Recharge Structure

Basin #1

Time =
$$\frac{4,670 \text{ CF}}{(2.41"/\text{hr})(1'/12")(1,612 \text{ SF})}$$
 = 14.4 hours < 72 hours

Basin #2

Time = $\frac{6,383 \text{ CF}}{(2.41"/\text{hr})(1'/12")(2,410 \text{ SF})}$

13.2 hours < 72 hours

Mounding Analysis

"Mounding analysis is required when the vertical separation from the bottom of an exfiltration system to seasonal high groundwater is less than four (4) feet and the recharge system is proposed to attenuate the peak discharge from a 10-year or higher 24-hour storm (e.g., 10year, 25-year, 50-year, or 100-year 24-hour storm). In such cases, the mounding analysis must demonstrate that the Required Recharge Volume (e.g., infiltration basin storage) is fully dewatered within 72 hours (so the next storm can be stored for exfiltration). The mounding analysis must also show that the groundwater mound that forms under the recharge system will not break out above the land or water surface of a wetland (e.g., it doesn't increase the water sheet elevation in a Bordering Vegetated Wetland, Salt Marsh, or Land Under Water within the 72-hour evaluation period)."

=

"The Hantush¹ or other equivalent method may be used to conduct the mounding analysis. The Hantush method predicts the maximum height of the groundwater mound beneath a rectangular or circular recharge area. It assumes unconfined groundwater flow, and that a linear relation exists between the water table elevation and water table decline rate. It results in a water table recession hydrograph depicting exponential decline. The Hantush method is available in proprietary software and free on-line calculators on the Web in automated format. If the analysis indicates the mound will prevent the infiltration BMP from fully draining within the 72-hour period, an iterative process must be employed to determine an alternative design that drains within the 72-hour period."

This mounding will not interfere with dewatering within 72 hours or result in break out above the land or water surface of a wetland.

See Mounding Analysis sheets

¹ Hantush 1967 – See Reference for Standard 3.

This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0), height of the water table if the bottom of the aguifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

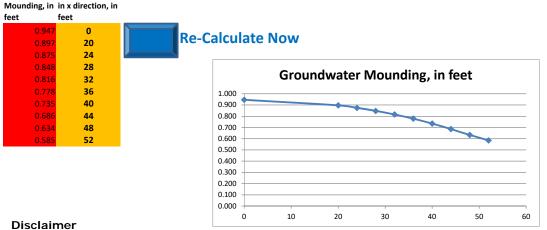
Cells highlighted in yellow are values that can be changed by the user. Cells highlighted in red are output values based on user-specified inputs. The user MUST click the blue "Re-Calculate Now" button each time ANY of the user-specified inputs are changed otherwise necessary iterations to converge on the correct solution will not be done and values shown will be incorrect. Use consistent units for all input values (for example, feet and days)

use consistent units (e.g. feet & days **or** inches & hours)

		use consistent units (e.g. reet & days of inches & nours)	Conver	SION TADIE	
Input Values			inch/ho	our feet/o	day
0.9970	R	Recharge (infiltration) rate (feet/day)		0.67	1.33
0.200	Sy	Specific yield, Sy (dimensionless, between 0 and 1)			
32.00	к	Horizontal hydraulic conductivity, Kh (feet/day)*		2.00	4.00 In the report accompanying this spreadsheet
45.000	x	1/2 length of basin (x direction, in feet)			(USGS SIR 2010-5102), vertical soil permeability
27.000	У	1/2 width of basin (y direction, in feet)	hours	days	(ft/d) is assumed to be one-tenth horizontal
1.000	t	duration of infiltration period (days)		36	1.50 hydraulic conductivity (ft/d).
40.000	hi(0)	initial thickness of saturated zone (feet)			

Conversion Table

maximum thickness of saturated zone (beneath center of basin at end of infiltration period) maximum groundwater mounding (beneath center of basin at end of infiltration period)



h(max)

Δh(max)

Distance from center of basin

40.94 0.94

Ground-

water

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

Basin 2

This spreadsheet will calculate the height of a groundwater mound beneath a stormwater infiltration basin. More information can be found in the U.S. Geological Survey Scientific Investigations Report 2010-5102 "Simulation of groundwater mounding beneath hypothetical stormwater infiltration basins".

The user must specify infiltration rate (R), specific yield (Sy), horizontal hydraulic conductivity (Kh), basin dimensions (x, y), duration of infiltration period (t), and the initial thickness of the saturated zone (hi(0), height of the water table if the bottom of the aguifer is the datum). For a square basin the half width equals the half length (x = y). For a rectangular basin, if the user wants the water-table changes perpendicular to the long side, specify x as the short dimension and y as the long dimension. Conversely, if the user wants the values perpendicular to the short side, specify y as the short dimension, x as the long dimension. All distances are from the center of the basin. Users can change the distances from the center of the basin at which water-table aquifer thickness are calculated.

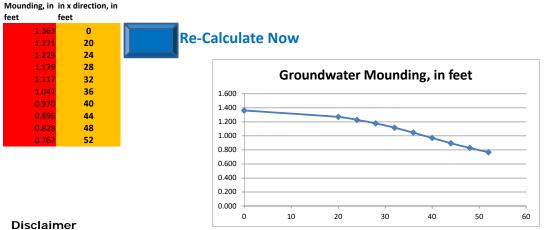
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use consistent units (e.g. feet & days **or** inches & hours)

			use consistent units (e.g. reet & days of inches & nours)	conver	SIOII TADIE	
Ir	nput Values			inch/ho	our feet	t/day
	1.5600	R	Recharge (infiltration) rate (feet/day)		0.67	1.33
	0.200	Sy	Specific yield, Sy (dimensionless, between 0 and 1)			
	32.00	к	Horizontal hydraulic conductivity, Kh (feet/day)*		2.00	4.00 In the report accompanying this spreadsheet
	38.000	x	1/2 length of basin (x direction, in feet)			(USGS SIR 2010-5102), vertical soil permeability
	28.000	У	1/2 width of basin (y direction, in feet)	hours	day	/s (ft/d) is assumed to be one-tenth horizontal
	1.000	t	duration of infiltration period (days)		36	1.50 hydraulic conductivity (ft/d).
	40.000	hi(0)	initial thickness of saturated zone (feet)			

Conversion Table

maximum thickness of saturated zone (beneath center of basin at end of infiltration period) maximum groundwater mounding (beneath center of basin at end of infiltration period)



h(max)

Δh(max)

Distance from center of basin

41.363 1.363

Ground-

water

This spreadsheet solving the Hantush (1967) equation for ground-water mounding beneath an infiltration basin is made available to the general public as a convenience for those wishing to replicate values documented in the USGS Scientific Investigations Report 2010-5102 "Groundwater mounding beneath hypothetical stormwater infiltration basins" or to calculate values based on user-specified site conditions. Any changes made to the spreadsheet (other than values identified as user-specified) after transmission from the USGS could have unintended, undesirable consequences. These consequences could include, but may not be limited to: erroneous output, numerical instabilities, and violations of underlying assumptions that are inherent in results presented in the accompanying USGS published report. The USGS assumes no responsibility for the consequences of any changes made to the spreadsheet. If changes are made to the spreadsheet, the user is responsible for documenting the changes and justifying the results and conclusions.

STANDARD 4. WATER QUALITY

TSS Removal

The proposed work meets the requirement for removal of total suspended solids (TSS). See TSS Removal Worksheet

Long-Term Pollution Prevention Plan

The long-term pollution prevention plan will be combined with the Operation and Maintenance Plan required by Standard 9.

WATER QUALITY TREATMENT VOLUME

- $V_{WQ} = (D_{WQ}/12 \text{ inches/foot}) * (A_{IMP} * 43,560 \text{ square feet/acre})$
- *VwQ* = *Required Water Quality Volume* (in cubic feet)
- D_{WQ} = Water Quality Depth: one-inch for discharges within a Zone II or Interim Wellhead Protection Area, to or near another critical area, runoff from a LUHPPL, or exfiltration to soils with infiltration rate greater than 2.4 inches/hour or greater; ¹/₂-inch for discharges near or to other areas.
- A_{IMP} = Impervious Area (in acres)
- The site is located in soils with an infiltration rate greater than 2.4 inches/hour so a Water Quality Depth of one-inch is required.
- $V_{WQ} = (1 \text{ inch}/12 \text{ inches}/\text{foot}) * (43,184 \text{ square feet}) = 3,598 \text{ CF}$

3,741 CF storage volume provided in the infiltration basin #1 below the drainage system outlet.

5,832 CF storage volume provided in the infiltration basin #2 below the drainage system outlet.

INSTRUCTIONS: 1. In BMP Column, click on Blue Cell to Activate Drop Down Menu 2. Select BMP from Drop Down Menu 3. Atter BMP is selected, TSS Removal and other Columns are automatically completed.

							1	누
	F Domoinion	Load (D-E)	0.75	0.36	0.07			Separate Form Needs to be Completed for Each Outlet or BMP Train
	A B C E	Removed (C*D)	0.25	0.39	0.29			93%
	D Stortion TSS	Juaning 199 Load*	1.00	0.75	0.36			Total TSS Removal =
Location: Infiltration Basins 1 & 2	C TSS Domoval	Rate ¹	0.25	0.52	0.80			
Location:	Ш	BMP ¹	Deep Sump and Hooded Catch Basin	Stormceptor	Infiltration Basin			
			sheet I		nəЯ V no		_	

*Equals remaining load from previous BMP (E) which enters the BMP

Prepared By: Grady Consulting LLC

Date: 11/19/2019

Project: 70 Old Cart Path Lane

Version 1, Automated: Mar. 4, 2008

STANDARD 5 LAND USES WITH HIGHER POTENTIAL POLLUTANT LOADS

The land use is not considered a higher potential pollutant load.

STANDARD 6. CRITICAL AREAS

The land use is not located within a critical area.

STANDARD 7. REDEVELOPMENT PROJECT

"A redevelopment project is required to meet the following Stormwater Management Standards only to the maximum extent practicable: Standard 2, Standard 3, and the pretreatment and structural stormwater best management practice requirements of Standards 4, 5, and 6. Existing stormwater discharges shall comply with Standard 1 only to the maximum extent practicable. A redevelopment project shall also comply with all other requirements of the Stormwater Management Standards and improve existing conditions."

The project is not a redevelopment project.

STANDARD 8. CONSTRUCTION PERIOD CONTROLS

A plan to control construction-related impacts, including erosion, sedimentation, and other pollutant sources during construction and land disturbance activities (construction period erosion, sedimentation, and pollution prevention plan) shall be developed and implemented.

The proposed project will disturb more than one acre of land and is required to obtain coverage under the NPDES Construction General Permit issued by EPA and prepare a Stormwater Pollution Plan (see attached O&M Plan during construction)

STANDARD 9. LONG-TERM OPERATION AND MAINTENANCE (O&M) PLAN

A Long -Term Operation and Maintenance (O&M) Plan shall be developed and implemented to ensure that stormwater management systems function as designed.

The Long-Term Operation and Maintenance Plan shall at a minimum include:

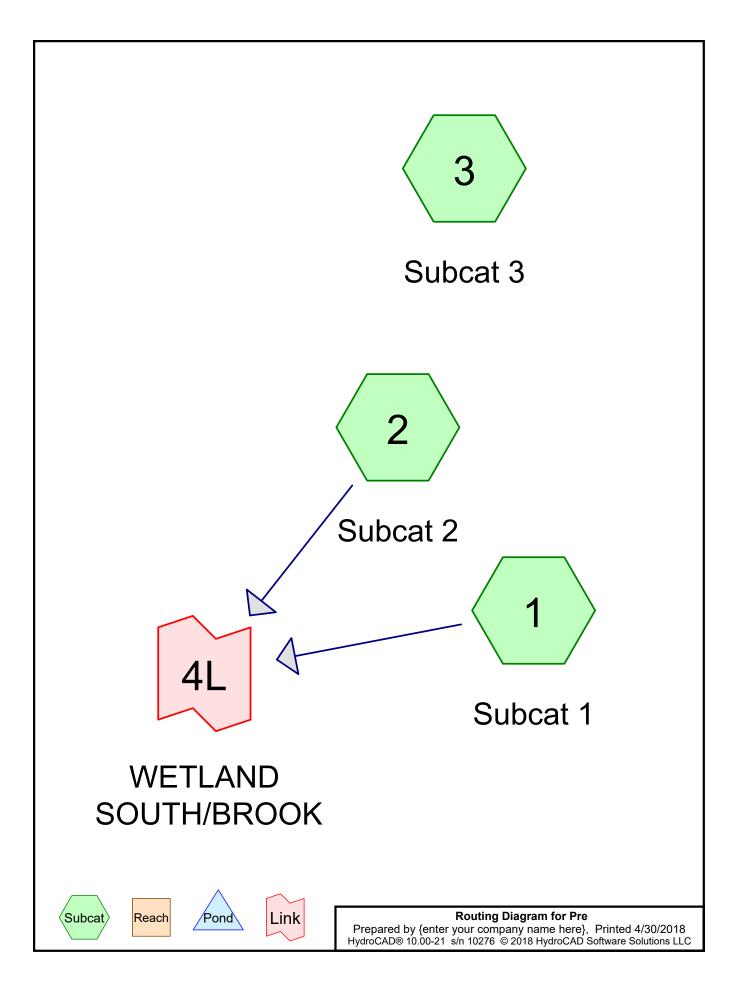
- 1. Stormwater management system(s) owners;
- 2. The party or parties responsible for operation and maintenance, including how future property owners will be notified of the presence of the stormwater management system and the requirement for proper operation and maintenance;
- 3. The routine and non-routine maintenance tasks to be undertaken after construction is complete and a schedule for implementing those tasks;
- 4. A plan that is drawn to scale and shows the location of all stormwater BMPs in each treatment train along with the discharge point;
- 5. A description and delineation of public safety features; and
- 6. An estimated operations and maintenance budget.

STANDARD 10. ILLICIT DISCHARGES PROHIBITED

"All illicit discharges to the stormwater management system are prohibited."

Section II

Overall Site Analysis



Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
115,198	49	50-75% Grass cover, Fair, HSG A (1, 2, 3)
13,030	98	Paved roads w/curbs & sewers, HSG A (1, 2, 3)
3,485	98	Roofs, HSG A (1, 2, 3)
186,876	36	Woods, Fair, HSG A (1, 2, 3)
318,589	44	TOTAL AREA

Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
318,589	HSG A	1, 2, 3
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
318,589		TOTAL AREA

		Ground		oucs		
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
 (sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
115,198	0	0	0	0	115,198	50-75% Grass cover, Fair
13,030	0	0	0	0	13,030	Paved roads w/curbs & sewers
3,485	0	0	0	0	3,485	Roofs
186,876	0	0	0	0	186,876	Woods, Fair
318,589	0	0	0	0	318,589	TOTAL AREA

Ground Covers (all nodes)

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=42,391 sf 12.55% Impervious Runoff Depth>0.22" Flow Length=368' Tc=8.5 min CN=52 Runoff=0.08 cfs 788 cf
Subcatchment2: Subcat2	Runoff Area=122,920 sf 7.11% Impervious Runoff Depth>0.09" Flow Length=500' Tc=14.9 min CN=46 Runoff=0.03 cfs 876 cf
Subcatchment3: Subcat3	Runoff Area=153,278 sf 1.60% Impervious Runoff Depth>0.01" Flow Length=585' Tc=18.6 min CN=40 Runoff=0.01 cfs 127 cf
Link 4L: WETLAND SOUTH/BROOK	Inflow=0.08 cfs 1,664 cf Primary=0.08 cfs 1,664 cf

Total Runoff Area = 318,589 sfRunoff Volume = 1,791 cfAverage Runoff Depth = 0.07"94.82% Pervious = 302,073 sf5.18% Impervious = 16,515 sf

Summary for Subcatchment 1: Subcat 1

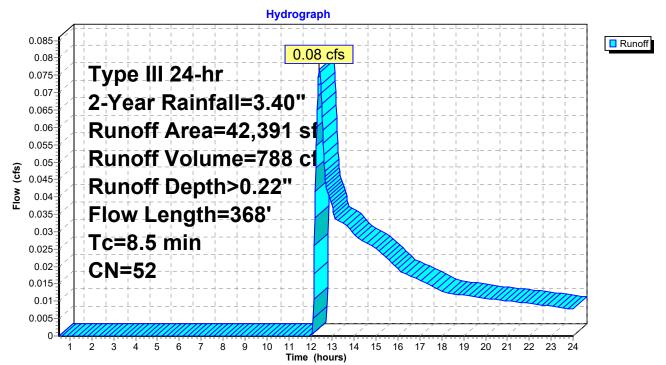
Runoff = 0.08 cfs @ 12.41 hrs, Volume= 788 cf, Depth> 0.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN E	Description					
		28,260	49 5	9 50-75% Grass cover, Fair, HSG A					
		5,097	98 F	Paved roads w/curbs & sewers, HSG A					
		222		Roofs, HSG A					
_		8,811	<u>36</u> V	Voods, Fai	r, HSG A				
		42,391		Veighted A	0				
		37,071	-		vious Area				
		5,319	1	2.55% Imp	pervious Ar	ea			
	Та	Longth	Clana	Valacity	Consoitu	Description			
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description			
_	. /	(166()							
	60	/		/	(015)	Chaot Flow			
	6.9	50	0.0500	0.12	(013)	Sheet Flow, Grass: Dense, n= 0.240, P2= 2.20"			
		50	0.0500	0.12	(015)	Grass: Dense n= 0.240 P2= 2.20"			
	6.9 0.6			/	(015)	Grass: Dense n= 0.240 P2= 2.20" Shallow Concentrated Flow,			
	0.6	50 144	0.0500 0.0530	0.12 3.71	(013)	Grass: Dense n= 0.240 P2= 2.20" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
		50	0.0500	0.12	(015)	Grass: Dense n= 0.240 P2= 2.20" Shallow Concentrated Flow,			

8.5 368 Total

Subcatchment 1: Subcat 1



Summary for Subcatchment 2: Subcat 2

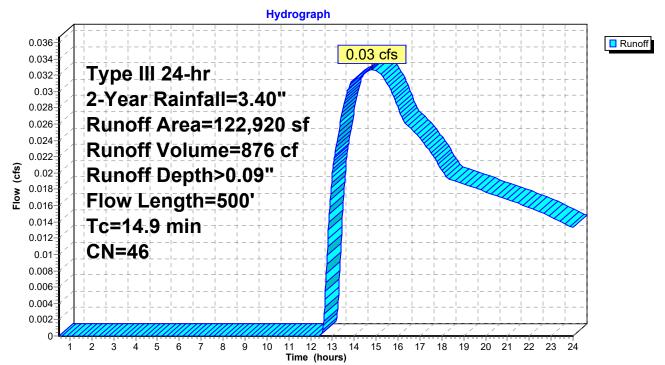
Runoff = 0.03 cfs @ 14.82 hrs, Volume= 876 cf, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN E	Description					
		54,860	49 5	0-75% Gra	ass cover, F	Fair, HSG A			
		7,011	98 F	aved road	s w/curbs &	& sewers, HSG A			
		1,732	98 F	3 Roofs, HSG A					
_		59,317	17 36 Woods, Fair, HSG A						
	1	22,920		Veighted A					
	1	14,177	-		vious Area				
		8,743	7	′.11% Impe	ervious Are	а			
	т.	1	0	\/.l!t.	0	Description			
	Tc (min)	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)				
	12.6	50	0.0300	0.07		Sheet Flow,			
	0.0	4 4 0	0 0000	0.70		Woods: Light underbrush n= 0.400 P2= 2.20"			
	0.9	143	0.0300	2.79		Shallow Concentrated Flow,			
	4 4	207	0.0520	0.74		Unpaved Kv= 16.1 fps			
	1.4	307	0.0530	3.71		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
_	44.0	500	T ()			Ulipaved NV-10.1 lps			

14.9 500 Total

Subcatchment 2: Subcat 2



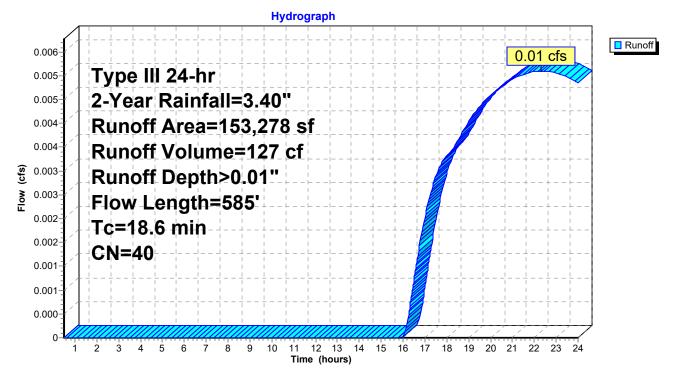
Summary for Subcatchment 3: Subcat 3

Runoff = 0.01 cfs @ 22.30 hrs, Volume= 127 cf, Depth> 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

A	rea (sf)	CN E	Description					
	32,078	49 50-75% Grass cover, Fair, HSG A						
	923	98 F	Paved road	s w/curbs &	& sewers, HSG A			
	1,530	98 F	Roofs, HSG	βA				
1	18,747	36 V	Voods, Fai	r, HSG A				
1	53,278	40 V	Veighted A	verage				
1	50,825	ç	98.40% Pei	vious Area				
	2,453	1	.60% Impe	ervious Area	а			
Tc	Length	Slope	Velocity	Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
14.9	50	0.0200	0.06		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.20"			
0.9	171	0.0350	3.01		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
2.6	291	0.0130	1.84		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
0.2	73	0.1920	7.05		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
18.6	585	Total						

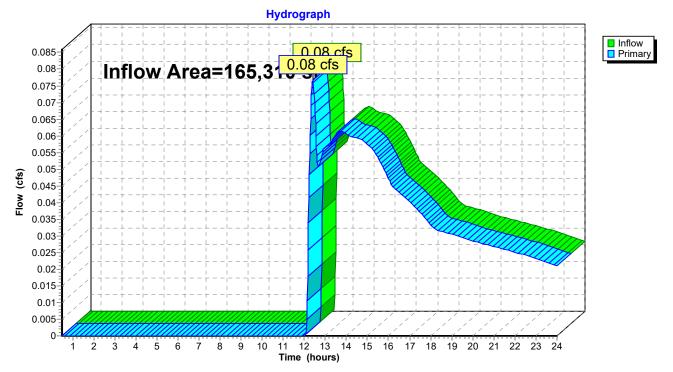
Subcatchment 3: Subcat 3



Summary for Link 4L: WETLAND SOUTH/BROOK

Inflow Are	a =	165,310 sf,	8.51% Impervious,	Inflow Depth >	0.12"	for 2-Year event
Inflow	=	0.08 cfs @ 1	12.41 hrs, Volume=	1,664 cf		
Primary	=	0.08 cfs @ 1	12.41 hrs, Volume=	1,664 cf	, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 4L: WETLAND SOUTH/BROOK

Pre	Type III 24-hr	10-Year Rainfall=4.70"
Prepared by {enter your company name here}		Printed 4/30/2018
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solutio	ns LLC	Page 11

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=42,391 sf 12.55% Impervious Runoff Depth>0.67" Flow Length=368' Tc=8.5 min CN=52 Runoff=0.45 cfs 2,374 cf
Subcatchment2: Subcat2	Runoff Area=122,920 sf 7.11% Impervious Runoff Depth>0.39" Flow Length=500' Tc=14.9 min CN=46 Runoff=0.44 cfs 3,994 cf
Subcatchment 3: Subcat 3	Runoff Area=153,278 sf 1.60% Impervious Runoff Depth>0.17" Flow Length=585' Tc=18.6 min CN=40 Runoff=0.09 cfs 2,183 cf
Link 4L: WETLAND SOUTH/BROOK	Inflow=0.75 cfs 6,367 cf Primary=0.75 cfs 6,367 cf

Total Runoff Area = 318,589 sf Runoff Volume = 8,550 cfAverage Runoff Depth = 0.32"94.82% Pervious = 302,073 sf5.18% Impervious = 16,515 sf

Summary for Subcatchment 1: Subcat 1

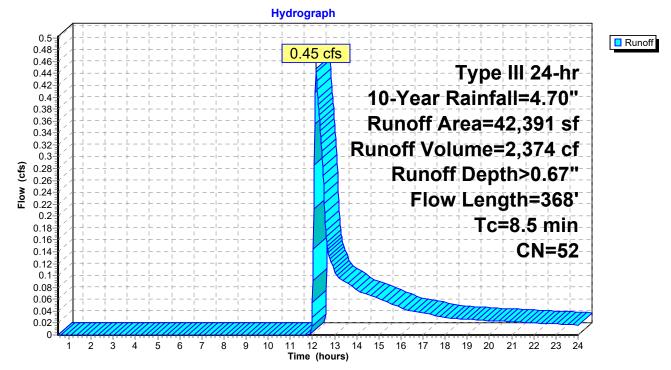
Runoff = 0.45 cfs @ 12.16 hrs, Volume= 2,374 cf, Depth> 0.67"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	A	rea (sf)	CN	Description						
		28,260	49	9 50-75% Grass cover, Fair, HSG A						
		5,097	98	Paved road	s w/curbs &	& sewers, HSG A				
		222		Roofs, HSG						
_		8,811	36	Woods, Fai	r, HSG A					
		42,391		Weighted A						
		37,071		87.45% Per						
		5,319		12.55% Imp	pervious Ar	ea				
	Та	l e ve extle	Clana	Valasity	Consolity	Description				
	Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
-	· /				(015)	Chaot Flow				
	6.9	50	0.0500	0.12		Sheet Flow, Grass: Dense n= 0.240 P2= 2.20"				
	0.6	144	0.0530	3.71		Shallow Concentrated Flow,				
	0.0	144	0.0000	5.71		Unpaved Kv= 16.1 fps				
	1.0	174	0.0300	2.79		Shallow Concentrated Flow,				
	1.0	174	0.0000	2.10		Unpaved Kv= 16.1 fps				
-	0.5	200	Tatal			• · · p · · · · · · · · · · · · · · · ·				

8.5 368 Total

Subcatchment 1: Subcat 1



Summary for Subcatchment 2: Subcat 2

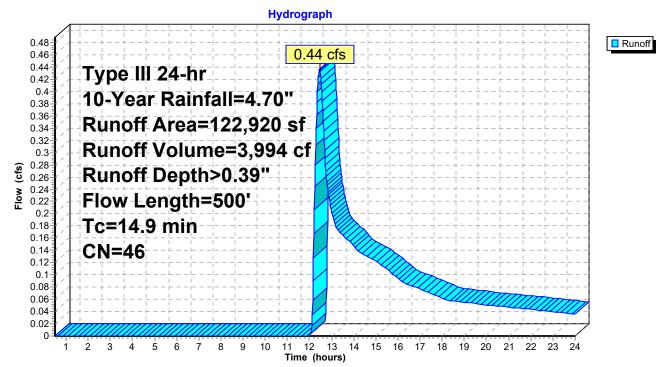
Runoff = 0.44 cfs @ 12.46 hrs, Volume= 3,994 cf, Depth> 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	A	rea (sf)	CN E	Description					
		54,860 49 50-75% Grass cover, Fair, HSG A							
	7,011 98 Paved roads w/curbs & sewers, HSG A								
		1,732 98 Roofs, HSG A							
59,317 36 Woods, Fair, HSG A									
	1	22,920		Weighted Average					
	114,177 92.89% Pervious Ar								
8,743 7.11% Impervious Area									
	т.	1	0	\/.l!t.	0	Description			
	Tc (min)	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	<u>(ft/ft)</u>	(ft/sec)	(cfs)				
	12.6	50	0.0300	0.07		Sheet Flow,			
	0.0	4 4 0	0 0000	0.70		Woods: Light underbrush n= 0.400 P2= 2.20"			
	0.9	143	0.0300	2.79		Shallow Concentrated Flow,			
	4 4	207	0.0520	0.74		Unpaved Kv= 16.1 fps			
	1.4	307	0.0530	3.71		Shallow Concentrated Flow, Unpaved Kv= 16.1 fps			
_	44.0	500	T ()			Ulipaved NV-10.1 lps			

14.9 500 Total

Subcatchment 2: Subcat 2

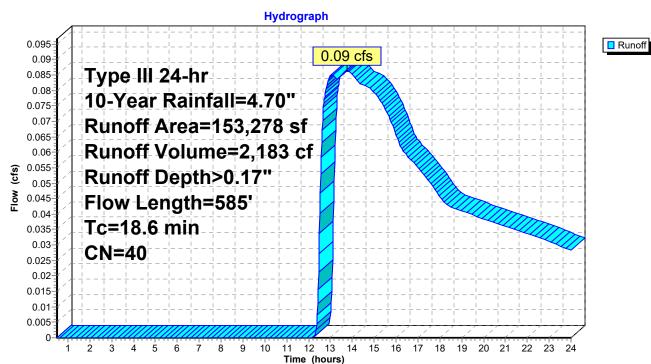


Summary for Subcatchment 3: Subcat 3

Runoff = 0.09 cfs @ 13.78 hrs, Volume= 2,183 cf, Depth> 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN E	Description							
	32,078	8 49 50-75% Grass cover, Fair, HSG A								
	923	98 F	Paved roads w/curbs & sewers, HSG A							
	1,530	98 F	Roofs, HSG A							
1	18,747	747 36 Woods, Fair, HSG A								
153,278 40 Weighted Average										
1	50,825	ç	98.40% Pervious Area							
2,453 1.60% Impervious Area										
Tc	Length	Slope	Velocity	Capacity	Description					
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
14.9	50	0.0200	0.06		Sheet Flow,					
					Woods: Light underbrush n= 0.400 P2= 2.20"					
0.9	171	0.0350	3.01		Shallow Concentrated Flow,					
					Unpaved Kv= 16.1 fps					
2.6	291	0.0130	1.84		Shallow Concentrated Flow,					
					Unpaved Kv= 16.1 fps					
0.2	73	0.1920	7.05		Shallow Concentrated Flow,					
					Unpaved Kv= 16.1 fps					
18.6	585	Total								

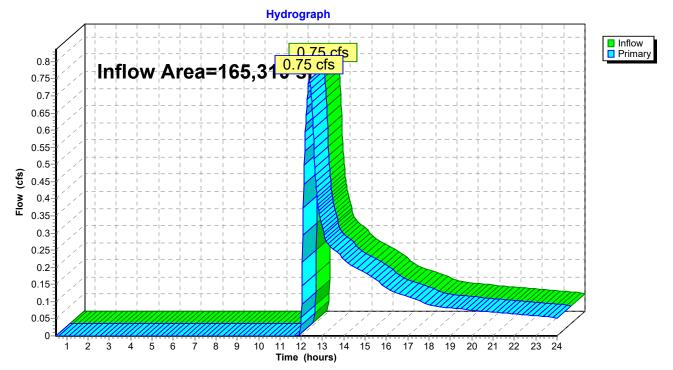


Subcatchment 3: Subcat 3

Summary for Link 4L: WETLAND SOUTH/BROOK

Inflow Area	a =	165,310 sf,	8.51% Impervious,	Inflow Depth >	0.46" for	10-Year event
Inflow	=	0.75 cfs @ 1	12.39 hrs, Volume=	6,367 cf		
Primary	=	0.75 cfs @ 1	12.39 hrs, Volume=	6,367 cf	, Atten= 0	%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 4L: WETLAND SOUTH/BROOK

Pre	Type III 24-hr 25-Year Rainfall=5.60"
Prepared by {enter your company name here}	Printed 4/30/2018
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solutio	ns LLC Page 17

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=42,391 sf 12.55% Impervious Runoff Depth>1.08" Flow Length=368' Tc=8.5 min CN=52 Runoff=0.89 cfs 3,823 cf
Subcatchment 2: Subcat 2	Runoff Area=122,920 sf 7.11% Impervious Runoff Depth>0.70" Flow Length=500' Tc=14.9 min CN=46 Runoff=1.04 cfs 7,185 cf
Subcatchment 3: Subcat 3	Runoff Area=153,278 sf 1.60% Impervious Runoff Depth>0.38" Flow Length=585' Tc=18.6 min CN=40 Runoff=0.43 cfs 4,859 cf
Link 4L: WETLAND SOUTH/BROOK	Inflow=1.68 cfs 11,008 cf Primary=1.68 cfs 11,008 cf

Total Runoff Area = 318,589 sf Runoff Volume = 15,867 cfAverage Runoff Depth = 0.60"94.82% Pervious = 302,073 sf5.18% Impervious = 16,515 sf

Summary for Subcatchment 1: Subcat 1

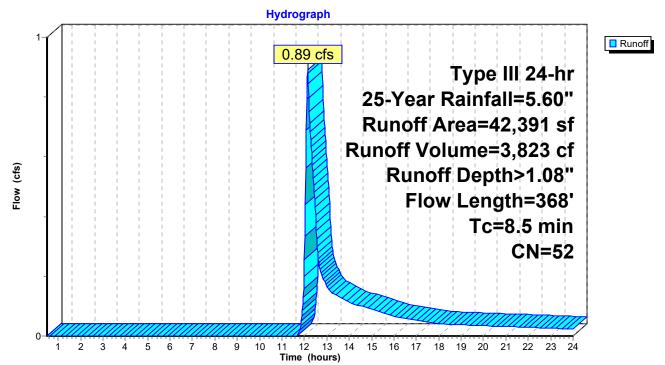
Runoff = 0.89 cfs @ 12.14 hrs, Volume= 3,823 cf, Depth> 1.08"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

A	rea (sf)	CN	Description						
	28,260	49	49 50-75% Grass cover, Fair, HSG A						
	5,097	98							
	222	98	Roofs, HSC	βA					
	8,811	36	36 Woods, Fair, HSG A						
	42,391	52	Weighted A	verage					
	37,071		87.45% Per	vious Area					
	5,319		12.55% Imp	pervious Ar	ea				
Тс	Length	Slop	,	Capacity	Description				
 (min)	(feet)	(ft/f	i) (ft/sec)	(cfs)					
6.9	50	0.050	0.12		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 2.20"				
0.6	144	0.053	0 3.71		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
1.0	174	0.030	0 2.79		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
~ -	~~~	T ()							

8.5 368 Total

Subcatchment 1: Subcat 1



Summary for Subcatchment 2: Subcat 2

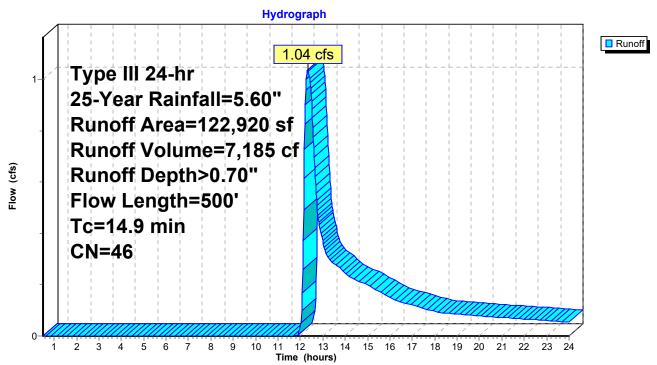
Runoff = 1.04 cfs @ 12.33 hrs, Volume= 7,185 cf, Depth> 0.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

_	A	rea (sf)	CN [Description						
_		54,860	49 5	49 50-75% Grass cover, Fair, HSG A						
		7,011	98 F	Paved road	s w/curbs &	& sewers, HSG A				
		1,732		Roofs, HSC						
_		59,317	<u>36</u> \	Voods, Fai	r, HSG A					
	1	22,920		Veighted A						
	1	14,177	-		vious Area					
		8,743	7	7.11% Impe	ervious Are	а				
	Та	l e re erthe	Clana	Valasity	Consolity	Description				
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
-	<i>ii</i> _ <i>i</i>	· /		· /	(015)	Shoot Flow				
	12.6	50	0.0300	0.07		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.20"				
	0.9	143	0.0300	2.79		Shallow Concentrated Flow,				
	0.9	145	0.0300	2.19		Unpaved Kv= 16.1 fps				
	1.4	307	0.0530	3.71		Shallow Concentrated Flow,				
	1.4	007	0.0000	0.71		Unpaved Kv= 16.1 fps				
-	110	500	Tatal							

14.9 500 Total

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 0.43 cfs @ 12.55 hrs, Volume= 4,859 cf, Depth> 0.38"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

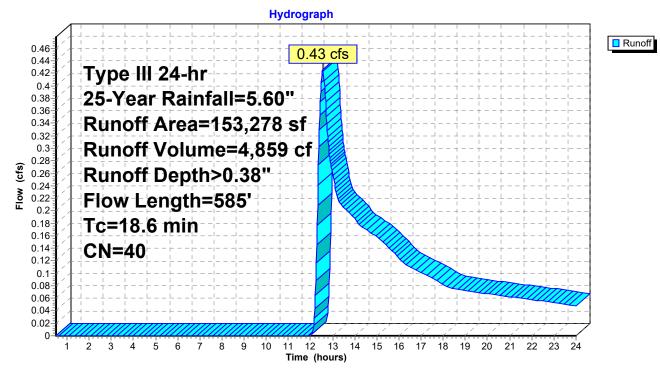
A	rea (sf)	CN E	Description						
	32,078	49 5	49 50-75% Grass cover, Fair, HSG A						
	923	98 F	Paved road	s w/curbs &	& sewers, HSG A				
	1,530	98 F	Roofs, HSG	βA					
1	18,747	36 V	Voods, Fai	r, HSG A					
1	53,278	40 V	Veighted A	verage					
1	50,825	g	8.40% Per	vious Area					
	2,453	1	.60% Impe	ervious Area	а				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
14.9	50	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.20"				
0.9	171	0.0350	3.01		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
2.6	291	0.0130	1.84		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
0.2	73	0.1920	7.05		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
18.6	585	Total							

 Type III 24-hr
 25-Year Rainfall=5.60"

 Printed
 4/30/2018

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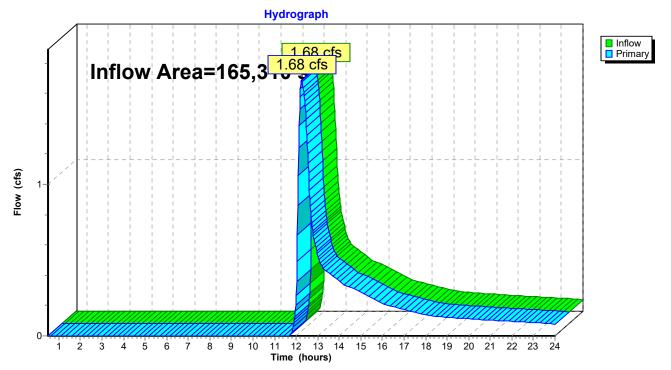




Summary for Link 4L: WETLAND SOUTH/BROOK

Inflow Area	a =	165,310 sf,	8.51% Impervious,	Inflow Depth >	0.80"	for 25-Year event
Inflow	=	1.68 cfs @ 1	12.27 hrs, Volume=	11,008 c	f	
Primary	=	1.68 cfs @ 1	12.27 hrs, Volume=	11,008 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 4L: WETLAND SOUTH/BROOK

Pre Type III 24-hr	100-Year Rainfall=7.00"
Prepared by {enter your company name here}	Printed 4/30/2018
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solutions LLC	Page 23

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=42,391 sf 12.55% Impervious Runoff Depth>1.84" Flow Length=368' Tc=8.5 min CN=52 Runoff=1.73 cfs 6,508 cf
Subcatchment2: Subcat2	Runoff Area=122,920 sf 7.11% Impervious Runoff Depth>1.31" Flow Length=500' Tc=14.9 min CN=46 Runoff=2.56 cfs 13,459 cf
Subcatchment3: Subcat3	Runoff Area=153,278 sf 1.60% Impervious Runoff Depth>0.84" Flow Length=585' Tc=18.6 min CN=40 Runoff=1.43 cfs 10,675 cf
Link 4L: WETLAND SOUTH/BROOK	Inflow=3.89 cfs 19,966 cf Primary=3.89 cfs 19,966 cf

Total Runoff Area = 318,589 sf Runoff Volume = 30,642 cfAverage Runoff Depth = 1.15"94.82% Pervious = 302,073 sf5.18% Impervious = 16,515 sf

Summary for Subcatchment 1: Subcat 1

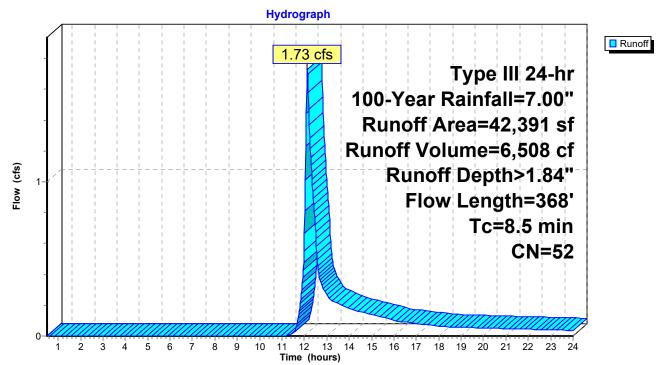
Runoff = 1.73 cfs @ 12.13 hrs, Volume= 6,508 cf, Depth> 1.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

	A	rea (sf)	CN	Description						
		28,260	49	49 50-75% Grass cover, Fair, HSG A						
		5,097	98							
		222	98	·						
_		8,811	36	,						
		42,391	52	Weighted A	verage					
		37,071		87.45% Per	vious Area					
		5,319		ea						
	_				_					
	Tc	Length	Slop		Capacity	Description				
_	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					
	6.9	50	0.050	0 0.12		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 2.20"				
	0.6	144	0.053	0 3.71		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	1.0	174	0.030	0 2.79		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0 5	000	— · ·							

8.5 368 Total

Subcatchment 1: Subcat 1



Summary for Subcatchment 2: Subcat 2

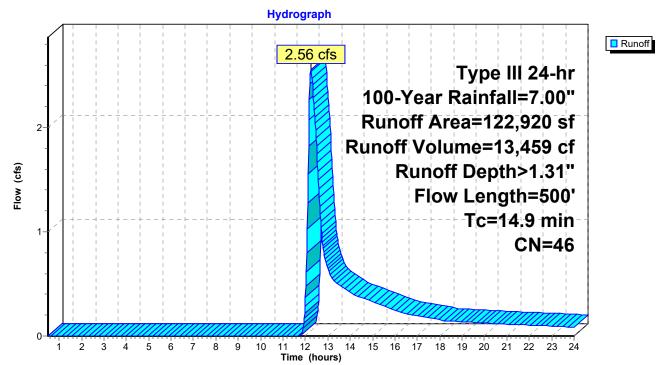
Runoff = 2.56 cfs @ 12.25 hrs, Volume= 13,459 cf, Depth> 1.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

A	rea (sf)	CN [Description						
	54,860	49 5	49 50-75% Grass cover, Fair, HSG A						
	7,011	98 F	98 Paved roads w/curbs & sewers, HSG A						
	1,732	98 F	Roofs, HSG	βA					
	59,317	36 \	Noods, Fai	r, HSG A					
1	22,920								
1	,	ę	92.89% Per	vious Area					
8,743 7.11% Impervious Area				ervious Are	а				
_		-							
	•				Description				
· /	(feet)			(cfs)					
12.6	50	0.0300	0.07		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.20"				
0.9	143	0.0300	2.79		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
1.4	307	0.0530	3.71		Shallow Concentrated Flow,				
		-			Unpaved Kv= 16.1 fps				
	1 1 (min) 12.6 0.9 1.4	1,732 59,317 122,920 114,177 8,743 Tc Length (feet) 12.6 50 0.9 143 1.4 307	54,860 49 54 7,011 98 F 1,732 98 F 59,317 36 N 122,920 46 N 114,177 98 F 8,743 7 7 Tc Length Slope (min) (feet) (ft/ft) 12.6 50 0.0300 0.9 143 0.0300 1.4 307 0.0530	54,860 49 50-75% Graves 7,011 98 Paved road 1,732 98 Roofs, HSG 59,317 36 Woods, Fai 122,920 46 Weighted A 114,177 92.89% Per 8,743 7.11% Imped Tc Length Slope 12.6 50 0.0300 0.07 0.9 143 0.0300 2.79 1.4 307 0.0530 3.71	54,860 49 50-75% Grass cover, I 7,011 98 Paved roads w/curbs 8 1,732 98 Roofs, HSG A 59,317 36 Woods, Fair, HSG A 122,920 46 Weighted Average 114,177 92.89% Pervious Area 8,743 7.11% Impervious Area 7.11% Impervious Area 12.6 50 0.0300 0.07 0.9 143 0.0300 2.79 1.4 307 0.0530 3.71				

14.9 500 Total

Subcatchment 2: Subcat 2



Summary for Subcatchment 3: Subcat 3

Runoff = 1.43 cfs @ 12.42 hrs, Volume= 10,675 cf, Depth> 0.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

A	rea (sf)	CN E	Description						
	32,078	49 5	49 50-75% Grass cover, Fair, HSG A						
	923	98 F	Paved road	s w/curbs &	& sewers, HSG A				
	1,530	98 F	Roofs, HSG	βA					
1	18,747	36 V	Voods, Fai	r, HSG A					
1	53,278	40 V	Veighted A	verage					
1	50,825	g	8.40% Per	vious Area					
	2,453	1	.60% Impe	ervious Area	а				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
14.9	50	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.20"				
0.9	171	0.0350	3.01		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
2.6	291	0.0130	1.84		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
0.2	73	0.1920	7.05		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
18.6	585	Total							

2

3 4 5 6 7 8 9 10

1

Hydrograph 1.43 cfs Type III 24-hr 100-Year Rainfall=7.00" Runoff Area=153,278 sf Runoff Volume=10,675 cf Runoff Depth>0.84" Flow Length=585' Tc=18.6 min CN=40

11 12 13 Time (hours)

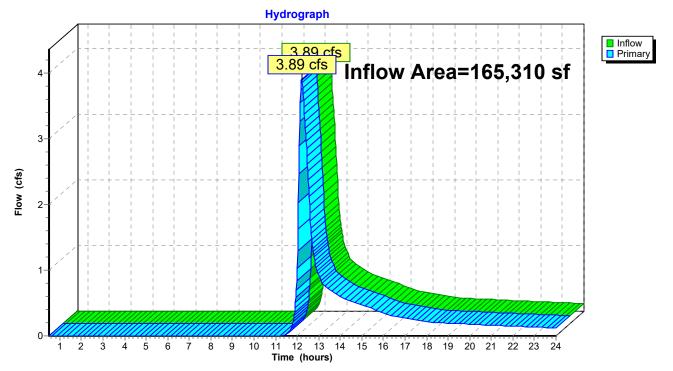
13 14 15 16 17 18 19 20 21 22 23 24

Subcatchment 3: Subcat 3

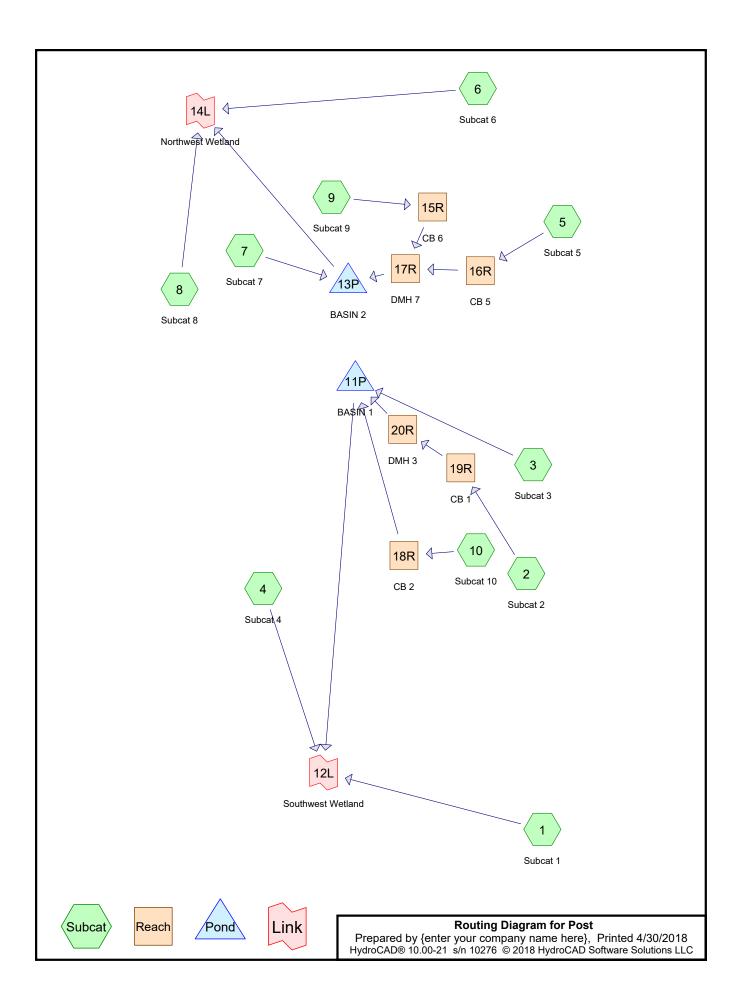
Summary for Link 4L: WETLAND SOUTH/BROOK

Inflow Area	a =	165,310 sf,	8.51% Impervious,	Inflow Depth > 1.45"	for 100-Year event
Inflow	=	3.89 cfs @ 1	12.21 hrs, Volume=	19,966 cf	
Primary	=	3.89 cfs @	12.21 hrs, Volume=	19,966 cf, Atte	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 4L: WETLAND SOUTH/BROOK



Area Listing (all nodes)

Area	CN	Description
(sq-ft)		(subcatchment-numbers)
151,524	49	50-75% Grass cover, Fair, HSG A (1, 2, 3, 4, 5, 6, 7, 8, 9, 10)
35,473	98	Paved roads w/curbs & sewers, HSG A (2, 3, 5, 7, 9, 10)
7,711	98	Roofs, HSG A (3, 4, 5, 6, 7, 8, 9)
123,881	36	Woods, Fair, HSG A (1, 2, 3, 4, 5, 6, 8, 9, 10)
318,589	51	TOTAL AREA

Soil Listing (all nodes)

Area (sq-ft)	Soil Group	Subcatchment Numbers
318,589	HSG A	1, 2, 3, 4, 5, 6, 7, 8, 9, 10
0	HSG B	
0	HSG C	
0	HSG D	
0	Other	
318,589		TOTAL AREA

		Ground		loues		
HSG-A	HSG-B	HSG-C	HSG-D	Other	Total	Ground
 (sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	(sq-ft)	Cover
151,524	0	0	0	0	151,524	50-75% Grass cover, Fair
35,473	0	0	0	0	35,473	Paved roads w/curbs & sewers
7,711	0	0	0	0	7,711	Roofs
123,881	0	0	0	0	123,881	Woods, Fair
318,589	0	0	0	0	318,589	TOTAL AREA

Ground Covers (all nodes)

Line#	Node Number	In-Invert (feet)	Out-Invert (feet)	Length (feet)	Slope (ft/ft)	n	Diam/Width (inches)	Height (inches)	Inside-Fill (inches)
1	15R	67.50	67.40	10.4	0.0096	0.013	12.0	0.0	0.0
2	16R	67.50	67.40	32.0	0.0031	0.013	12.0	0.0	0.0
3	17R	67.40	67.00	24.0	0.0167	0.013	15.0	0.0	0.0
4	18R	66.46	66.40	17.3	0.0035	0.013	12.0	0.0	0.0
5	19R	66.46	66.40	4.5	0.0133	0.013	12.0	0.0	0.0
6	20R	66.40	66.00	32.0	0.0125	0.013	15.0	0.0	0.0

Pipe Listing (all nodes)

Post	Тy
Prepared by {enter your company name here}	
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solution	s LL(

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=20,844 sf 0.00% Impervious Runoff Depth>0.05" Flow Length=319' Tc=10.0 min CN=44 Runoff=0.00 cfs 92 cf
Subcatchment2: Subcat2	Runoff Area=25,588 sf 31.23% Impervious Runoff Depth>0.65" Flow Length=288' Tc=8.4 min CN=64 Runoff=0.33 cfs 1,393 cf
Subcatchment3: Subcat3	Runoff Area=58,660 sf 8.73% Impervious Runoff Depth>0.15" Flow Length=261' Tc=15.8 min CN=49 Runoff=0.04 cfs 717 cf
Subcatchment4: Subcat4	Runoff Area=48,453 sf 1.98% Impervious Runoff Depth>0.02" Flow Length=187' Tc=9.0 min CN=41 Runoff=0.00 cfs 73 cf
Subcatchment 5: Subcat 5	Runoff Area=53,176 sf 19.07% Impervious Runoff Depth>0.28" Flow Length=355' Tc=14.3 min CN=54 Runoff=0.14 cfs 1,240 cf
Subcatchment6: Subcat6	Runoff Area=67,481 sf 1.12% Impervious Runoff Depth>0.02" Flow Length=644' Tc=17.9 min CN=41 Runoff=0.00 cfs 100 cf
Subcatchment7: Subcat7	Runoff Area=12,907 sf 18.31% Impervious Runoff Depth>0.41" Tc=6.0 min CN=58 Runoff=0.08 cfs 445 cf
Subcatchment8: Subcat8	Runoff Area=6,248 sf 5.00% Impervious Runoff Depth>0.09" Tc=6.0 min CN=46 Runoff=0.00 cfs 45 cf
Subcatchment9: Subcat9	Runoff Area=14,166 sf 51.29% Impervious Runoff Depth>1.17" Flow Length=137' Tc=8.6 min CN=74 Runoff=0.39 cfs 1,380 cf
Subcatchment 10: Subcat 10	Runoff Area=11,067 sf 74.80% Impervious Runoff Depth>2.01" Tc=6.0 min CN=86 Runoff=0.60 cfs 1,852 cf
Reach 15R: CB 6 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.23' Max Vel=2.93 fps Inflow=0.39 cfs 1,380 cf L=10.4' S=0.0096 '/' Capacity=3.49 cfs Outflow=0.39 cfs 1,380 cf
Reach 16R: CB 5 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.18' Max Vel=1.45 fps Inflow=0.14 cfs 1,240 cf L=32.0' S=0.0031 '/' Capacity=1.99 cfs Outflow=0.14 cfs 1,239 cf
Reach 17R: DMH 7 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.19' Max Vel=3.51 fps Inflow=0.40 cfs 2,619 cf L=24.0' S=0.0167 '/' Capacity=8.34 cfs Outflow=0.40 cfs 2,619 cf
Reach 18R: CB 2 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.37' Max Vel=2.30 fps Inflow=0.60 cfs 1,852 cf L=17.3' S=0.0035 '/' Capacity=2.10 cfs Outflow=0.60 cfs 1,852 cf
Reach 19R: CB 1 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.19' Max Vel=3.13 fps Inflow=0.33 cfs 1,393 cf L=4.5' S=0.0133 '/' Capacity=4.11 cfs Outflow=0.33 cfs 1,393 cf
Reach 20R: DMH 3	Avg. Flow Depth=0.18' Max Vel=2.98 fps Inflow=0.33 cfs 1,393 cf L=32.0' S=0.0125 '/' Capacity=7.22 cfs Outflow=0.33 cfs 1,393 cf

Post Prepared by {enter your com HydroCAD® 10.00-21 s/n 10276	Type III 24-hr 2-Year Rainfall=3.40 pany name here} Printed 4/30/201 © 2018 HydroCAD Software Solutions LLC Page	8
Pond 11P: BASIN 1	Peak Elev=64.69' Storage=1,240 cf Inflow=0.88 cfs 3,962 Discarded=0.11 cfs 3,943 cf Primary=0.00 cfs 0 cf Outflow=0.11 cfs 3,943 cf	
Pond 13P: BASIN 2	Peak Elev=65.33' Storage=585 cf Inflow=0.48 cfs 3,064 Discarded=0.14 cfs 3,052 cf Primary=0.00 cfs 0 cf Outflow=0.14 cfs 3,052 cf	
Link 12L: Southwest Wetland	Inflow=0.01 cfs 165 Primary=0.01 cfs 165	
Link 14L: Northwest Wetland	Inflow=0.00 cfs 145 Primary=0.00 cfs 145	

Total Runoff Area = 318,589 sf Runoff Volume = 7,337 cf Average Runoff Depth = 0.28" 86.45% Pervious = 275,405 sf 13.55% Impervious = 43,184 sf

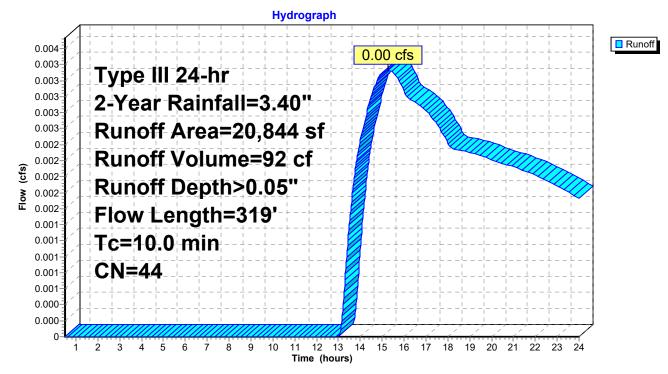
Summary for Subcatchment 1: Subcat 1

Runoff = 0.00 cfs @ 15.27 hrs, Volume= 92 cf, Depth> 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN	Description						
		12,620	49	49 50-75% Grass cover, Fair, HSG A						
_		8,223	36	36 Woods, Fair, HSG A						
		20,844	44	Weighted A	verage					
20,844 100.00% Pervious Area						a				
	Тс	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	8.4	50	0.0300	0.10		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 2.20"				
	0.7	148	0.0510	3.64		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.9	121	0.0190	2.22		Shallow Concentrated Flow,				
_						Unpaved Kv= 16.1 fps				
	10.0	319	Total							

Subcatchment 1: Subcat 1



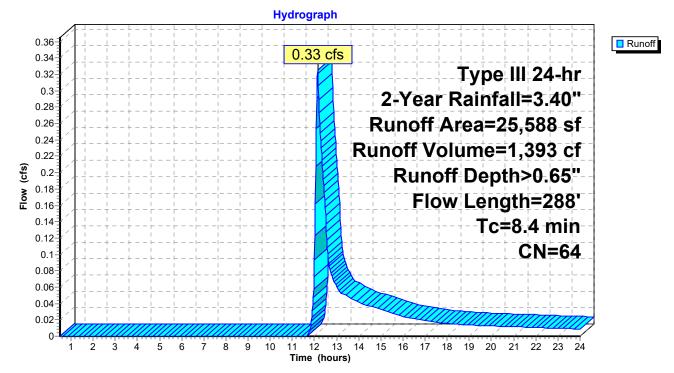
Summary for Subcatchment 2: Subcat 2

Runoff = 0.33 cfs @ 12.14 hrs, Volume= 1,393 cf, Depth> 0.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN [Description						
		17,077	49 5	49 50-75% Grass cover, Fair, HSG A						
		7,991	98 F	8 Paved roads w/curbs & sewers, HSG A						
_		520	36 \	,						
	25,588 64 Weighted Average									
		17,597	6	68.77% Per	vious Area					
		7,991	3	31.23% Imp	pervious Ar	ea				
	_		-							
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	6.9	50	0.0500	0.12		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 2.20"				
	0.4	100	0.0600	3.94		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	1.1	138	0.0110	2.13		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	8.4	288	Total							

Subcatchment 2: Subcat 2



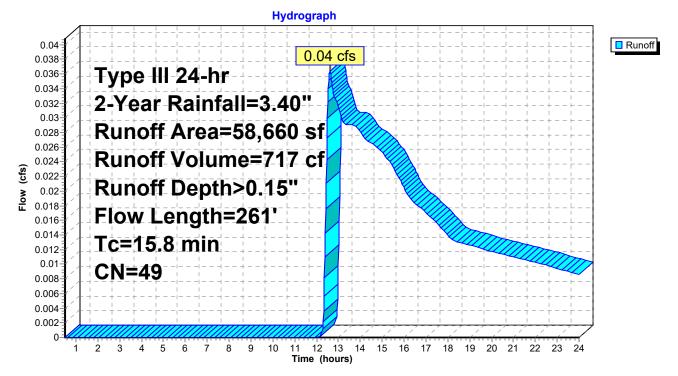
Summary for Subcatchment 3: Subcat 3

Runoff = 0.04 cfs @ 12.61 hrs, Volume= 717 cf, Depth> 0.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

A	rea (sf)	CN [Description						
	33,711	49 5	9 50-75% Grass cover, Fair, HSG A						
	3,296	98 F	Paved roads w/curbs & sewers, HSG A						
	1,826	98 F	Roofs, HSG A						
	19,827	36 \	Woods, Fair, HSG A						
	58,660	49 \	Veighted A	verage					
	53,538	ç	91.27% Per	vious Area					
	5,122	8	8.73% Impe	ervious Are	a				
Тс	Length	Slope	Velocity	Capacity	Description				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
			,		Description Sheet Flow,				
(min)	(feet)	(ft/ft)	(ft/sec)						
(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow,				
<u>(min)</u> 14.9	(feet) 50	(ft/ft) 0.0200	(ft/sec) 0.06		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.20"				

Subcatchment 3: Subcat 3



Summary for Subcatchment 4: Subcat 4

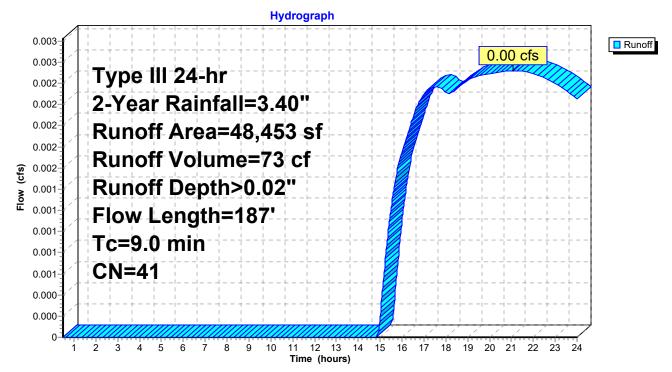
Runoff = 0.00 cfs @ 21.06 hrs, Volume= 73 cf, Depth> 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN I	Description							
		12,754	49 క	49 50-75% Grass cover, Fair, HSG A							
		959	98 I								
_		34,740	36	Woods, Fair, HSG A							
		48,453	41 \	Neighted A	verage						
47,493 98.02% Pervious Area											
		959		1.98% Impe	ervious Are	a					
	Тс	Length	Slope	,	Capacity	Description					
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
	8.4	50	0.0300	0.10		Sheet Flow,					
						Grass: Dense n= 0.240 P2= 2.20"					
	0.0	26	0.3100	8.96		Shallow Concentrated Flow,					
						Unpaved Kv= 16.1 fps					
	0.6	111	0.0410	3.26		Shallow Concentrated Flow,					
_						Unpaved Kv= 16.1 fps					
	0.0	197	Total								

9.0 187 Total

Subcatchment 4: Subcat 4



Summary for Subcatchment 5: Subcat 5

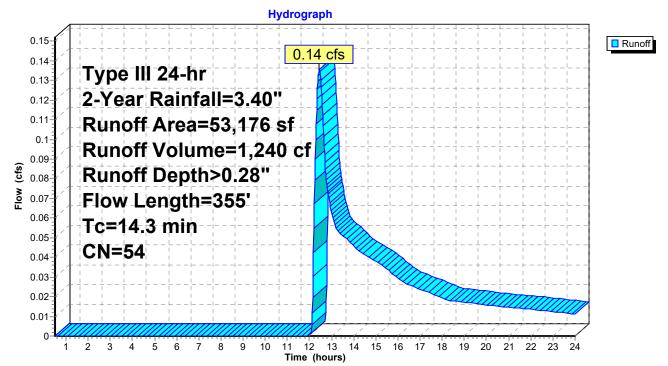
Runoff = 0.14 cfs @ 12.45 hrs, Volume= 1,240 cf, Depth> 0.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN [Description						
		27,303	49 5	49 50-75% Grass cover, Fair, HSG A						
		7,837	98 F	Paved roads w/curbs & sewers, HSG A						
		2,301	98 F	Roofs, HSO	βA					
_		15,734	<u>36</u> \	Woods, Fair, HSG A						
	53,176 54 Weighted Average									
		43,037	8	30.93% Per	vious Area					
		10,138	1	19.07% Imp	pervious Ar	ea				
	Tc	Length	Slope		Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	12.3	50	0.0320	0.07		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.20"				
	1.6	248	0.0270	2.65		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.4	57	0.0122	2.24		Shallow Concentrated Flow,				
	0.4	• •	••••							
_		0.55				Paved Kv= 20.3 fps				

14.3 355 Total

Subcatchment 5: Subcat 5



Summary for Subcatchment 6: Subcat 6

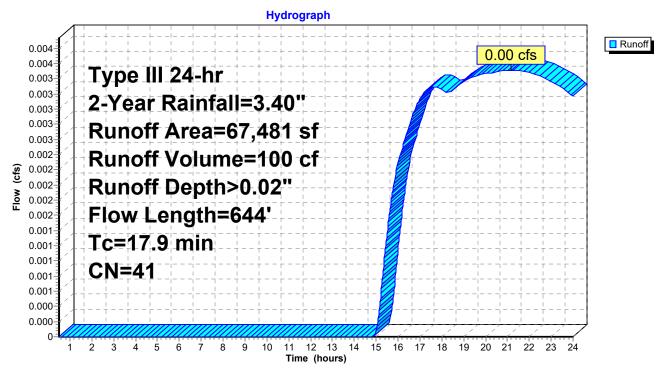
Runoff = 0.00 cfs @ 21.18 hrs, Volume= 100 cf, Depth> 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

_	A	rea (sf)	CN E	Description					
		24,941	49 50-75% Grass cover, Fair, HSG A						
	754 98 Roofs, HSG A 41,787 36 Woods, Fair, HSG A								
		41,787							
	67,481 41 Weighted Average								
	66,727 98.88% Pervious Area								
		754	1	.12% Impe	ervious Are	а			
	_		. .						
	Tc	Length	Slope	Velocity	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	14.9	50	0.0200	0.06		Sheet Flow,			
						Woods: Light underbrush n= 0.400 P2= 2.20"			
	2.2	282	0.0170	2.10		Shallow Concentrated Flow,			
						Unpaved Kv= 16.1 fps			
	0.6	245	0.1600	6.44		Shallow Concentrated Flow,			
			/			Unpaved Kv= 16.1 fps			
	0.2	67	0.2100	7.38		Shallow Concentrated Flow,			
_						Unpaved Kv= 16.1 fps			

17.9 644 Total

Subcatchment 6: Subcat 6



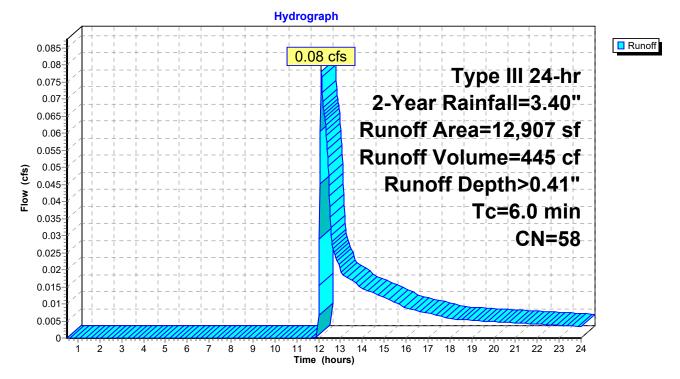
Summary for Subcatchment 7: Subcat 7

Runoff = 0.08 cfs @ 12.13 hrs, Volume= 445 cf, Depth> 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

Α	rea (sf)	CN	Description						
	10,544	49	50-75% Gra	ass cover, F	Fair, HSG A				
	1,337	98	Paved road	s w/curbs &	k sewers, HSG A				
	1,026	98	Roofs, HSG A						
	12,907	12,907 58 Weighted Average							
	10,544		81.69% Pei	vious Area					
	2,363		18.31% Imp	pervious Ar	ea				
_				_					
Tc	Length	Slope		Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Direct Entry,				
6.0					Direct Entry,				

Subcatchment 7: Subcat 7



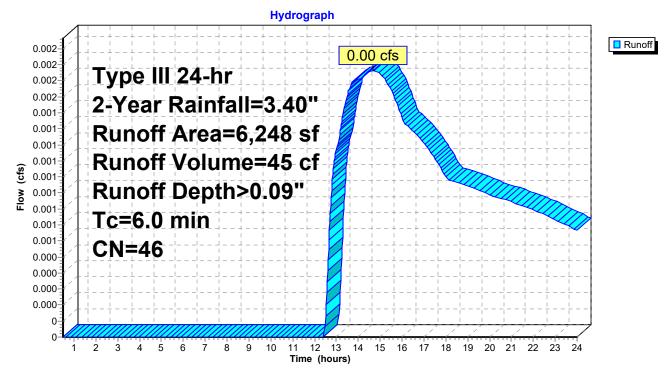
Summary for Subcatchment 8: Subcat 8

Runoff = 0.00 cfs @ 14.68 hrs, Volume= 45 cf, Depth> 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

A	rea (sf)	CN	Description					
	3,110	49	50-75% Gra	ass cover, F	Fair, HSG A			
	313	98	Roofs, HSG	βA				
	2,825	36	Woods, Fair, HSG A					
	6,248	46	Weighted Average					
	5,935		95.00% Pervious Area					
	313		5.00% Impe	ervious Area	a			
_				_				
Тс	Length	Slope		Capacity	Description			
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
6.0					Direct Entry,			

Subcatchment 8: Subcat 8



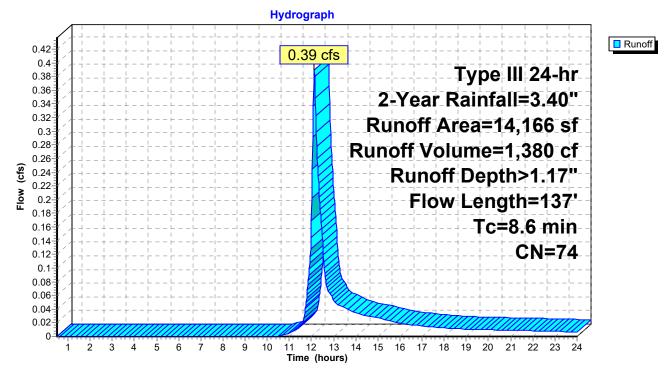
Summary for Subcatchment 9: Subcat 9

Runoff = 0.39 cfs @ 12.13 hrs, Volume= 1,380 cf, Depth> 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

<i>P</i>	vrea (sf)	CN Description							
	6,698	49 50-75% Grass cover, Fair, HSG A							
	6,734	98 Paved roads w/curbs & sewers, HSG A							
	532	98 F	98 Roofs, HSG A						
	202	36 V	36 Woods, Fair, HSG A						
	14,166	74 V	74 Weighted Average						
	6,900	4	8.71% Per	vious Area					
	7,266	5	51.29% Impervious Area						
Тс	Length	Slope	Velocity	Capacity	Description				
()	/								
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
(min) 7.8	(feet) 50	(ft/ft) 0.0360	(ft/sec) 0.11	(cfs)	Sheet Flow,				
	. ,	. ,		(cfs)	Sheet Flow, Grass: Dense n= 0.240 P2= 2.20"				
	. ,	. ,		(cfs)					
7.8	50	0.0360	0.11	(cfs)	Grass: Dense n= 0.240 P2= 2.20"				

Subcatchment 9: Subcat 9



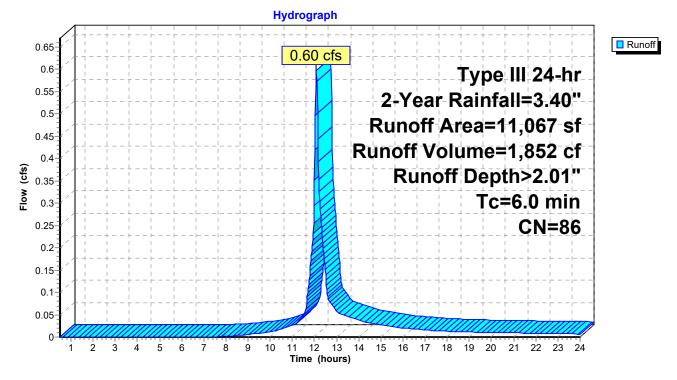
Summary for Subcatchment 10: Subcat 10

Runoff = 0.60 cfs @ 12.09 hrs, Volume= 1,852 cf, Depth> 2.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 2-Year Rainfall=3.40"

A	rea (sf)	CN	Description						
	2,766	49	50-75% Grass cover, Fair, HSG A						
	8,278	98	Paved roads w/curbs & sewers, HSG A						
	23	36	Woods, Fair, HSG A						
	11,067	86	Weighted Average						
	2,789								
	8,278		74.80% Impervious Area						
Тс	Length	Slope		Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Direct Entry,				

Subcatchment 10: Subcat 10



Summary for Reach 15R: CB 6

 Inflow Area =
 14,166 sf, 51.29% Impervious, Inflow Depth > 1.17" for 2-Year event

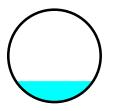
 Inflow =
 0.39 cfs @ 12.13 hrs, Volume=
 1,380 cf

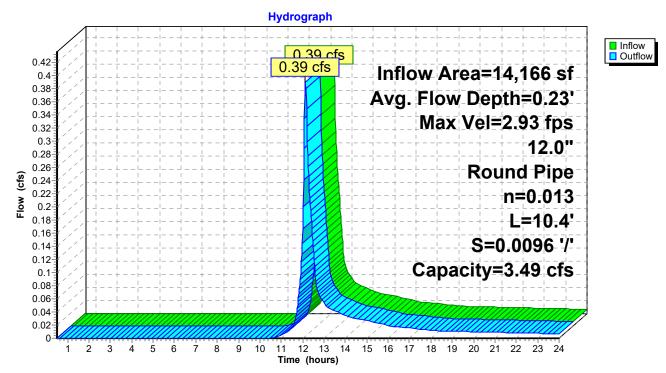
 Outflow =
 0.39 cfs @ 12.13 hrs, Volume=
 1,380 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.93 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.17 fps, Avg. Travel Time= 0.1 min

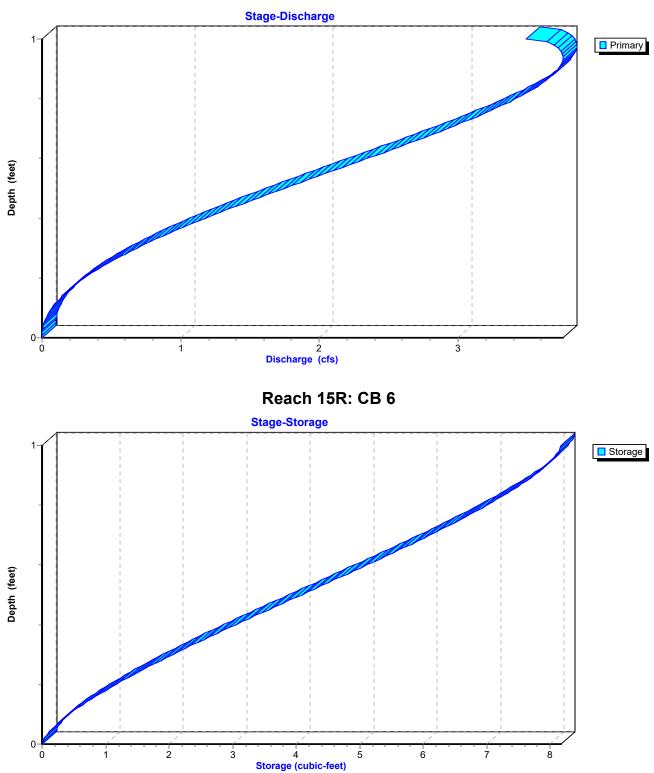
Peak Storage= 1 cf @ 12.13 hrs Average Depth at Peak Storage= 0.23' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.49 cfs

12.0" Round Pipe n= 0.013 Length= 10.4' Slope= 0.0096 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 15R: CB 6



Reach 15R: CB 6

Summary for Reach 16R: CB 5

 Inflow Area =
 53,176 sf, 19.07% Impervious, Inflow Depth > 0.28" for 2-Year event

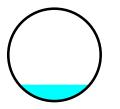
 Inflow =
 0.14 cfs @ 12.45 hrs, Volume=
 1,240 cf

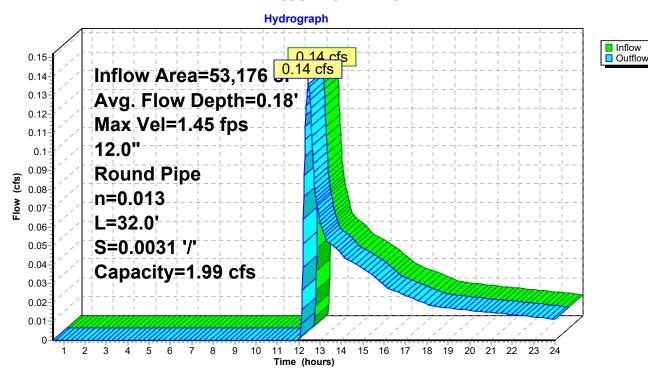
 Outflow =
 0.14 cfs @ 12.45 hrs, Volume=
 1,239 cf, Atten= 0%, Lag= 0.3 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 1.45 fps, Min. Travel Time= 0.4 min Avg. Velocity = 0.87 fps, Avg. Travel Time= 0.6 min

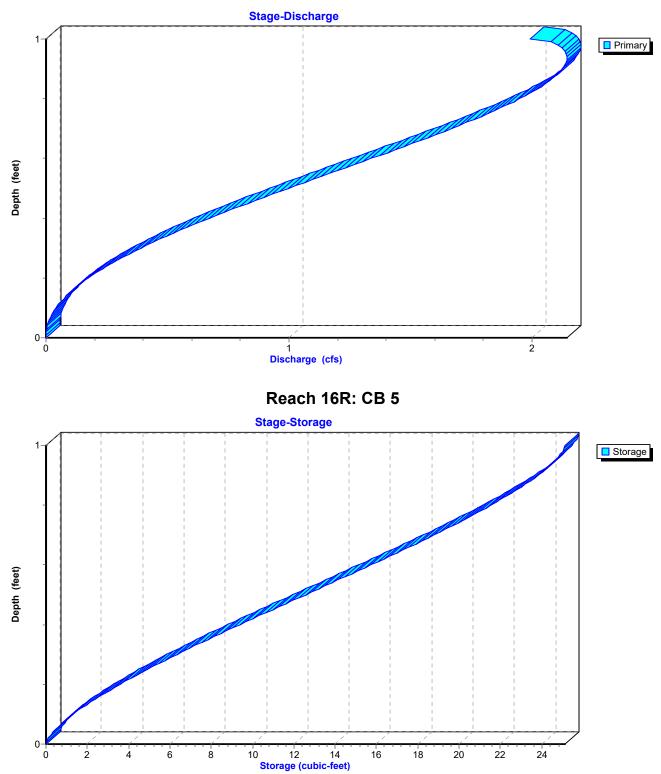
Peak Storage= 3 cf @ 12.45 hrs Average Depth at Peak Storage= 0.18' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 1.99 cfs

12.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0031 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 16R: CB 5



Reach 16R: CB 5

Summary for Reach 17R: DMH 7

 Inflow Area =
 67,342 sf, 25.85% Impervious, Inflow Depth > 0.47" for 2-Year event

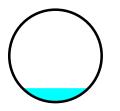
 Inflow =
 0.40 cfs @ 12.14 hrs, Volume=
 2,619 cf

 Outflow =
 0.40 cfs @ 12.14 hrs, Volume=
 2,619 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 3.51 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.74 fps, Avg. Travel Time= 0.2 min

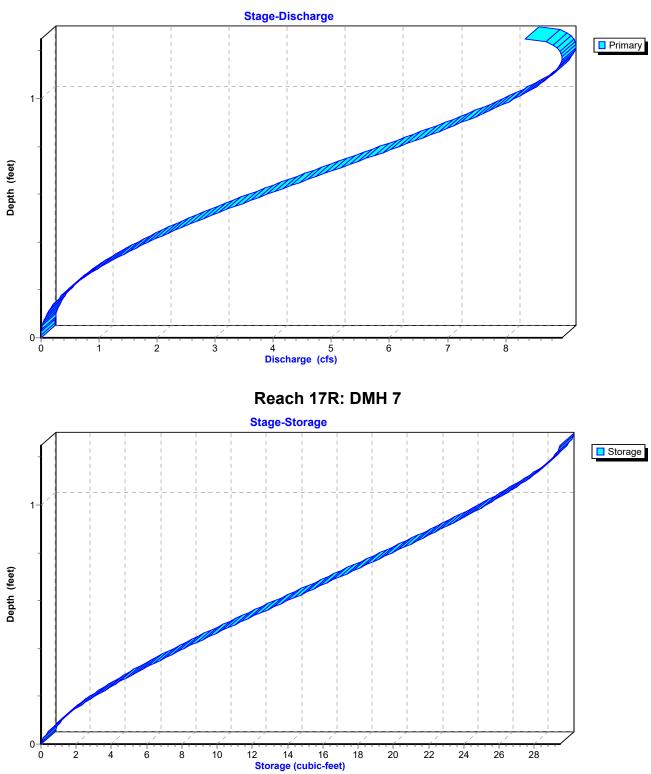
Peak Storage= 3 cf @ 12.14 hrs Average Depth at Peak Storage= 0.19' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 8.34 cfs

15.0" Round Pipe n= 0.013 Length= 24.0' Slope= 0.0167 '/' Inlet Invert= 67.40', Outlet Invert= 67.00'



Hydrograph Inflow Outflow 0 40 cfs 0.44 0.40 cfs Inflow Area=67,342 sf 0.42 0.4 Avg. Flow Depth=0.19' 0.38 0.36 Max Vel=3.51 fps 0.34 0.32-15.0" 0.3 0.28 **Round Pipe** 0.26 (**s**) 0.26 n=0.013 Flow 0.22 0.2 L=24.0' 0.18 0.16-S=0.0167 '/' 0.14-0.12-Capacity=8.34 cfs 0.1 0.08 0.06 0.04 0.02 0 Ż Ś 10 12 13 14 15 16 17 18 19 20 21 22 23 24 1 5 6 8 9 11 Time (hours)

Reach 17R: DMH 7



Reach 17R: DMH 7

Summary for Reach 18R: CB 2

 Inflow Area =
 11,067 sf, 74.80% Impervious, Inflow Depth > 2.01" for 2-Year event

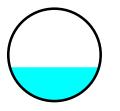
 Inflow =
 0.60 cfs @
 12.09 hrs, Volume=
 1,852 cf

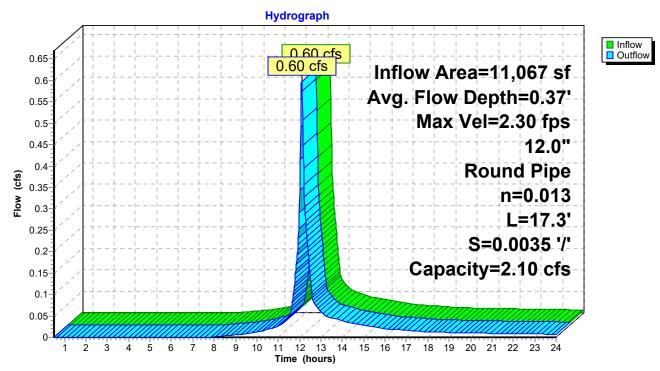
 Outflow =
 0.60 cfs @
 12.09 hrs, Volume=
 1,852 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.30 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.81 fps, Avg. Travel Time= 0.4 min

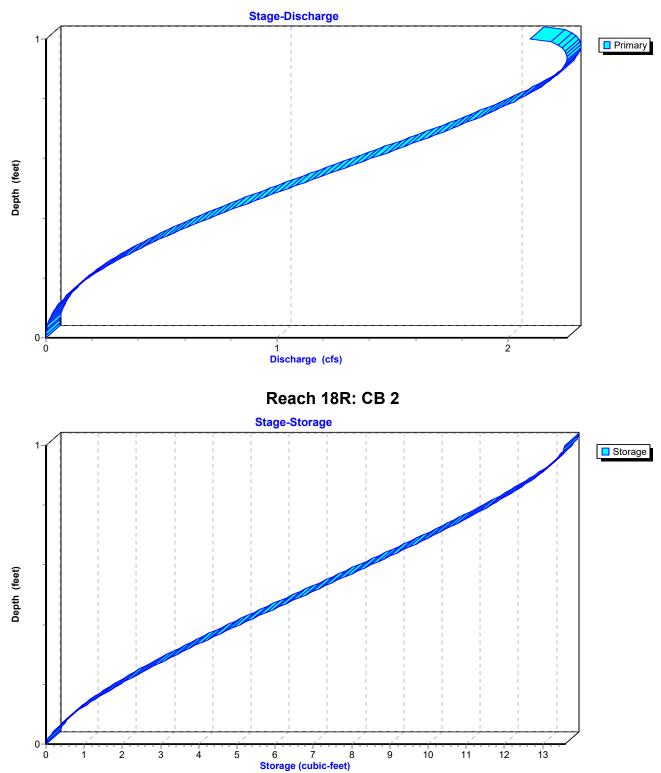
Peak Storage= 4 cf @ 12.09 hrs Average Depth at Peak Storage= 0.37' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.10 cfs

12.0" Round Pipe n= 0.013 Length= 17.3' Slope= 0.0035 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 18R: CB 2



Reach 18R: CB 2

Summary for Reach 19R: CB 1

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 0.65" for 2-Year event

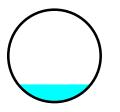
 Inflow =
 0.33 cfs @ 12.14 hrs, Volume=
 1,393 cf

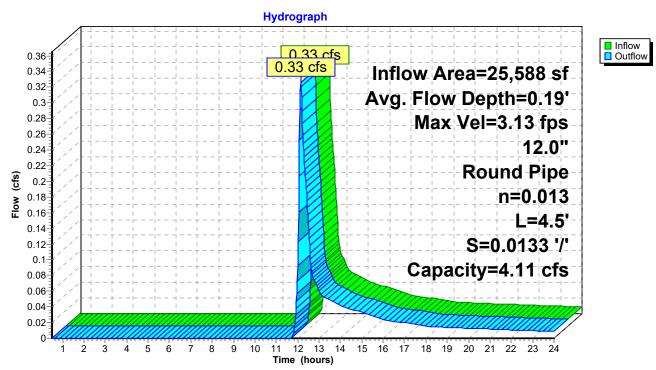
 Outflow =
 0.33 cfs @ 12.14 hrs, Volume=
 1,393 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 3.13 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.41 fps, Avg. Travel Time= 0.1 min

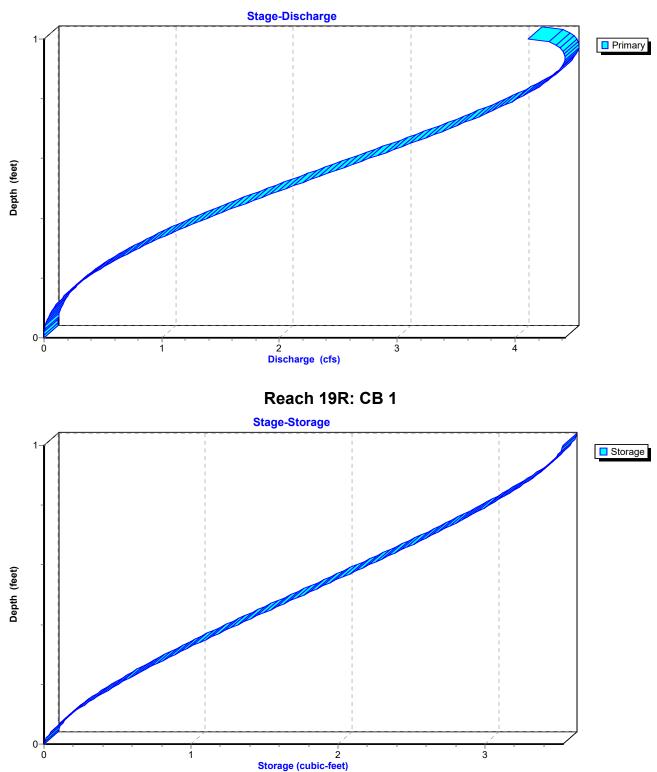
Peak Storage= 0 cf @ 12.14 hrs Average Depth at Peak Storage= 0.19' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 4.11 cfs

12.0" Round Pipe n= 0.013 Length= 4.5' Slope= 0.0133 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 19R: CB 1



Reach 19R: CB 1

Summary for Reach 20R: DMH 3

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 0.65" for 2-Year event

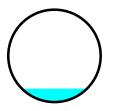
 Inflow =
 0.33 cfs @ 12.14 hrs, Volume=
 1,393 cf

 Outflow =
 0.33 cfs @ 12.15 hrs, Volume=
 1,393 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.98 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.34 fps, Avg. Travel Time= 0.4 min

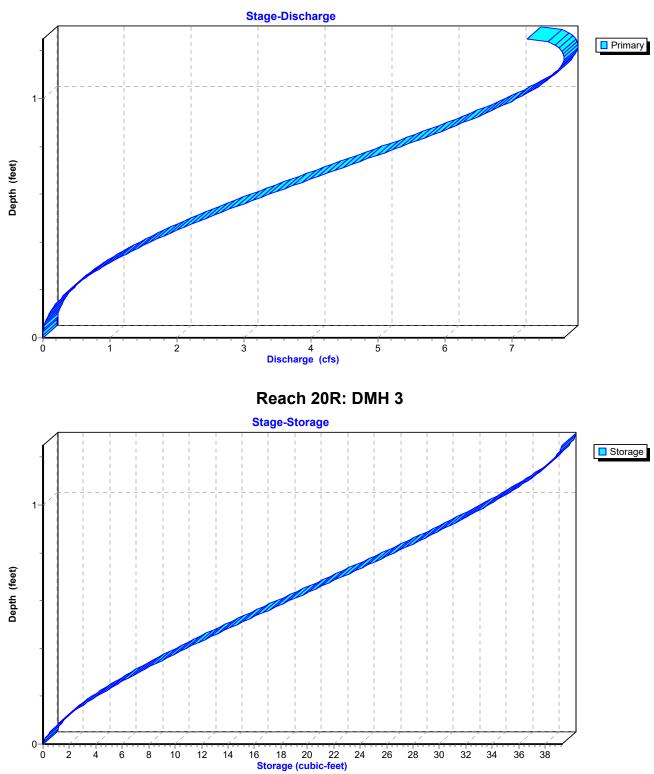
Peak Storage= 4 cf @ 12.15 hrs Average Depth at Peak Storage= 0.18' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 7.22 cfs

15.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0125 '/' Inlet Invert= 66.40', Outlet Invert= 66.00'



Hydrograph Inflow Outflow 0.33 cfs 0.36 0.33 cfs Inflow Area=25,588 sf 0.34 0.32 Avg. Flow Depth=0.18' 0.3 0.28 Max Vel=2.98 fps 0.26 15.0" 0 24 0.22 **Round Pipe** (cfs) 0.2 n=0.013 Flow 0.18 0.16 L=32.0' 0.14 S=0.0125 '/' 0.12 0.1 Capacity=7.22 cfs 0.08 0.06 0.04 0.02 0 Ż Ś 10 11 12 13 14 15 16 17 18 19 20 21 22 23 1 5 6 8 9 24 Time (hours)

Reach 20R: DMH 3



Reach 20R: DMH 3

Summary for Pond 11P: BASIN 1

Inflow Area =	95,314 sf, 22.44% Impervious,	Inflow Depth > 0.50" for 2-Year event
Inflow =	0.88 cfs @ 12.11 hrs, Volume=	3,962 cf
Outflow =	0.11 cfs @ 13.95 hrs, Volume=	3,943 cf, Atten= 88%, Lag= 110.4 min
Discarded =	0.11 cfs @ 13.95 hrs, Volume=	3,943 cf
Primary =	0.00 cfs @ 0.50 hrs, Volume=	0 cf

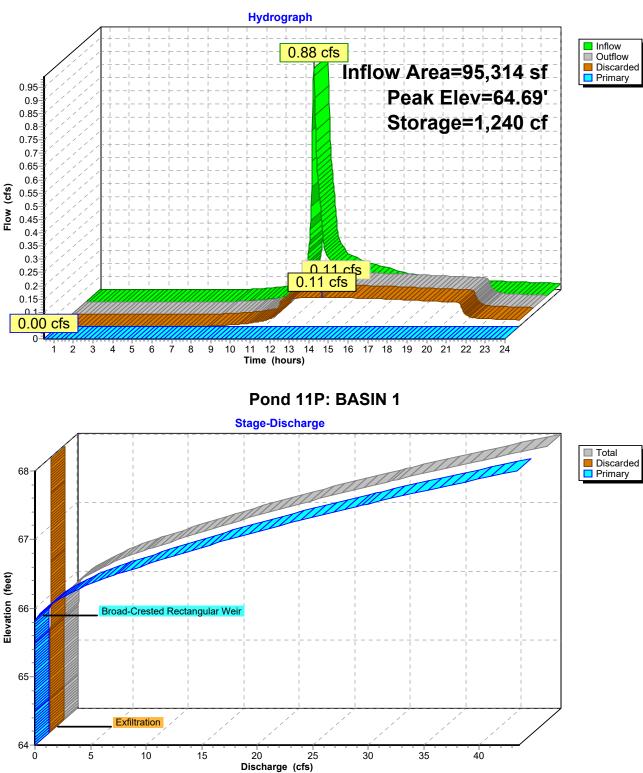
Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 64.69' @ 13.95 hrs Surf.Area= 1,955 sf Storage= 1,240 cf

Plug-Flow detention time= 115.6 min calculated for 3,943 cf (100% of inflow) Center-of-Mass det. time= 113.0 min (993.0 - 880.0)

Volume	Inve	rt Avail.Sto	rage Sto	rage Description	
#1	64.00	D' 10,88	30 cf Cu s	stom Stage Data (Pi	rismatic)Listed below
Elevatio	on S	Surf.Area	Inc.Stor	e Cum.Store	
(fee	et)	(sq-ft)	(cubic-fee	t) (cubic-feet)	
64.0	00	1,611		0 0	
64.5	50	1,857	86	7 867	
65.0	00	2,118	99	4 1,861	
65.5	50	2,392	1,12	8 2,988	
66.0	00	2,681	1,26	8 4,257	
66.5	50	2,984	1,41	6 5,673	
67.0	00	3,301	1,57	1 7,244	
67.5	50	3,632	1,73		
68.0		3,977	1,90		
		-) -	,	-,	
Device	Routing	Invert	Outlet De	evices	
#1	Primary	65.80'	4.0' lona	x 0.5' breadth Broa	ad-Crested Rectangular Weir
	,			et) 0.20 0.40 0.60	
				nglish) 2.80 2.92 3.	
#2	Discardeo	64.00'		hr Exfiltration over	
	210001.000	. 01.00			
D '					

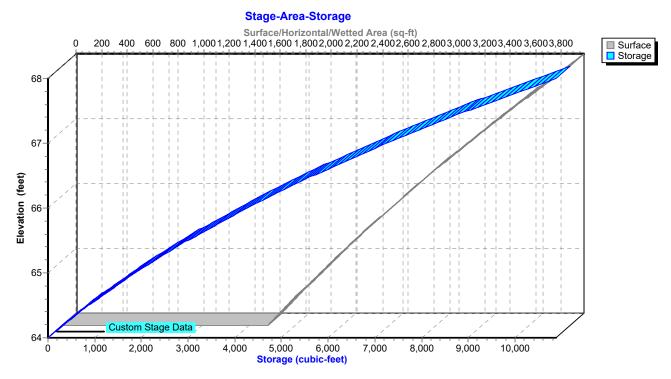
Discarded OutFlow Max=0.11 cfs @ 13.95 hrs HW=64.69' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.11 cfs)

Primary OutFlow Max=0.00 cfs @ 0.50 hrs HW=64.00' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 11P: BASIN 1

Pond 11P: BASIN 1



Summary for Pond 13P: BASIN 2

Inflow Area =	80,249 sf, 24.63% Impervious,	Inflow Depth > 0.46" for 2-Year event
Inflow =	0.48 cfs @ 12.14 hrs, Volume=	3,064 cf
Outflow =	0.14 cfs @ 12.95 hrs, Volume=	3,052 cf, Atten= 70%, Lag= 48.2 min
Discarded =	0.14 cfs @ 12.95 hrs, Volume=	3,052 cf
Primary =	0.00 cfs $\overline{@}$ 0.50 hrs, Volume=	0 cf

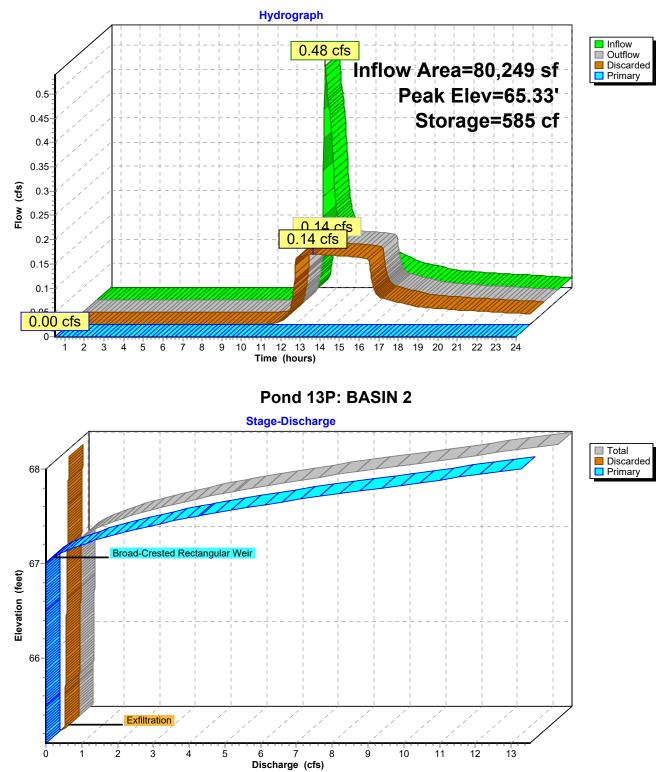
Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 65.33' @ 12.95 hrs Surf.Area= 2,583 sf Storage= 585 cf

Plug-Flow detention time= 32.2 min calculated for 3,052 cf (100% of inflow) Center-of-Mass det. time= 30.2 min (938.0 - 907.8)

Volume	Inver	t Avail.Sto	rage Storag	e Description	
#1	65.10	' 9,9 ⁻	10 cf Custo	m Stage Data (Pi	rismatic)Listed below
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
65.1	10	2,409	0	0	
65.5	50	2,714	1,025	1,025	
66.0	00	3,033	1,437	2,461	
66.5	50	3,366	1,600	4,061	
67.0	00	3,714	1,770	5,831	
67.5	50	4,075	1,947	7,778	
68.0	00	4,451	2,132	9,910	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	67.00'	4.0' long x	0.5' breadth Broa	ad-Crested Rectangular Weir
	2		Head (feet)	0.20 0.40 0.60	0.80 1.00
			Coef. (Englis	sh) 2.80 2.92 3.	08 3.30 3.32
#2	Discarded	65.10'	2.410 in/hr	Exfiltration over	Surface area
Dia a a sol		$\sim M_{ov} - 0.44$ of			Diacharra)

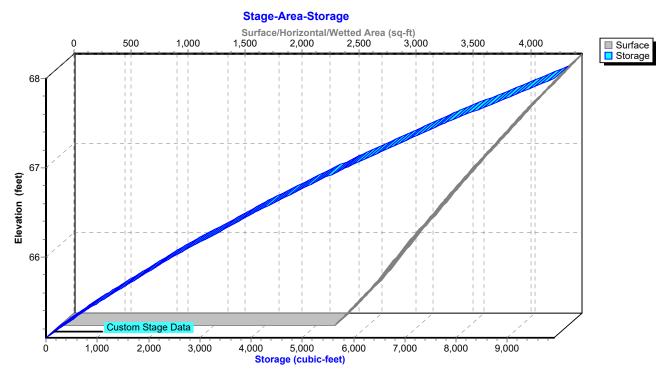
Discarded OutFlow Max=0.14 cfs @ 12.95 hrs HW=65.33' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.14 cfs)

Primary OutFlow Max=0.00 cfs @ 0.50 hrs HW=65.10' (Free Discharge) —1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 13P: BASIN 2

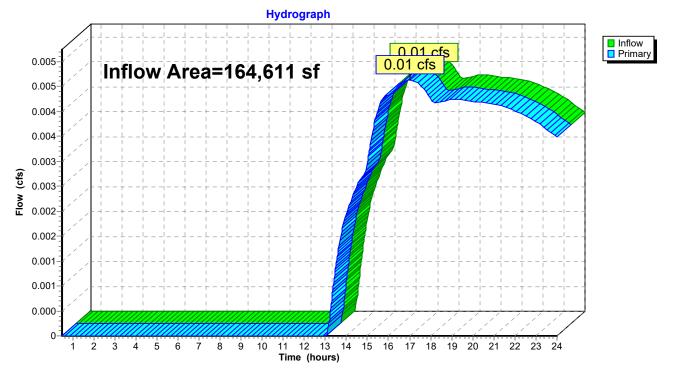
Pond 13P: BASIN 2



Summary for Link 12L: Southwest Wetland

Inflow Area	a =	164,611 sf,	13.58% Impervious,	Inflow Depth >	0.01"	for 2-Year event
Inflow	=	0.01 cfs @	17.00 hrs, Volume=	165 c	f	
Primary	=	0.01 cfs @	17.00 hrs, Volume=	165 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs

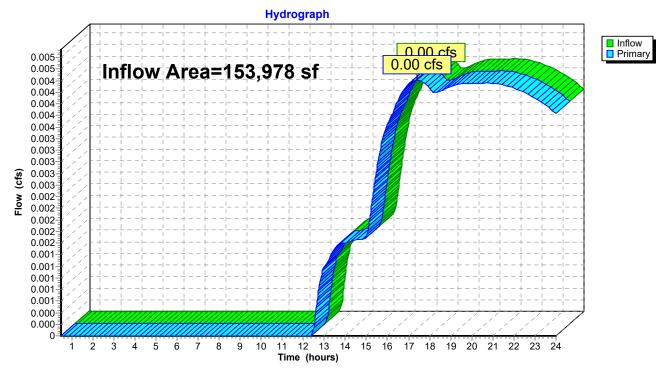


Link 12L: Southwest Wetland

Summary for Link 14L: Northwest Wetland

Inflow Area	a =	153,978 sf,	13.53% Impervious,	Inflow Depth >	0.01"	for 2-Year event
Inflow	=	0.00 cfs @	17.40 hrs, Volume=	145 c	f	
Primary	=	0.00 cfs @	17.40 hrs, Volume=	145 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 14L: Northwest Wetland

Post	Туре
Prepared by {enter your company name here}	
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solution	าร LLC

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=20,844 sf 0.00% Impervious Runoff Depth>0.31" Flow Length=319' Tc=10.0 min CN=44 Runoff=0.05 cfs 539 cf
Subcatchment2: Subcat2	Runoff Area=25,588 sf 31.23% Impervious Runoff Depth>1.39" Flow Length=288' Tc=8.4 min CN=64 Runoff=0.81 cfs 2,956 cf
Subcatchment 3: Subcat 3	Runoff Area=58,660 sf 8.73% Impervious Runoff Depth>0.52" Flow Length=261' Tc=15.8 min CN=49 Runoff=0.34 cfs 2,556 cf
Subcatchment4: Subcat4	Runoff Area=48,453 sf 1.98% Impervious Runoff Depth>0.20" Flow Length=187' Tc=9.0 min CN=41 Runoff=0.05 cfs 822 cf
Subcatchment 5: Subcat 5	Runoff Area=53,176 sf 19.07% Impervious Runoff Depth>0.78" Flow Length=355' Tc=14.3 min CN=54 Runoff=0.61 cfs 3,438 cf
Subcatchment 6: Subcat 6	Runoff Area=67,481 sf 1.12% Impervious Runoff Depth>0.20" Flow Length=644' Tc=17.9 min CN=41 Runoff=0.06 cfs 1,138 cf
Subcatchment7: Subcat7	Runoff Area=12,907 sf 18.31% Impervious Runoff Depth>1.01" Tc=6.0 min CN=58 Runoff=0.29 cfs 1,082 cf
Subcatchment8: Subcat8	Runoff Area=6,248 sf 5.00% Impervious Runoff Depth>0.39" Tc=6.0 min CN=46 Runoff=0.02 cfs 204 cf
Subcatchment9: Subcat9	Runoff Area=14,166 sf 51.29% Impervious Runoff Depth>2.12" Flow Length=137' Tc=8.6 min CN=74 Runoff=0.73 cfs 2,507 cf
Subcatchment10: Subcat10	Runoff Area=11,067 sf 74.80% Impervious Runoff Depth>3.18" Tc=6.0 min CN=86 Runoff=0.94 cfs 2,937 cf
Reach 15R: CB 6 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.31' Max Vel=3.52 fps Inflow=0.73 cfs 2,507 cf L=10.4' S=0.0096 '/' Capacity=3.49 cfs Outflow=0.73 cfs 2,507 cf
Reach 16R: CB 5 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.38' Max Vel=2.23 fps Inflow=0.61 cfs 3,438 cf L=32.0' S=0.0031 '/' Capacity=1.99 cfs Outflow=0.61 cfs 3,437 cf
Reach 17R: DMH 7 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.32' Max Vel=4.80 fps Inflow=1.18 cfs 5,944 cf L=24.0' S=0.0167 '/' Capacity=8.34 cfs Outflow=1.18 cfs 5,943 cf
Reach 18R: CB 2 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.47' Max Vel=2.59 fps Inflow=0.94 cfs 2,937 cf L=17.3' S=0.0035 '/' Capacity=2.10 cfs Outflow=0.94 cfs 2,937 cf
Reach 19R: CB 1 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.30' Max Vel=4.07 fps Inflow=0.81 cfs 2,956 cf L=4.5' S=0.0133 '/' Capacity=4.11 cfs Outflow=0.81 cfs 2,956 cf
Reach 20R: DMH 3 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.28' Max Vel=3.89 fps Inflow=0.81 cfs 2,956 cf L=32.0' S=0.0125 '/' Capacity=7.22 cfs Outflow=0.81 cfs 2,955 cf

Post Prepared by {enter your com HydroCAD® 10.00-21 s/n 10276		<i>10-Year Rainfall=4.70"</i> Printed 4/30/2018 Page 39
Pond 11P: BASIN 1 D	Peak Elev=65.82' Storage=3,795 c iscarded=0.14 cfs 6,304 cf Primary=0.04 cfs 161 cf	
Pond 13P: BASIN 2	Peak Elev=66.07' Storage=2,673 c Discarded=0.17 cfs 7,000 cf Primary=0.00 cfs 0 cf	
Link 12L: Southwest Wetland		Inflow=0.10 cfs 1,523 cf Primary=0.10 cfs 1,523 cf
Link 14L: Northwest Wetland		Inflow=0.07 cfs 1,342 cf Primary=0.07 cfs 1,342 cf

Total Runoff Area = 318,589 sf Runoff Volume = 18,179 cf Average Runoff Depth = 0.68" 86.45% Pervious = 275,405 sf 13.55% Impervious = 43,184 sf

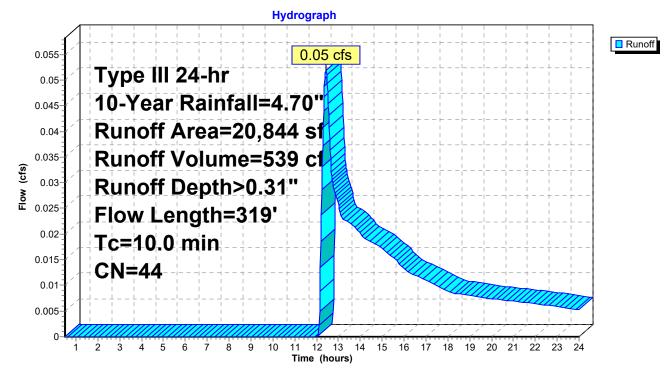
Summary for Subcatchment 1: Subcat 1

Runoff = 0.05 cfs @ 12.43 hrs, Volume= 539 cf, Depth> 0.31"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN [Description		
	12,620	49 5	50-75% Gra	ass cover, l	Fair, HSG A
	8,223	36 V	<u> Noods, Fai</u>	r, HSG A	
	20,844	44 \	Veighted A	verage	
	20,844	1	100.00% Pe	ervious Are	a
Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
8.4	50	0.0300	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 2.20"
0.7	148	0.0510	3.64		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.9	121	0.0190	2.22		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
10.0	319	Total			

Subcatchment 1: Subcat 1



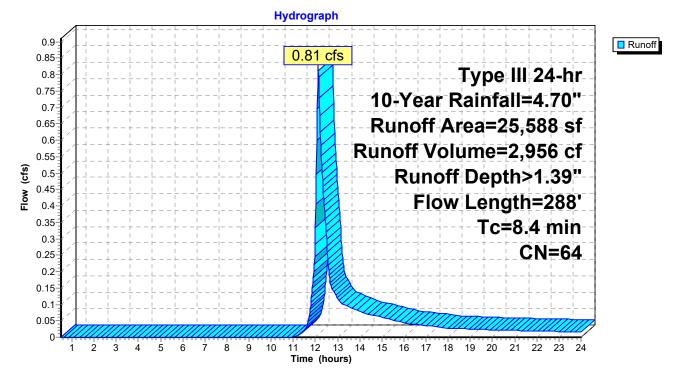
Summary for Subcatchment 2: Subcat 2

Runoff = 0.81 cfs @ 12.13 hrs, Volume= 2,956 cf, Depth> 1.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	A	rea (sf)	CN [Description		
		17,077	49 5	50-75% Gra	ass cover, F	Fair, HSG A
		7,991	98 F	Paved road	s w/curbs &	& sewers, HSG A
_		520	36 V	Voods, Fai	r, HSG A	
		25,588	64 V	Veighted A	verage	
		17,597	6	68.77% Per	vious Area	
		7,991	3	81.23% Imp	pervious Are	ea
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	6.9	50	0.0500	0.12		Sheet Flow,
						Grass: Dense n= 0.240 P2= 2.20"
	0.4	100	0.0600	3.94		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	1.1	138	0.0110	2.13		Shallow Concentrated Flow,
_						Paved Kv= 20.3 fps
	8.4	288	Total			

Subcatchment 2: Subcat 2



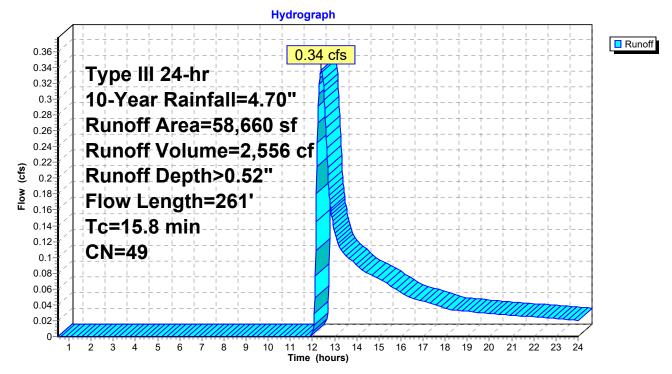
Summary for Subcatchment 3: Subcat 3

Runoff = 0.34 cfs @ 12.39 hrs, Volume= 2,556 cf, Depth> 0.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN E	Description		
	33,711	49 5	50-75% Gra	ass cover, F	Fair, HSG A
	3,296	98 F	Paved road	s w/curbs &	& sewers, HSG A
	1,826	98 F	Roofs, HSG	βA	
	19,827	36 V	Voods, Fai	r, HSG A	
	58,660	49 V	Veighted A	verage	
	53,538	ç	1.27% Per	vious Area	
	5,122	8	8.73% Impe	ervious Are	а
Тс	Length	Slope	Velocity	Capacity	Description
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
					Description Sheet Flow,
(min)	(feet)	(ft/ft)	(ft/sec)		
(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow,
<u>(min)</u> 14.9	(feet) 50	(ft/ft) 0.0200	(ft/sec) 0.06		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.20"

Subcatchment 3: Subcat 3



Summary for Subcatchment 4: Subcat 4

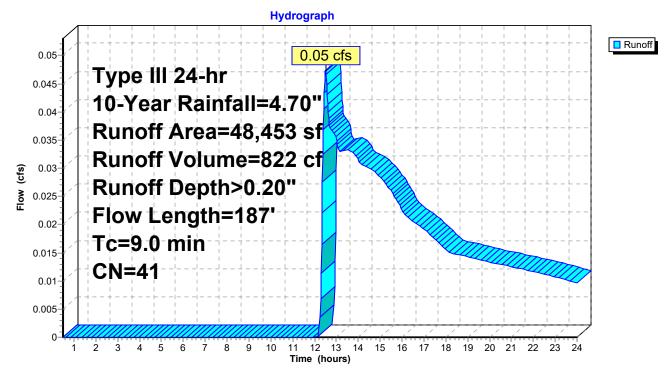
0.05 cfs @ 12.50 hrs, Volume= 822 cf, Depth> 0.20" Runoff =

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN E	Description						
	12,754	49 50-75% Grass cover, Fair, HSG A							
	959	98 F	Roofs, HSG A						
	34,740	36 V	Woods, Fair, HSG A						
	48,453 41 Weighted Average								
	47,493	ç	8.02% Per	vious Area					
	959	1	.98% Impe	ervious Area	а				
Тс	Length	Slope	Velocity	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.4	50	0.0300	0.10		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 2.20"				
0.0	26	0.3100	8.96		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
0.6	111	0.0410	3.26		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
9.0	187	Total							

Total 187

Subcatchment 4: Subcat 4



Summary for Subcatchment 5: Subcat 5

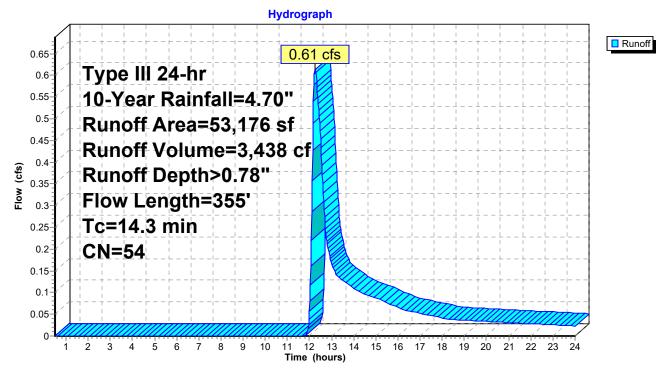
Runoff = 0.61 cfs @ 12.25 hrs, Volume= 3,438 cf, Depth> 0.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

_	A	rea (sf)	CN E	Description							
		27,303	49 5	49 50-75% Grass cover, Fair, HSG A							
		7,837	98 F	,							
		2,301	98 F	3 Roofs, HSG A							
_		15,734	36 V	Voods, Fai	r, HSG A						
		53,176	54 V	Veighted A	verage						
		43,037	8	0.93% Per	vious Area						
		10,138	1	9.07% Imp	pervious Are	ea					
	_										
	Tc	Length	Slope	Velocity	Capacity	Description					
	(min)				· · ·						
_	(11111)	(feet)	(ft/ft)	(ft/sec)	(cfs)						
_	12.3	(feet) 50	(ft/ft) 0.0320	(ft/sec) 0.07	(cfs)	Sheet Flow,					
_	12.3	50	0.0320	0.07	(cfs)	Woods: Light underbrush n= 0.400 P2= 2.20"					
_		· /		/	(cfs)	Woods: Light underbrush n= 0.400 P2= 2.20" Shallow Concentrated Flow,					
_	12.3 1.6	50 248	0.0320 0.0270	0.07 2.65	(cfs)	Woods: Light underbrush n= 0.400 P2= 2.20" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					
_	12.3	50	0.0320	0.07	(cfs)	Woods: Light underbrush n= 0.400 P2= 2.20" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps Shallow Concentrated Flow,					
_	12.3 1.6	50 248	0.0320 0.0270	0.07 2.65	(cfs)	Woods: Light underbrush n= 0.400 P2= 2.20" Shallow Concentrated Flow, Unpaved Kv= 16.1 fps					

14.3 355 Total

Subcatchment 5: Subcat 5



Summary for Subcatchment 6: Subcat 6

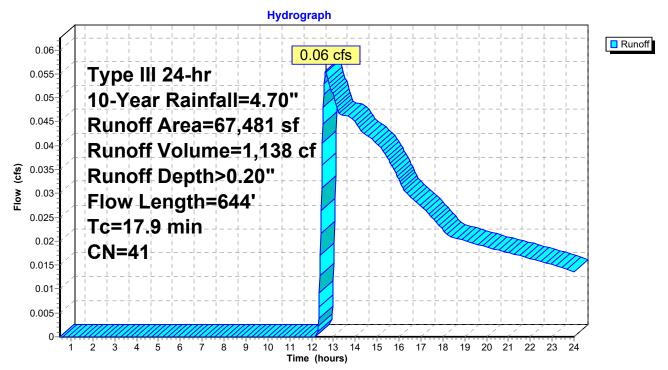
Runoff = 0.06 cfs @ 12.65 hrs, Volume= 1,138 cf, Depth> 0.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

	А	rea (sf)	CN [Description						
		24,941	49 5	49 50-75% Grass cover, Fair, HSG A						
		754	98 F							
		41,787	36 \	,						
		67,481	41 \	Veighted A	verage					
		66,727	ç	98.88% Pei	vious Area	l				
		754	-	l.12% Impe	ervious Are	a				
				-						
	Тс	Length	Slope	Velocity	Capacity	Description				
(I	min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	14.9	50	0.0200	0.06		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.20"				
	2.2	282	0.0170	2.10		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.6	245	0.1600	6.44		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.2	67	0.2100	7.38		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				

17.9 644 Total

Subcatchment 6: Subcat 6



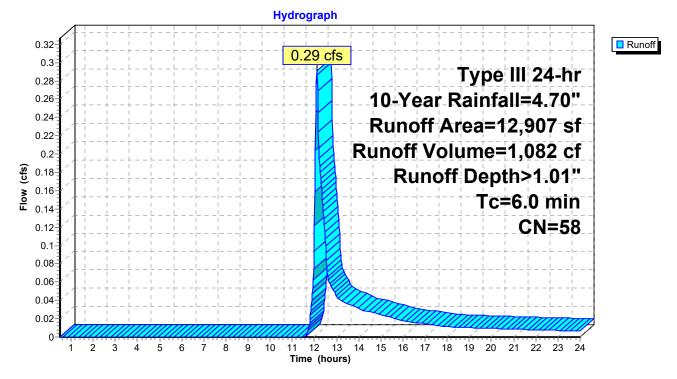
Summary for Subcatchment 7: Subcat 7

Runoff = 0.29 cfs @ 12.10 hrs, Volume= 1,082 cf, Depth> 1.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

Area	a (sf)	CN	Description							
10),544	49	50-75% Grass cover, Fair, HSG A							
1	1,337	98	Paved roads w/curbs & sewers, HSG A							
1	1,026	98	Roofs, HSG	6 A						
12	2,907	58	Neighted A	verage						
10),544	1	31.69% Per	vious Area						
2	2,363		18.31% Impervious Area							
Tc L	.ength	Slope		Capacity	Description					
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)						
6.0					Direct Entry,					

Subcatchment 7: Subcat 7



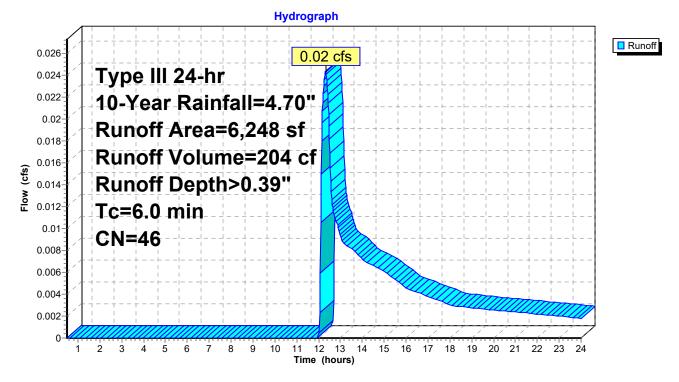
Summary for Subcatchment 8: Subcat 8

Runoff = 0.02 cfs @ 12.32 hrs, Volume= 204 cf, Depth> 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN	Description						
	3,110	49	50-75% Gra	ass cover, F	Fair, HSG A				
	313	98	Roofs, HSG A						
	2,825	36	Woods, Fai	r, HSG A					
	6,248	46	Weighted A	verage					
	5,935		95.00% Per	vious Area	l				
	313		5.00% Impe	ervious Area	а				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description				
6.0			<u> </u>		Direct Entry,				

Subcatchment 8: Subcat 8



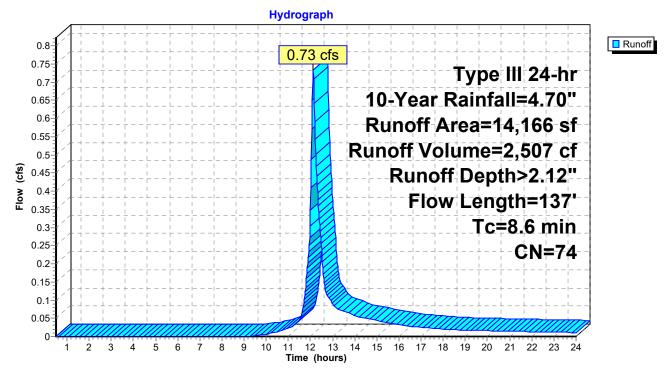
Summary for Subcatchment 9: Subcat 9

Runoff = 0.73 cfs @ 12.13 hrs, Volume= 2,507 cf, Depth> 2.12"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

A	rea (sf)	CN [Description			_			
	6,698	49 5	Fair, HSG A						
	6,734	98 Paved roads w/curbs & sewers, HSG A							
	532	98 F	98 Roofs, HSG A						
	202	36 Woods, Fair, HSG A							
	14,166	74 V	Veighted A	verage					
	6,900	4	8.71% Per	vious Area					
	7,266	5	51.29% Imp	pervious Ar	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	_			
	0				Description Sheet Flow,	_			
(min)	(feet)	(ft/ft)	(ft/sec)			_			
(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow, Grass: Dense n= 0.240 P2= 2.20" Shallow Concentrated Flow,	_			
<u>(min)</u> 7.8	(feet) 50	(ft/ft) 0.0360	(ft/sec) 0.11		Sheet Flow, Grass: Dense n= 0.240 P2= 2.20"	_			

Subcatchment 9: Subcat 9

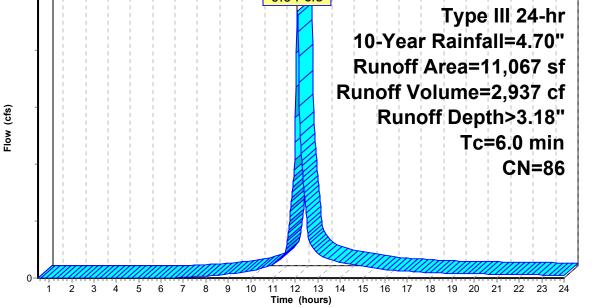


Summary for Subcatchment 10: Subcat 10

Runoff = 0.94 cfs @ 12.09 hrs, Volume= 2,937 cf, Depth> 3.18"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 10-Year Rainfall=4.70"

Area (sf)	CN	Description							
2,766 49 50-75% Grass cover, Fair, HSG A									
8,278	98 Paved roads w/curbs & sewers, HSG A								
23	36	36 Woods, Fair, HSG A							
11,067	7 86 Weighted Average								
2,789		25.20% Per	vious Area	1					
8,278		74.80% Imp	pervious Ar	ea					
Tc Length (min) (feet)	Slop (ft/f		Capacity (cfs)	Description					
6.0				Direct Entry,					
	Subcatchment 10: Subcat 10								
	1 1		Hydro	grapn		I			
1-* 1-*	1- 0.94 cfs Type III 24-hr 10 Veer Deinfelle 4 70"								



Summary for Reach 15R: CB 6

 Inflow Area =
 14,166 sf, 51.29% Impervious, Inflow Depth > 2.12" for 10-Year event

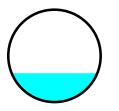
 Inflow =
 0.73 cfs @
 12.13 hrs, Volume=
 2,507 cf

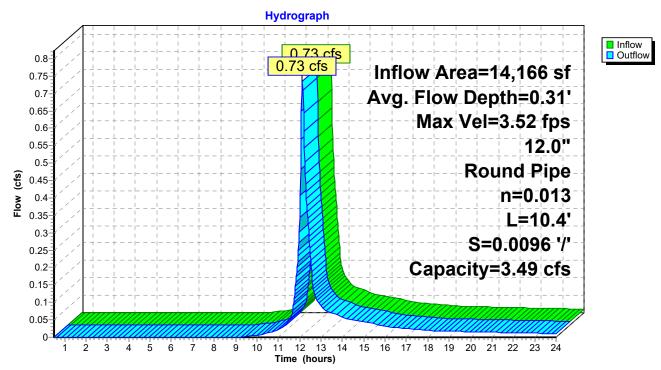
 Outflow =
 0.73 cfs @
 12.13 hrs, Volume=
 2,507 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 3.52 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.34 fps, Avg. Travel Time= 0.1 min

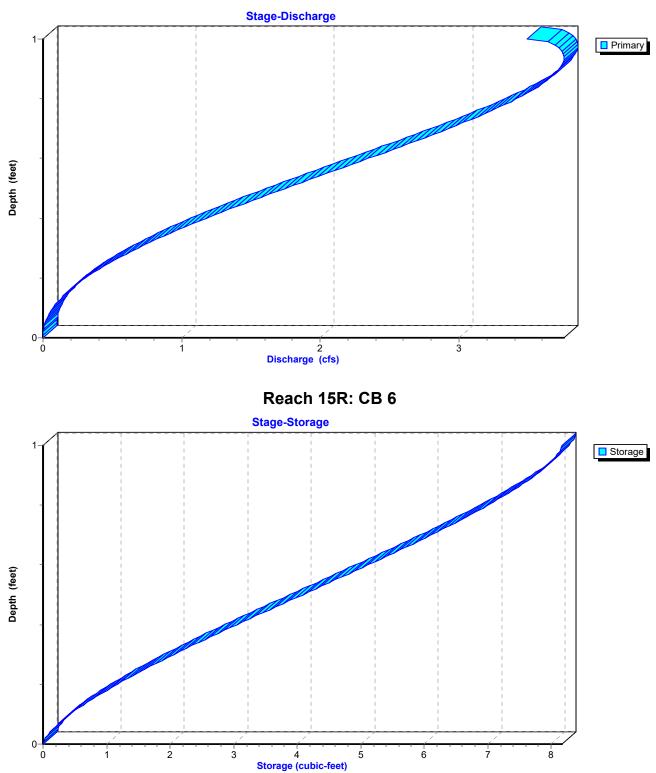
Peak Storage= 2 cf @ 12.13 hrs Average Depth at Peak Storage= 0.31' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.49 cfs

12.0" Round Pipe n= 0.013 Length= 10.4' Slope= 0.0096 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 15R: CB 6



Reach 15R: CB 6

Summary for Reach 16R: CB 5

 Inflow Area =
 53,176 sf, 19.07% Impervious, Inflow Depth > 0.78" for 10-Year event

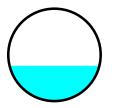
 Inflow =
 0.61 cfs @ 12.25 hrs, Volume=
 3,438 cf

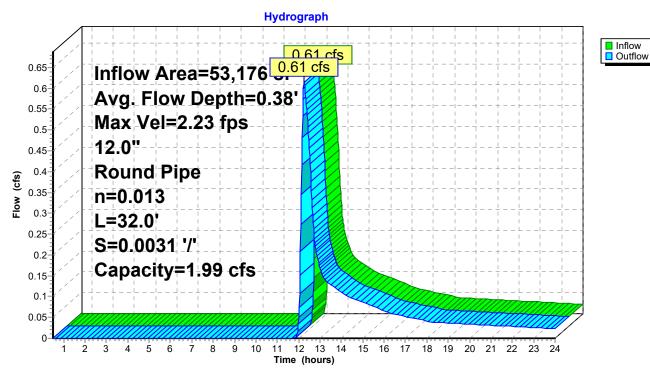
 Outflow =
 0.61 cfs @ 12.26 hrs, Volume=
 3,437 cf, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.23 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.12 fps, Avg. Travel Time= 0.5 min

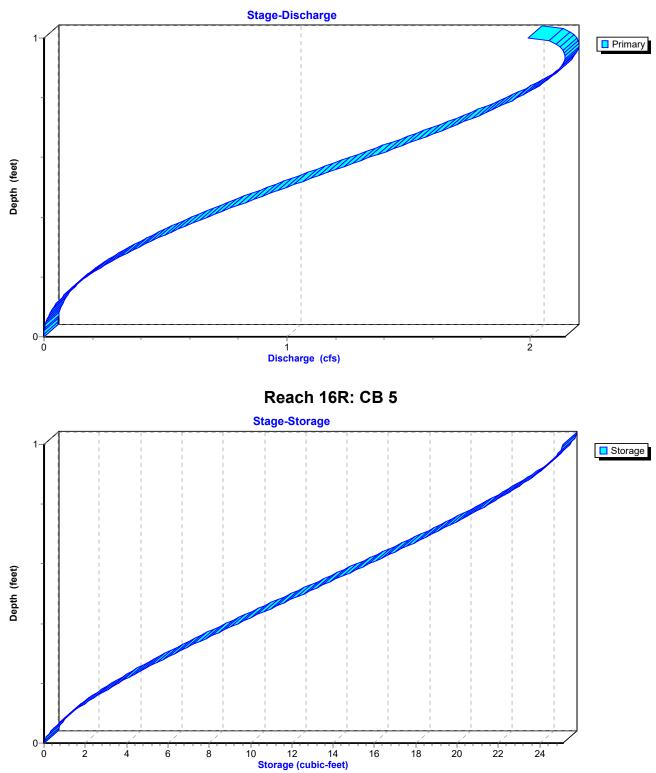
Peak Storage= 9 cf @ 12.26 hrs Average Depth at Peak Storage= 0.38' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 1.99 cfs

12.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0031 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 16R: CB 5



Reach 16R: CB 5

Summary for Reach 17R: DMH 7

 Inflow Area =
 67,342 sf, 25.85% Impervious, Inflow Depth > 1.06" for 10-Year event

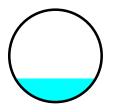
 Inflow =
 1.18 cfs @ 12.18 hrs, Volume=
 5,944 cf

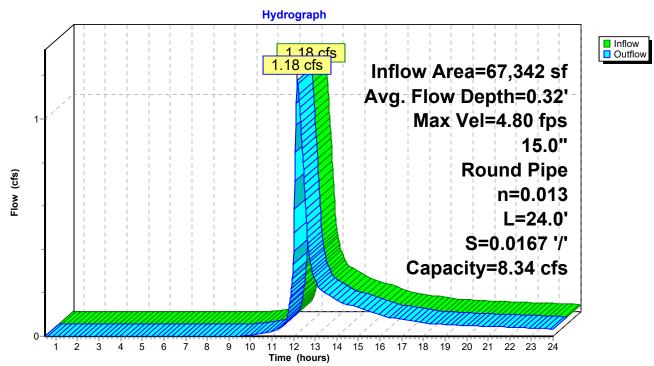
 Outflow =
 1.18 cfs @ 12.18 hrs, Volume=
 5,943 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.80 fps, Min. Travel Time= 0.1 min Avg. Velocity = 2.08 fps, Avg. Travel Time= 0.2 min

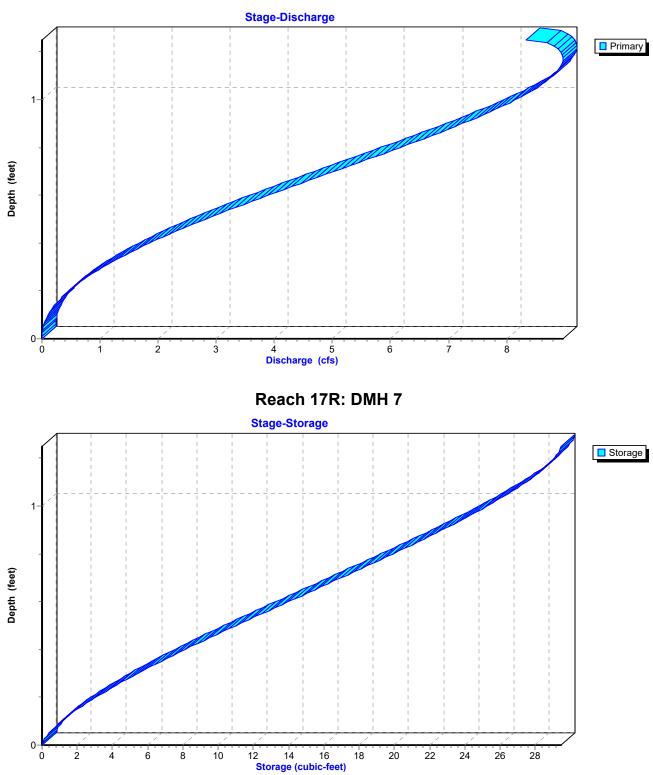
Peak Storage= 6 cf @ 12.18 hrs Average Depth at Peak Storage= 0.32' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 8.34 cfs

15.0" Round Pipe n= 0.013 Length= 24.0' Slope= 0.0167 '/' Inlet Invert= 67.40', Outlet Invert= 67.00'





Reach 17R: DMH 7



Reach 17R: DMH 7

Summary for Reach 18R: CB 2

 Inflow Area =
 11,067 sf, 74.80% Impervious, Inflow Depth > 3.18" for 10-Year event

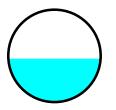
 Inflow =
 0.94 cfs @
 12.09 hrs, Volume=
 2,937 cf

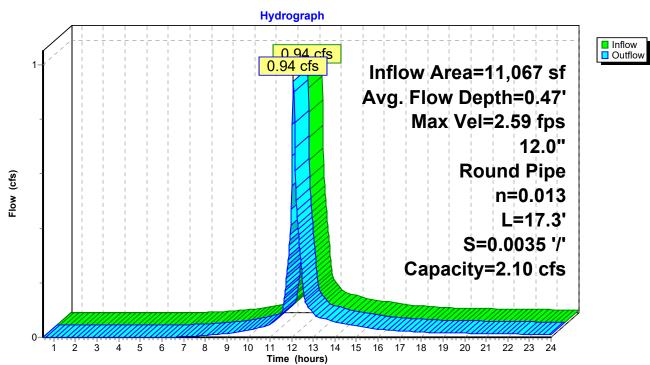
 Outflow =
 0.94 cfs @
 12.09 hrs, Volume=
 2,937 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.59 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.90 fps, Avg. Travel Time= 0.3 min

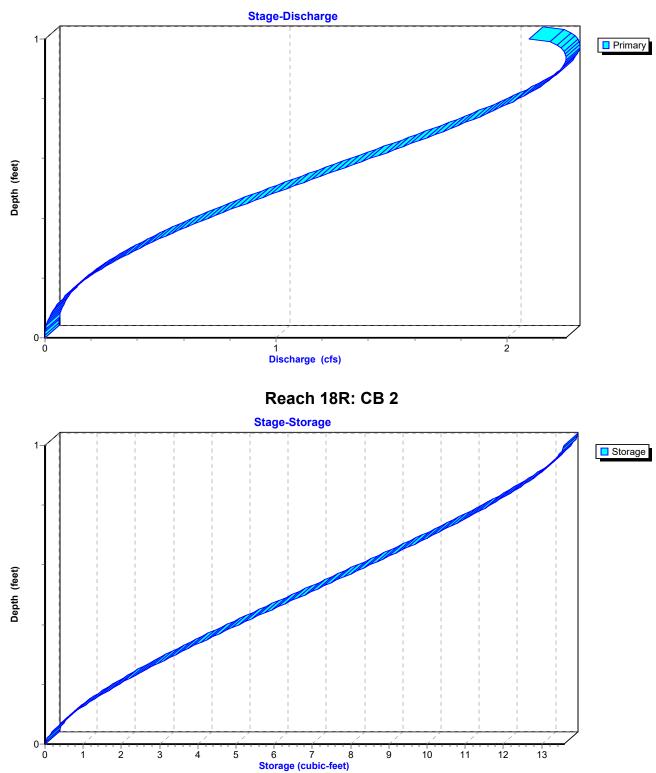
Peak Storage= 6 cf @ 12.09 hrs Average Depth at Peak Storage= 0.47' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.10 cfs

12.0" Round Pipe n= 0.013 Length= 17.3' Slope= 0.0035 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 18R: CB 2



Reach 18R: CB 2

Summary for Reach 19R: CB 1

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 1.39" for 10-Year event

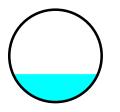
 Inflow =
 0.81 cfs @ 12.13 hrs, Volume=
 2,956 cf

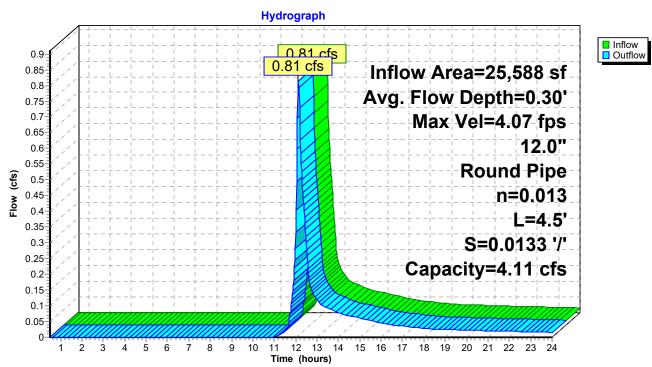
 Outflow =
 0.81 cfs @ 12.13 hrs, Volume=
 2,956 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.07 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.68 fps, Avg. Travel Time= 0.0 min

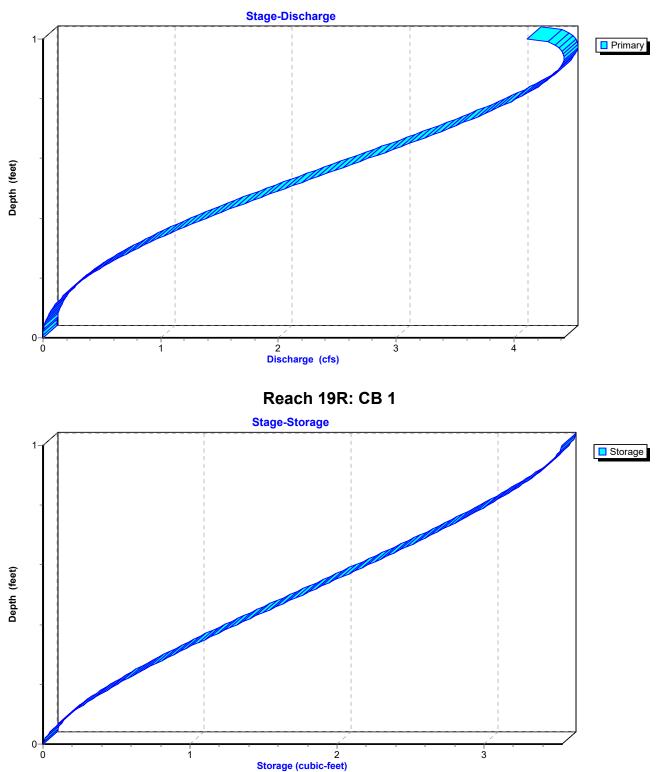
Peak Storage= 1 cf @ 12.13 hrs Average Depth at Peak Storage= 0.30' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 4.11 cfs

12.0" Round Pipe n= 0.013 Length= 4.5' Slope= 0.0133 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 19R: CB 1



Reach 19R: CB 1

Summary for Reach 20R: DMH 3

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 1.39" for 10-Year event

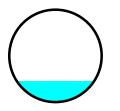
 Inflow =
 0.81 cfs @ 12.13 hrs, Volume=
 2,956 cf

 Outflow =
 0.81 cfs @ 12.13 hrs, Volume=
 2,955 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 3.89 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.60 fps, Avg. Travel Time= 0.3 min

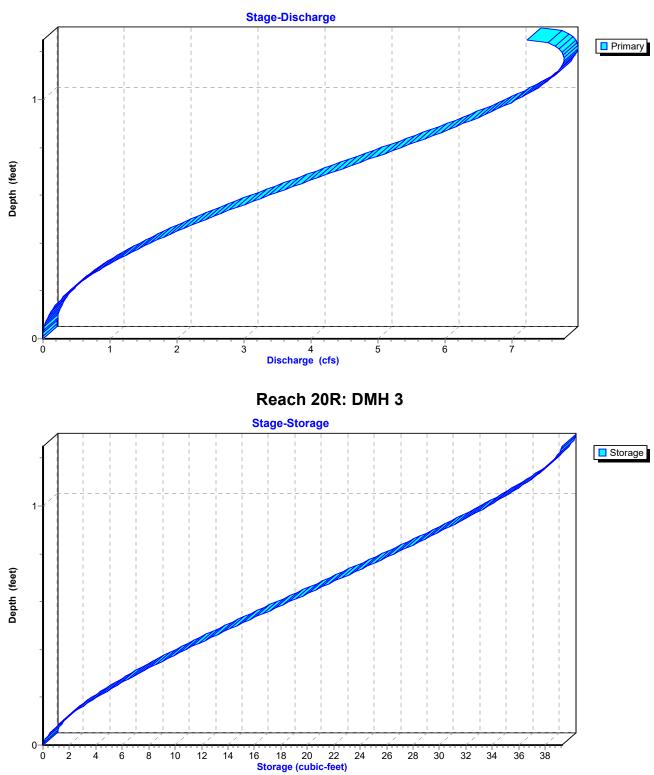
Peak Storage= 7 cf @ 12.13 hrs Average Depth at Peak Storage= 0.28' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 7.22 cfs

15.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0125 '/' Inlet Invert= 66.40', Outlet Invert= 66.00'



Hydrograph Inflow Outflow 0.81 cfs 0.9 0.81 cfs Inflow Area=25,588 sf 0.85 0.8 Avg. Flow Depth=0.28' 0.75 0.7 Max Vel=3.89 fps 0.65 15.0" 0.6 0.55 **Round Pipe** (cfs) 0.5 n=0.013 Flow 0.45 0.4 L=32.0' 0.35 S=0.0125 '/' 0.3 0.25 Capacity=7.22 cfs 0.2 0.15 0.1 0.05 0 Ż Ś 10 12 13 14 15 16 17 18 19 20 21 22 23 24 1 5 6 8 9 11 Time (hours)

Reach 20R: DMH 3



Reach 20R: DMH 3

Summary for Pond 11P: BASIN 1

Inflow Area =	95,314 sf, 22.44% Impervious,	Inflow Depth > 1.06" for 10-Year event
Inflow =	1.76 cfs @ 12.11 hrs, Volume=	8,448 cf
Outflow =	0.18 cfs @ 14.82 hrs, Volume=	6,465 cf, Atten= 90%, Lag= 162.2 min
Discarded =	0.14 cfs @ 14.82 hrs, Volume=	6,304 cf
Primary =	0.04 cfs @ 14.82 hrs, Volume=	161 cf

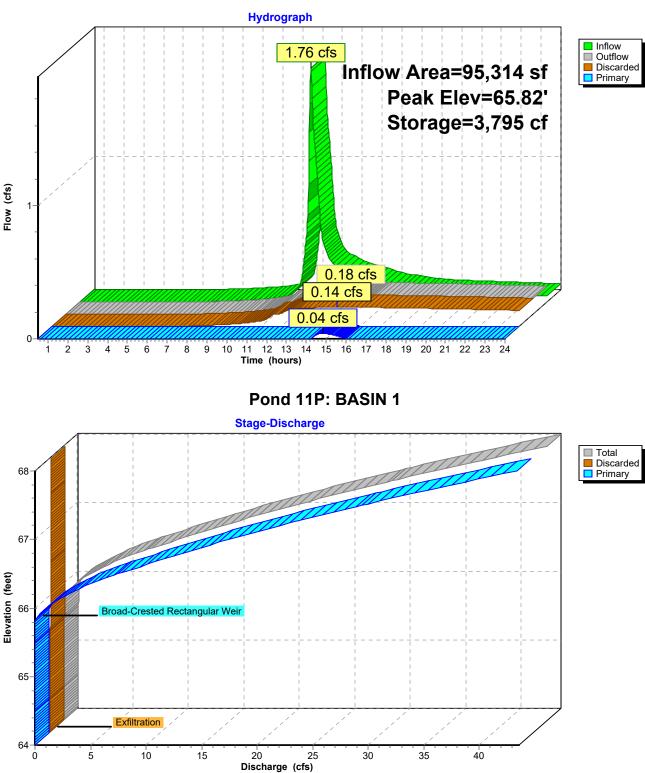
Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 65.82' @ 14.82 hrs Surf.Area= 2,576 sf Storage= 3,795 cf

Plug-Flow detention time= 263.2 min calculated for 6,459 cf (76% of inflow) Center-of-Mass det. time= 170.4 min (1,037.6 - 867.2)

Volume	Inver	t Avail.Sto	rage Storag	e Description	
#1	64.00)' 10,88	30 cf Custo	m Stage Data (P	rismatic)Listed below
	_				
Elevatio		Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
64.0	00	1,611	0	0	
64.5	50	1,857	867	867	
65.0	00	2,118	994	1,861	
65.5	50	2,392	1,128	2,988	
66.0	00	2,681	1,268	4,257	
66.5	50	2,984	1,416	5,673	
67.0	00	3,301	1,571	7,244	
67.5	50	3,632	1,733	8,977	
68.0	00	3,977	1,902	10,880	
		,			
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	65.80'	4.0' long x	0.5' breadth Bro	ad-Crested Rectangular Weir
	-			0.20 0.40 0.60	
			()	sh) 2.80 2.92 3.	
#2	Discarded	64.00'	(U	Exfiltration over	
.			<u> </u>		

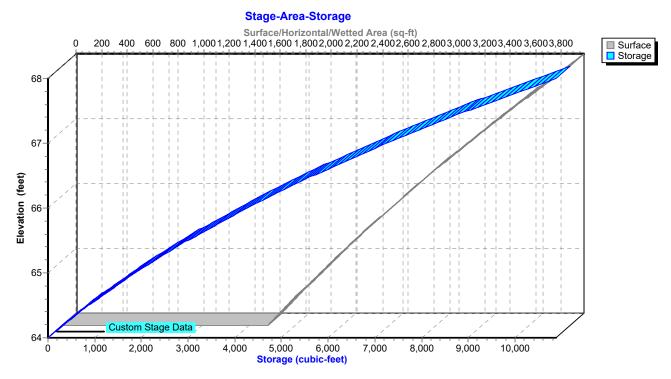
Discarded OutFlow Max=0.14 cfs @ 14.82 hrs HW=65.82' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.14 cfs)

Primary OutFlow Max=0.03 cfs @ 14.82 hrs HW=65.82' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.03 cfs @ 0.37 fps)



Pond 11P: BASIN 1

Pond 11P: BASIN 1



Summary for Pond 13P: BASIN 2

Inflow Area =	80,249 sf, 24.63% Impervious,	Inflow Depth > 1.05" for 10-Year event
Inflow =	1.42 cfs @ 12.16 hrs, Volume=	7,025 cf
Outflow =	0.17 cfs @ 14.58 hrs, Volume=	7,000 cf, Atten= 88%, Lag= 145.1 min
Discarded =	0.17 cfs @ 14.58 hrs, Volume=	7,000 cf
Primary =	0.00 cfs $\overline{@}$ 0.50 hrs, Volume=	0 cf

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 66.07' @ 14.58 hrs Surf.Area= 3,077 sf Storage= 2,673 cf

Plug-Flow detention time= 170.4 min calculated for 6,994 cf (100% of inflow) Center-of-Mass det. time= 168.3 min (1,049.6 - 881.3)

Volume	Inver	t Avail.Sto	rage Storage	e Description	
#1	65.10	' 9,9 ⁻	10 cf Custor	n Stage Data (Pr	ismatic)Listed below
Flovetic		f. A	In a Ctara	Curra Charra	
Elevatio		urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
65.´	10	2,409	0	0	
65.5	50	2,714	1,025	1,025	
66.0	00	3,033	1,437	2,461	
66.5	50	3,366	1,600	4,061	
67.0	00	3,714	1,770	5,831	
67.5	50	4,075	1,947	7,778	
68.0	00	4,451	2,132	9,910	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	67.00'	4.0' long x ().5' breadth Broa	ad-Crested Rectangular Weir
	-		Head (feet)	0.20 0.40 0.60	0.80 1.00
			Coef. (Englis	h) 2.80 2.92 3.0	08 3.30 3.32
#2	Discarded	65.10'	2.410 in/hr E	xfiltration over	Surface area
Discord	ad OutElay	$\sqrt{M_{OV}-0.17}$ of	~ 0.1158 hrs	HM = 66.07' (Er	ee Discharge)

Discarded OutFlow Max=0.17 cfs @ 14.58 hrs HW=66.07' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.17 cfs)

Primary OutFlow Max=0.00 cfs @ 0.50 hrs HW=65.10' (Free Discharge) —1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Discharge (cfs)

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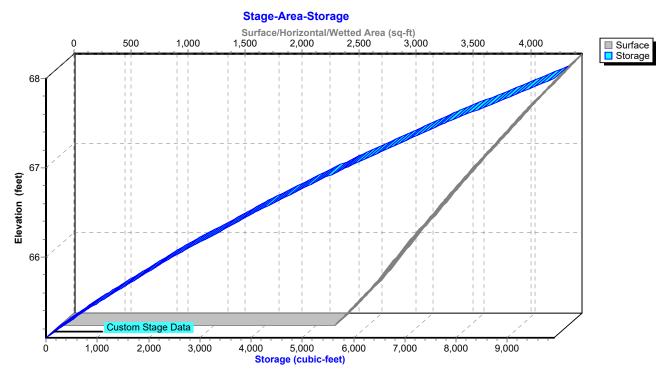
12

13

Hydrograph Inflow
 Outflow 1.42 cfs Inflow Area=80,249 sf Discarded Primary Peak Elev=66.07' Storage=2,673 cf Flow (cfs) 0 17 cfs 0.17 cfs 0.00 cfs 0-4 1 2 11 12 13 14 15 16 17 18 19 20 21 22 23 24 ż ģ 4 5 6 7 8 10 Time (hours) Pond 13P: BASIN 2 Stage-Discharge Total Discarded 68 Primary Broad-Crested Rectangular Weir 67 Elevation (feet) 66-Exfiltration 2 3

Pond 13P: BASIN 2

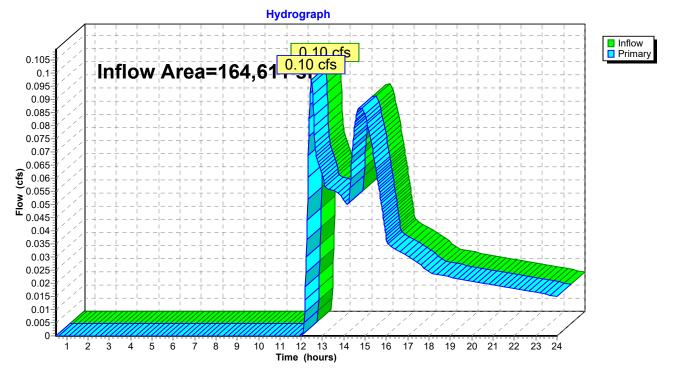
Pond 13P: BASIN 2



Summary for Link 12L: Southwest Wetland

Inflow Area	a =	164,611 sf,	13.58% Impervious,	Inflow Depth >	0.11"	for 10-Year event
Inflow	=	0.10 cfs @	12.48 hrs, Volume=	1,523 c	f	
Primary	=	0.10 cfs @	12.48 hrs, Volume=	1,523 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs

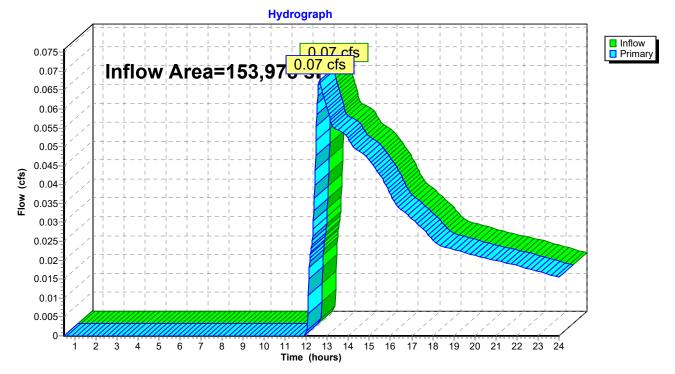


Link 12L: Southwest Wetland

Summary for Link 14L: Northwest Wetland

Inflow Area	a =	153,978 sf,	13.53% Impervious,	Inflow Depth >	0.10"	for 10-Year event
Inflow	=	0.07 cfs @	12.64 hrs, Volume=	1,342 c	f	
Primary	=	0.07 cfs @	12.64 hrs, Volume=	1,342 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 14L: Northwest Wetland

Post	Тур
Prepared by {enter your company name here}	
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Solutio	ns LL(

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=20,844 sf 0.00% Impervious Runoff Depth>0.59" Flow Length=319' Tc=10.0 min CN=44 Runoff=0.14 cfs 1,023 cf
Subcatchment2: Subcat2	Runoff Area=25,588 sf 31.23% Impervious Runoff Depth>1.98" Flow Length=288' Tc=8.4 min CN=64 Runoff=1.21 cfs 4,219 cf
Subcatchment3: Subcat3	Runoff Area=58,660 sf 8.73% Impervious Runoff Depth>0.88" Flow Length=261' Tc=15.8 min CN=49 Runoff=0.73 cfs 4,321 cf
Subcatchment4: Subcat4	Runoff Area=48,453 sf 1.98% Impervious Runoff Depth>0.43" Flow Length=187' Tc=9.0 min CN=41 Runoff=0.19 cfs 1,741 cf
Subcatchment 5: Subcat 5	Runoff Area=53,176 sf 19.07% Impervious Runoff Depth>1.22" Flow Length=355' Tc=14.3 min CN=54 Runoff=1.12 cfs 5,395 cf
Subcatchment6: Subcat6	Runoff Area=67,481 sf 1.12% Impervious Runoff Depth>0.43" Flow Length=644' Tc=17.9 min CN=41 Runoff=0.24 cfs 2,413 cf
Subcatchment7: Subcat7	Runoff Area=12,907 sf 18.31% Impervious Runoff Depth>1.51" Tc=6.0 min CN=58 Runoff=0.48 cfs 1,625 cf
Subcatchment8: Subcat8	Runoff Area=6,248 sf 5.00% Impervious Runoff Depth>0.70" Tc=6.0 min CN=46 Runoff=0.07 cfs 367 cf
Subcatchment9: Subcat9	Runoff Area=14,166 sf 51.29% Impervious Runoff Depth>2.85" Flow Length=137' Tc=8.6 min CN=74 Runoff=0.99 cfs 3,360 cf
Subcatchment 10: Subcat 10	Runoff Area=11,067 sf 74.80% Impervious Runoff Depth>4.03" Tc=6.0 min CN=86 Runoff=1.18 cfs 3,714 cf
Reach 15R: CB 6 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.36' Max Vel=3.83 fps Inflow=0.99 cfs 3,360 cf L=10.4' S=0.0096 '/' Capacity=3.49 cfs Outflow=0.99 cfs 3,360 cf
Reach 16R: CB 5 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.54' Max Vel=2.61 fps Inflow=1.12 cfs 5,395 cf L=32.0' S=0.0031 '/' Capacity=1.99 cfs Outflow=1.12 cfs 5,394 cf
Reach 17R: DMH 7 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.41' Max Vel=5.51 fps Inflow=1.91 cfs 8,754 cf L=24.0' S=0.0167 '/' Capacity=8.34 cfs Outflow=1.91 cfs 8,753 cf
Reach 18R: CB 2 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.54' Max Vel=2.74 fps Inflow=1.18 cfs 3,714 cf L=17.3' S=0.0035 '/' Capacity=2.10 cfs Outflow=1.18 cfs 3,713 cf
Reach 19R: CB 1 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.37' Max Vel=4.55 fps Inflow=1.21 cfs 4,219 cf L=4.5' S=0.0133 '/' Capacity=4.11 cfs Outflow=1.21 cfs 4,219 cf
Reach 20R: DMH 3	Avg. Flow Depth=0.35' Max Vel=4.36 fps Inflow=1.21 cfs 4,219 cf L=32.0' S=0.0125 '/' Capacity=7.22 cfs Outflow=1.21 cfs 4,219 cf

Post Prepared by {enter your com HydroCAD® 10.00-21 s/n 10276	51	25-Year Rainfall=5.60" Printed 4/30/2018 Page 71
Pond 11P: BASIN 1 Dis	Peak Elev=65.96' Storage=4,157 cf carded=0.15 cfs 6,692 cf Primary=0.72 cfs 2,999 cf	
Pond 13P: BASIN 2	Peak Elev=66.72' Storage=4,824 cf Discarded=0.20 cfs 8,336 cf Primary=0.00 cfs 0 cf	
Link 12L: Southwest Wetland		Inflow=0.93 cfs 5,763 cf Primary=0.93 cfs 5,763 cf
Link 14L: Northwest Wetland		Inflow=0.27 cfs 2,780 cf Primary=0.27 cfs 2,780 cf

Total Runoff Area = 318,589 sf Runoff Volume = 28,177 cf Average Runoff Depth = 1.06" 86.45% Pervious = 275,405 sf 13.55% Impervious = 43,184 sf

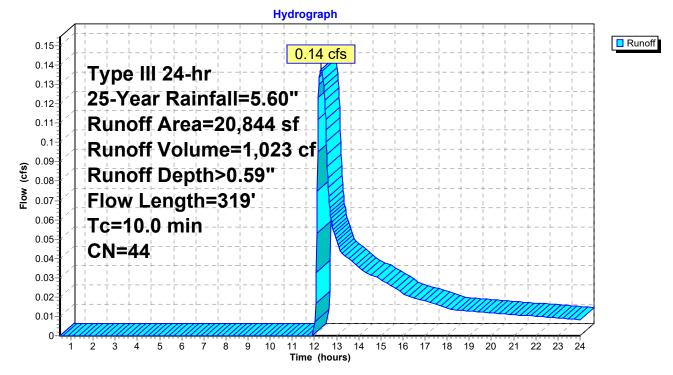
Summary for Subcatchment 1: Subcat 1

Runoff = 0.14 cfs @ 12.31 hrs, Volume= 1,023 cf, Depth> 0.59"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

	Area (sf)	CN	Description		
	12,620	49	50-75% Gra	ass cover, l	Fair, HSG A
	8,223	36	Woods, Fai	r, HSG A	
	20,844	44	Weighted A	verage	
	20,844		100.00% Pe	ervious Are	a
Т		Slope		Capacity	Description
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)	
8.4	4 50	0.0300	0.10		Sheet Flow,
					Grass: Dense n= 0.240 P2= 2.20"
0.	7 148	0.0510	3.64		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
0.9	9 121	0.0190	2.22		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
10.0	D 319	Total			

Subcatchment 1: Subcat 1



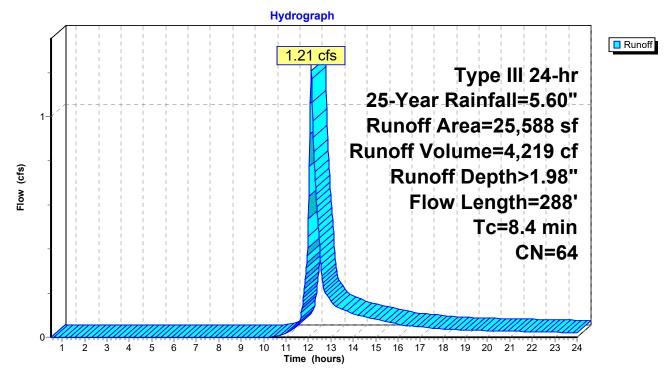
Summary for Subcatchment 2: Subcat 2

Runoff = 1.21 cfs @ 12.13 hrs, Volume= 4,219 cf, Depth> 1.98"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

/	Area (sf)	CN [Description		
	17,077	49 5	50-75% Gra	ass cover, F	Fair, HSG A
	7,991	98 F	Paved road	s w/curbs &	& sewers, HSG A
	520	36 \	Noods, Fai	r, HSG A	
	25,588	64 \	Neighted A	verage	
	17,597	6	58.77% Pei	vious Area	
	7,991	3	31.23% Imp	pervious Ar	ea
Tc	5	Slope	,	Capacity	Description
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)	
6.9	50	0.0500	0.12		Sheet Flow,
					Grass: Dense n= 0.240 P2= 2.20"
0.4	100	0.0600	3.94		Shallow Concentrated Flow,
					Unpaved Kv= 16.1 fps
1.1	138	0.0110	2.13		Shallow Concentrated Flow,
					Paved Kv= 20.3 fps
8.4	288	Total			

Subcatchment 2: Subcat 2



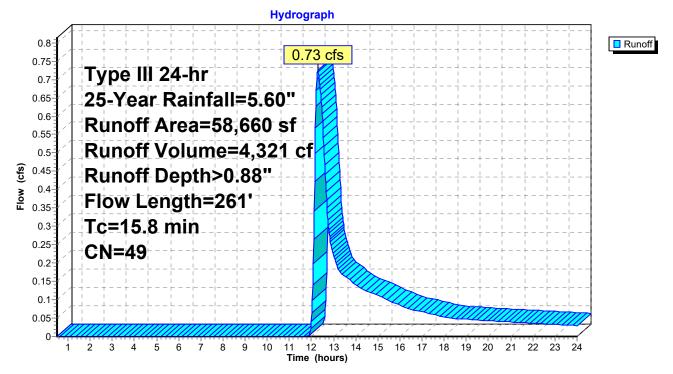
Summary for Subcatchment 3: Subcat 3

Runoff = 0.73 cfs @ 12.29 hrs, Volume= 4,321 cf, Depth> 0.88"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

A	rea (sf)	CN [Description		
	33,711	49 5	50-75% Gra	ass cover, F	Fair, HSG A
	3,296	98 F	Paved road	s w/curbs &	& sewers, HSG A
	1,826	98 F	Roofs, HSG	βA	
	19,827	36 \	Voods, Fai	r, HSG A	
	58,660	49 \	Veighted A	verage	
	53,538	ç	91.27% Per	vious Area	
	5,122	8	8.73% Impe	ervious Are	a
Тс	Length	Slope	Velocity	Capacity	Description
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
			,		Description Sheet Flow,
(min)	(feet)	(ft/ft)	(ft/sec)		
(min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow,
<u>(min)</u> 14.9	(feet) 50	(ft/ft) 0.0200	(ft/sec) 0.06		Sheet Flow, Woods: Light underbrush n= 0.400 P2= 2.20"

Subcatchment 3: Subcat 3



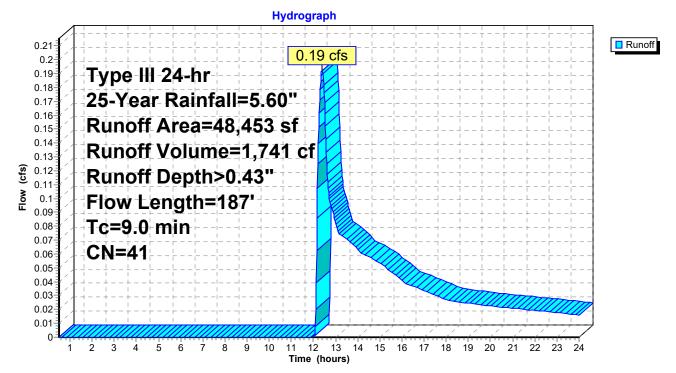
Summary for Subcatchment 4: Subcat 4

Runoff = 0.19 cfs @ 12.38 hrs, Volume= 1,741 cf, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

Area (sf) CN Description						
		12,754	49 5	50-75% Gra	ass cover, F	Fair, HSG A
		959	98 F	Roofs, HSG	βA	
_		34,740	36 V	<u> Voods, Fai</u>	r, HSG A	
48,453 41 Weighted Average					verage	
		47,493	ç	98.02% Per	vious Area	
		959	1	l.98% Impe	ervious Area	a
	Тс	Length	Slope		Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	8.4	50	0.0300	0.10		Sheet Flow,
						Grass: Dense n= 0.240 P2= 2.20"
	0.0	26	0.3100	8.96		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
	0.6	111	0.0410	3.26		Shallow Concentrated Flow,
_						Unpaved Kv= 16.1 fps
	9.0	187	Total			

Subcatchment 4: Subcat 4



Summary for Subcatchment 5: Subcat 5

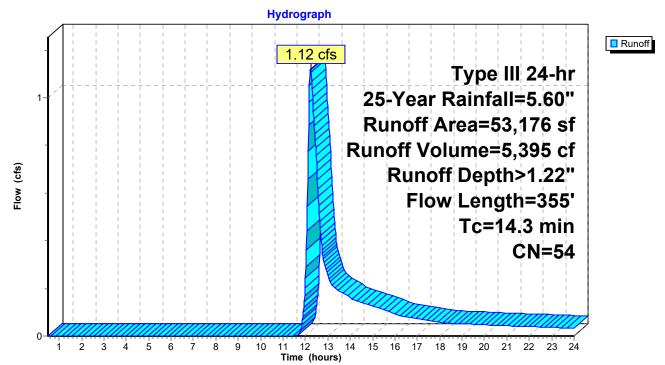
Runoff = 1.12 cfs @ 12.23 hrs, Volume= 5,395 cf, Depth> 1.22"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

	Are	ea (sf)	CN	Description		
	27,303 49 50-75% Grass cover, I				ass cover, F	Fair, HSG A
		7,837	98	Paved road	s w/curbs &	& sewers, HSG A
		2,301	98	Roofs, HSC	βA	
	1	5,734	36	Woods, Fai	r, HSG A	
	5	3,176	54	Weighted A	verage	
	4	3,037		80.93% Pei	vious Area	
	1	0,138		19.07% Imp	pervious Ar	ea
		Length	Slope	,	Capacity	Description
(mi	n)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
12	.3	50	0.0320	0.07		Sheet Flow,
						Woods: Light underbrush n= 0.400 P2= 2.20"
1	.6	248	0.0270	2.65		Shallow Concentrated Flow,
						Unpaved Kv= 16.1 fps
0	.4	57	0.0122	2.24		Shallow Concentrated Flow,
						Paved Kv= 20.3 fps
	~	~	— · ·			

14.3 355 Total

Subcatchment 5: Subcat 5



Summary for Subcatchment 6: Subcat 6

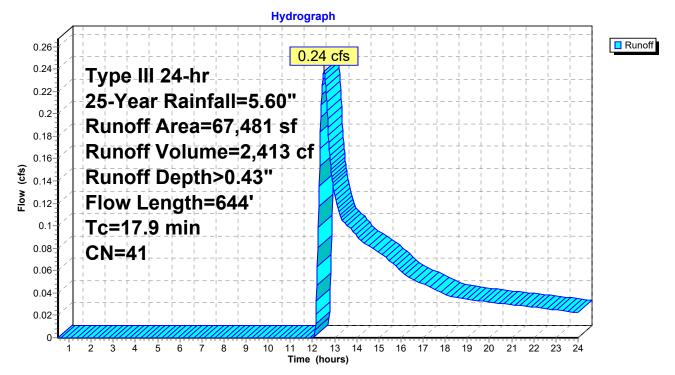
Runoff = 0.24 cfs @ 12.52 hrs, Volume= 2,413 cf, Depth> 0.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

	Area (sf)	CN E	N Description					
24,941 49 50-75% Grass cover, Fair, HSG A								
	754	98 F	Roofs, HSO	βA				
	41,787	36 V						
	67,481	41 V	Veighted A	verage				
	66,727	ç	98.88% Pei	vious Area				
	754	1	.12% Impe	ervious Area	a			
_								
T	0	Slope	Velocity	Capacity	Description			
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)				
14.9	9 50	0.0200	0.06		Sheet Flow,			
					Woods: Light underbrush n= 0.400 P2= 2.20"			
2.2	2 282	0.0170	2.10		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			
0.0	6 245	0.1600	6.44		Shallow Concentrated Flow,			
-					Unpaved Kv= 16.1 fps			
0.2	2 67	0.2100	7.38		Shallow Concentrated Flow,			
					Unpaved Kv= 16.1 fps			

17.9 644 Total

Subcatchment 6: Subcat 6



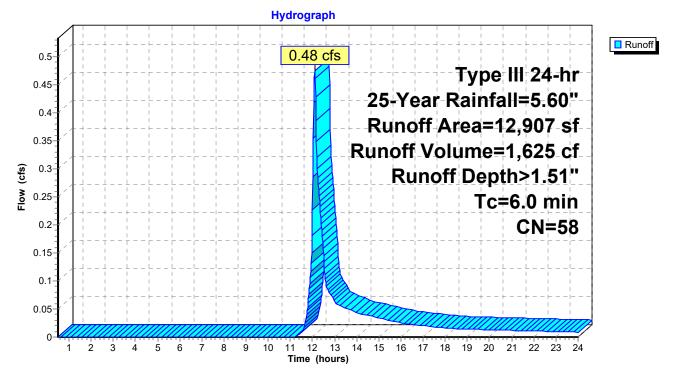
Summary for Subcatchment 7: Subcat 7

Runoff = 0.48 cfs @ 12.10 hrs, Volume= 1,625 cf, Depth> 1.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

A	rea (sf)	CN I	CN Description						
	10,544	49 క	50-75% Grass cover, Fair, HSG A						
	1,337	98 I	Paved road	s w/curbs &	& sewers, HSG A				
	1,026	98 I	Roofs, HSG	βA					
	12,907	58 \	Neighted A						
	10,544	8	31.69% Per	vious Area	a				
	2,363		18.31% Imp	pervious Ar	rea				
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)					
6.0					Direct Entry,				

Subcatchment 7: Subcat 7



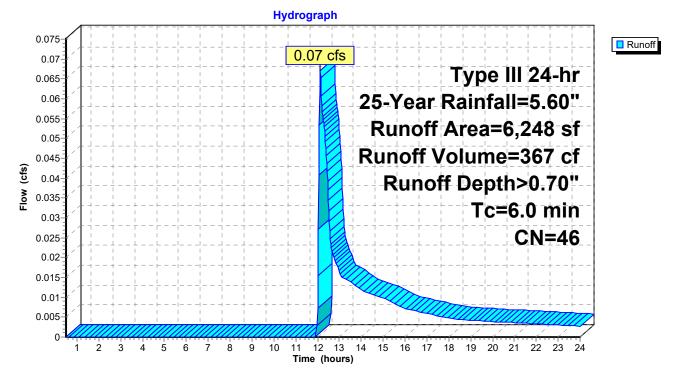
Summary for Subcatchment 8: Subcat 8

Runoff = 0.07 cfs @ 12.13 hrs, Volume= 367 cf, Depth> 0.70"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

A	rea (sf)	CN	Description					
	3,110	49	50-75% Gra	ass cover, F	Fair, HSG A			
	313	98	Roofs, HSG	βA				
	2,825	36	Woods, Fair, HSG A					
	6,248	46	Weighted A	verage				
	5,935		95.00% Per	vious Area	1			
	313		5.00% Impe	ervious Area	a			
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
6.0					Direct Entry,			

Subcatchment 8: Subcat 8



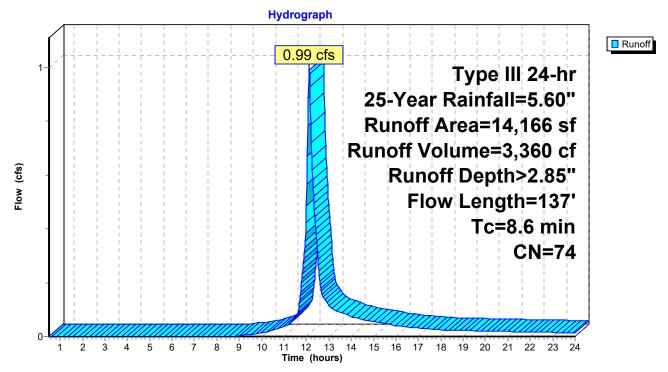
Summary for Subcatchment 9: Subcat 9

Runoff = 0.99 cfs @ 12.12 hrs, Volume= 3,360 cf, Depth> 2.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

	A	rea (sf)	CN [
		6,698	49 5	50-75% Gra	ass cover, F	Fair, HSG A	-			
		6,734	98 F	Paved road	s w/curbs &	& sewers, HSG A				
		532	98 F	Roofs, HSG	βA					
		202	36 \	Voods, Fai	r, HSG A		_			
		14,166	74 \	Veighted A	verage					
		6,900	2	8.71% Per	vious Area	l				
		7,266	5	51.29% Imp	pervious Ar	ea				
	Тс	Length	Slope	Velocity	Capacity	Description				
(r	Tc nin)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description	_			
(r				,		Description Sheet Flow,	-			
(r	nin)	(feet)	(ft/ft)	(ft/sec)			-			
<u>(r</u>	nin)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow,	-			
(r	<u>min)</u> 7.8	<u>(feet)</u> 50	(ft/ft) 0.0360	(ft/sec) 0.11		Sheet Flow, Grass: Dense n= 0.240 P2= 2.20"	-			

Subcatchment 9: Subcat 9



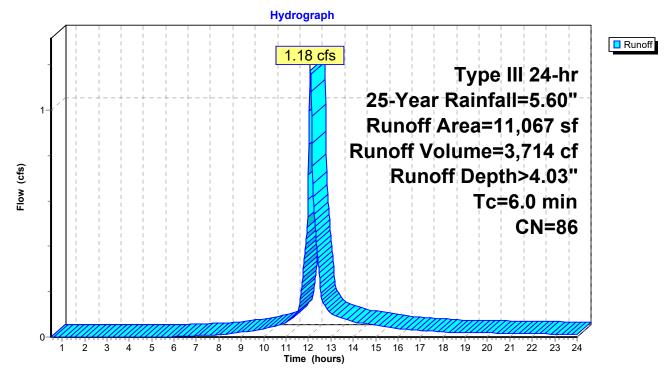
Summary for Subcatchment 10: Subcat 10

Runoff = 1.18 cfs @ 12.09 hrs, Volume= 3,714 cf, Depth> 4.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 25-Year Rainfall=5.60"

Ar	ea (sf)	CN	Description					
	2,766	49	50-75% Grass cover, Fair, HSG A					
	8,278	98	Paved road	s w/curbs &	& sewers, HSG A			
	23	36	Woods, Fair, HSG A					
	11,067	86	Weighted A	verage				
	2,789		25.20% Pervious Area					
	8,278		74.80% Impervious Area					
Tc (min)	Length (feet)	Slope (ft/ft)		Capacity (cfs)	Description			
6.0					Direct Entry,			
			_	_				

Subcatchment 10: Subcat 10



Summary for Reach 15R: CB 6

 Inflow Area =
 14,166 sf, 51.29% Impervious, Inflow Depth > 2.85" for 25-Year event

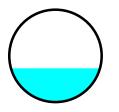
 Inflow =
 0.99 cfs @ 12.12 hrs, Volume=
 3,360 cf

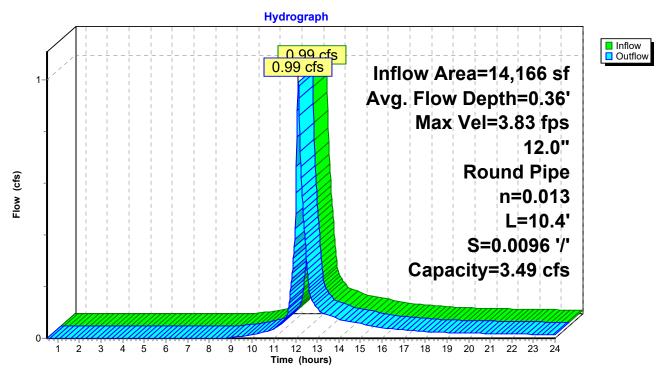
 Outflow =
 0.99 cfs @ 12.12 hrs, Volume=
 3,360 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 3.83 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.43 fps, Avg. Travel Time= 0.1 min

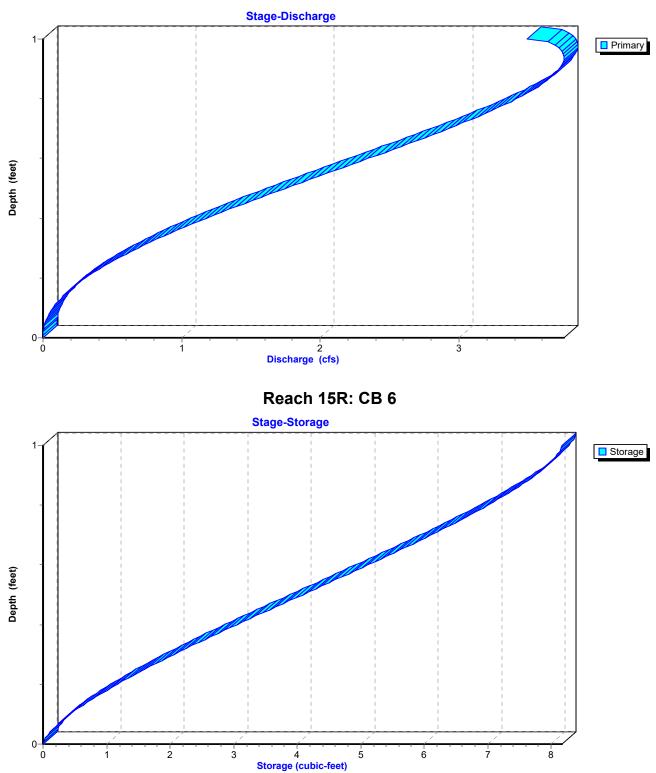
Peak Storage= 3 cf @ 12.12 hrs Average Depth at Peak Storage= 0.36' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.49 cfs

12.0" Round Pipe n= 0.013 Length= 10.4' Slope= 0.0096 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 15R: CB 6



Reach 15R: CB 6

Summary for Reach 16R: CB 5

 Inflow Area =
 53,176 sf, 19.07% Impervious, Inflow Depth > 1.22" for 25-Year event

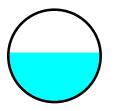
 Inflow =
 1.12 cfs @ 12.23 hrs, Volume=
 5,395 cf

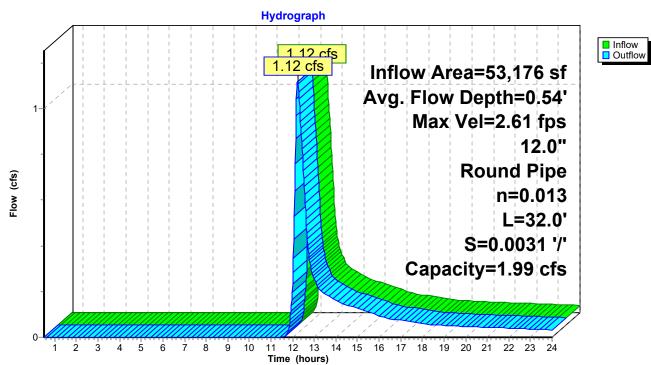
 Outflow =
 1.12 cfs @ 12.23 hrs, Volume=
 5,394 cf, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.61 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.26 fps, Avg. Travel Time= 0.4 min

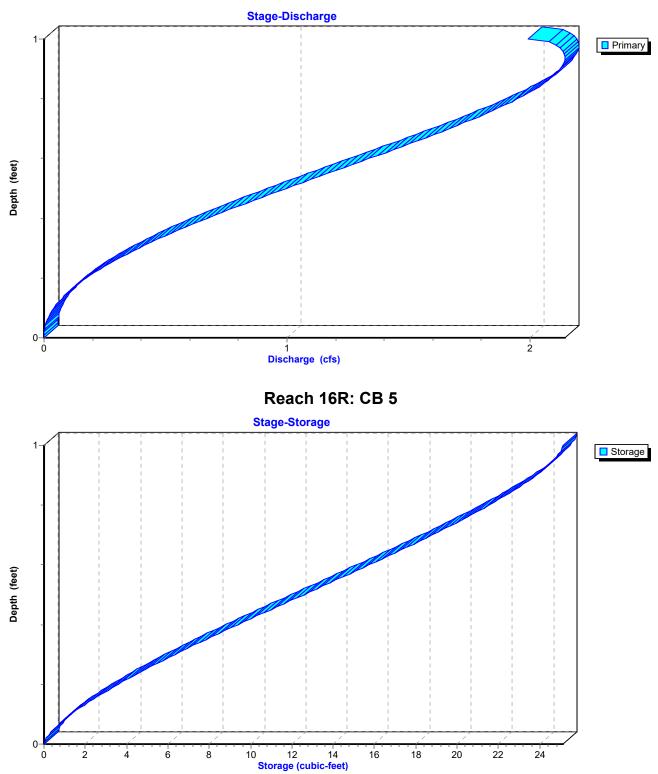
Peak Storage= 14 cf @ 12.23 hrs Average Depth at Peak Storage= 0.54' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 1.99 cfs

12.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0031 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 16R: CB 5



Reach 16R: CB 5

Summary for Reach 17R: DMH 7

 Inflow Area =
 67,342 sf, 25.85% Impervious, Inflow Depth > 1.56" for 25-Year event

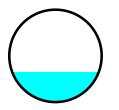
 Inflow =
 1.91 cfs @ 12.17 hrs, Volume=
 8,754 cf

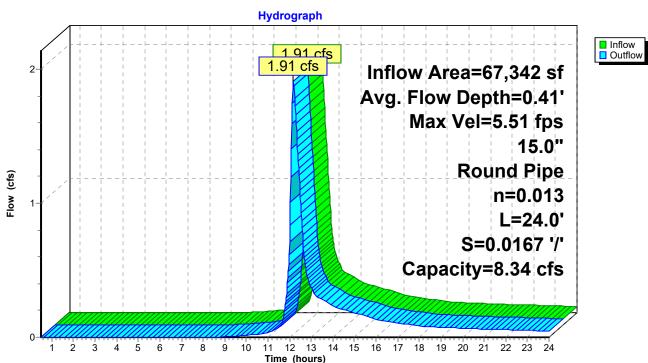
 Outflow =
 1.91 cfs @ 12.18 hrs, Volume=
 8,753 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 5.51 fps, Min. Travel Time= 0.1 min Avg. Velocity = 2.26 fps, Avg. Travel Time= 0.2 min

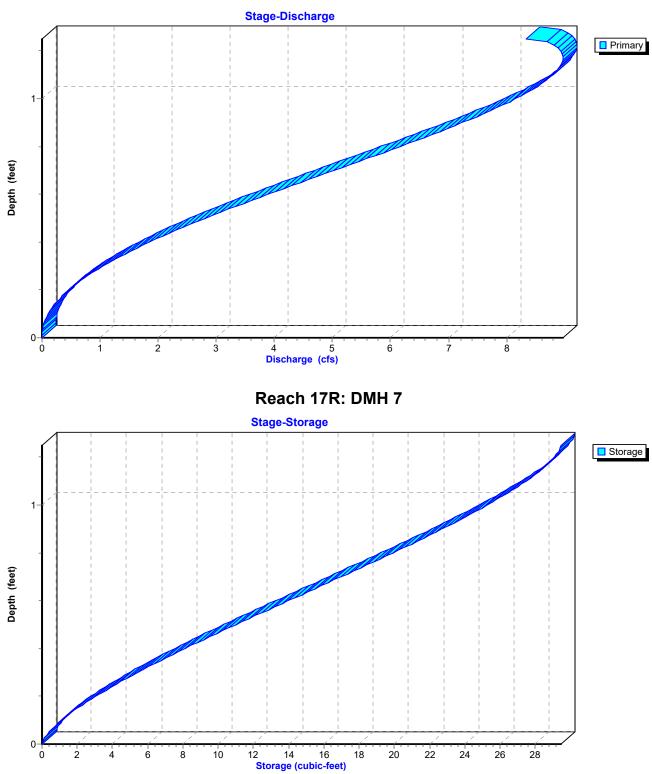
Peak Storage= 8 cf @ 12.18 hrs Average Depth at Peak Storage= 0.41' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 8.34 cfs

15.0" Round Pipe n= 0.013 Length= 24.0' Slope= 0.0167 '/' Inlet Invert= 67.40', Outlet Invert= 67.00'





Reach 17R: DMH 7



Reach 17R: DMH 7

Summary for Reach 18R: CB 2

 Inflow Area =
 11,067 sf, 74.80% Impervious, Inflow Depth > 4.03" for 25-Year event

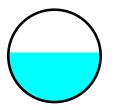
 Inflow =
 1.18 cfs @ 12.09 hrs, Volume=
 3,714 cf

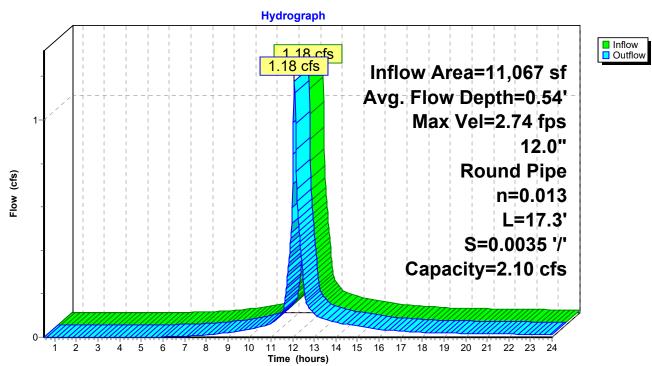
 Outflow =
 1.18 cfs @ 12.09 hrs, Volume=
 3,713 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.74 fps, Min. Travel Time= 0.1 min Avg. Velocity = 0.95 fps, Avg. Travel Time= 0.3 min

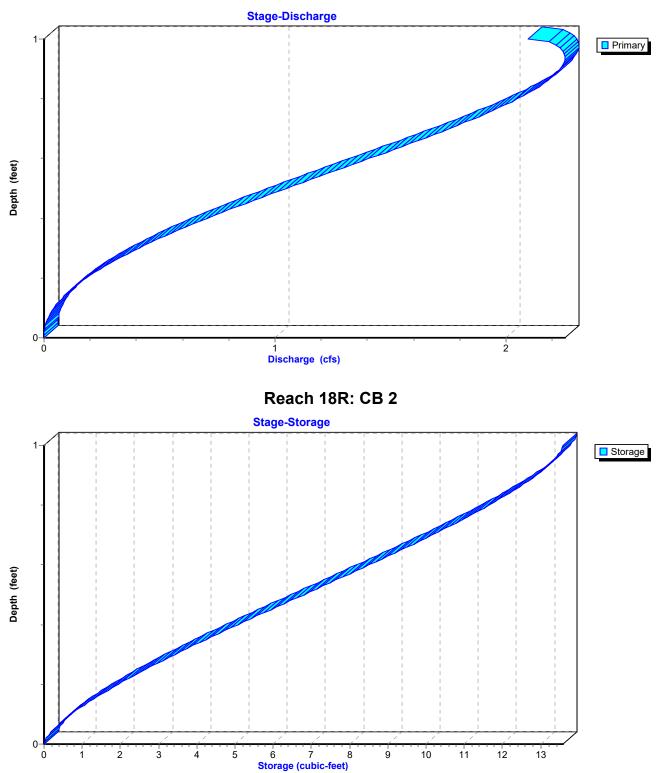
Peak Storage= 7 cf @ 12.09 hrs Average Depth at Peak Storage= 0.54' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.10 cfs

12.0" Round Pipe n= 0.013 Length= 17.3' Slope= 0.0035 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 18R: CB 2



Reach 18R: CB 2

Summary for Reach 19R: CB 1

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 1.98" for 25-Year event

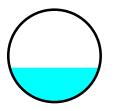
 Inflow =
 1.21 cfs @ 12.13 hrs, Volume=
 4,219 cf

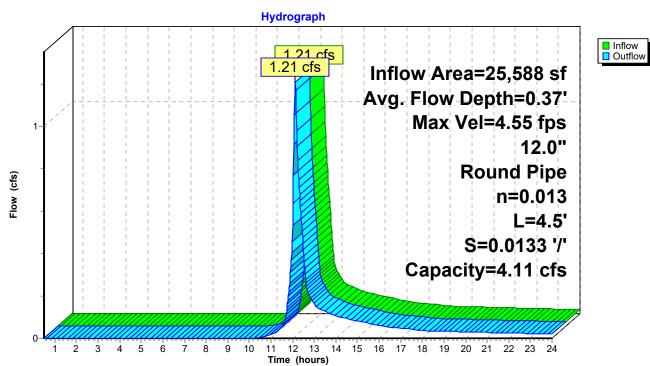
 Outflow =
 1.21 cfs @ 12.13 hrs, Volume=
 4,219 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.55 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.82 fps, Avg. Travel Time= 0.0 min

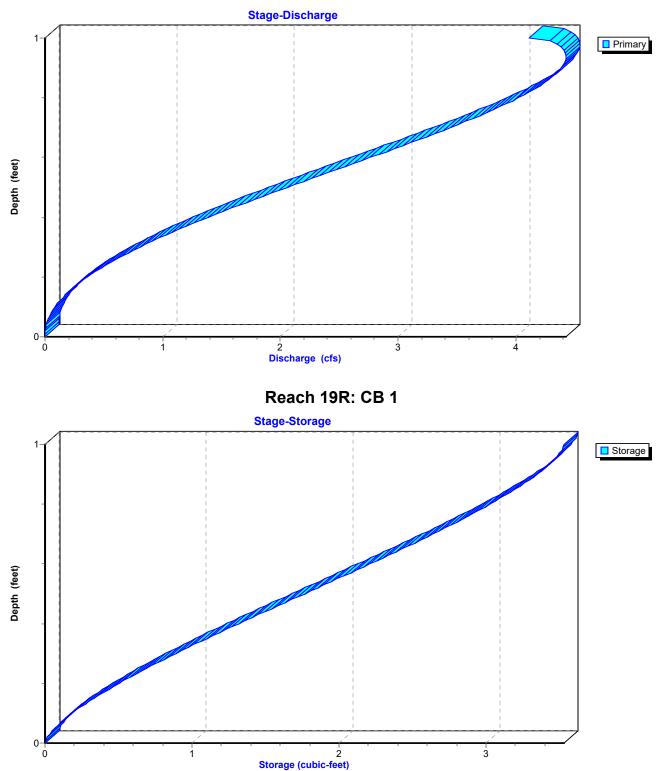
Peak Storage= 1 cf @ 12.13 hrs Average Depth at Peak Storage= 0.37' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 4.11 cfs

12.0" Round Pipe n= 0.013 Length= 4.5' Slope= 0.0133 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 19R: CB 1



Reach 19R: CB 1

Summary for Reach 20R: DMH 3

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 1.98" for 25-Year event

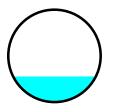
 Inflow =
 1.21 cfs @ 12.13 hrs, Volume=
 4,219 cf

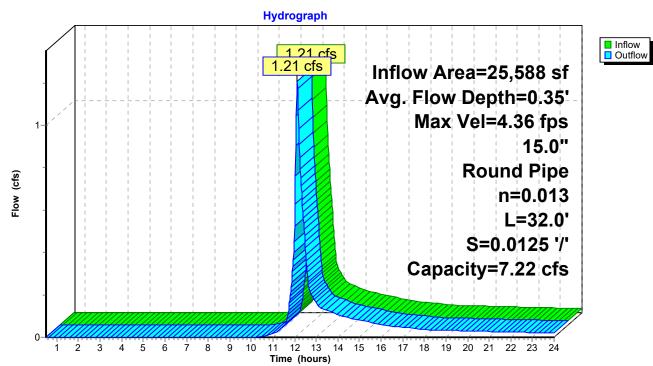
 Outflow =
 1.21 cfs @ 12.13 hrs, Volume=
 4,219 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.36 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.73 fps, Avg. Travel Time= 0.3 min

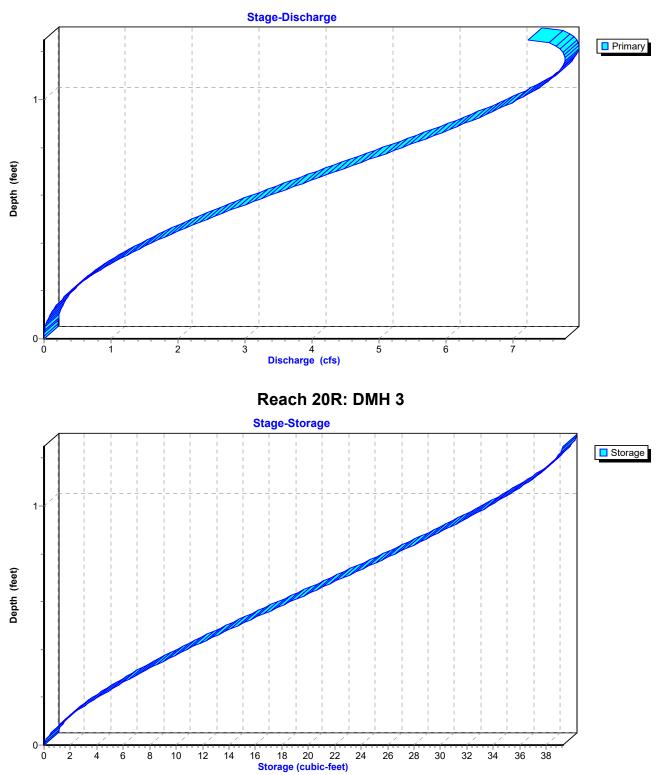
Peak Storage= 9 cf @ 12.13 hrs Average Depth at Peak Storage= 0.35' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 7.22 cfs

15.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0125 '/' Inlet Invert= 66.40', Outlet Invert= 66.00'





Reach 20R: DMH 3



Reach 20R: DMH 3

Summary for Pond 11P: BASIN 1

Inflow Area =	95,314 sf, 22.44% Impervious,	Inflow Depth > 1.54" for 25-Year event
Inflow =	2.63 cfs @ 12.12 hrs, Volume=	12,253 cf
Outflow =	0.87 cfs @ 12.62 hrs, Volume=	9,692 cf, Atten= 67%, Lag= 29.8 min
Discarded =	0.15 cfs @ 12.62 hrs, Volume=	6,692 cf
Primary =	0.72 cfs @ 12.62 hrs, Volume=	2,999 cf

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 65.96' @ 12.62 hrs Surf.Area= 2,658 sf Storage= 4,157 cf

Plug-Flow detention time= 191.1 min calculated for 9,692 cf (79% of inflow) Center-of-Mass det. time= 106.2 min (965.6 - 859.4)

Volume	Inve	rt Avail.Sto	rage Storag	ge Description			
#1	64.00)' 10,88	30 cf Custo	om Stage Data (Prismatic)Listed below			
Elevatio		Surf.Area	Inc.Store				
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
64.0	00	1,611	0	0			
64.5	50	1,857	867	867			
65.0	00	2,118	994	1,861			
65.5	50	2,392	1,128	2,988			
66.0	00	2,681	1,268	4,257			
66.5	50	2,984	1,416	5,673			
67.0	00	3,301	1,571	7,244			
67.5	50	3,632	1,733	8,977			
68.0	00	3,977	1,902	10,880			
Device	Routing	Invert	Outlet Devic	ices			
#1	Primary	65.80'	4.0' long x	x 0.5' breadth Broad-Crested Rectangular Weir			
	-) 0.20 0.40 0.60 0.80 1.00			
			()	, lish) 2.80 2.92 3.08 3.30 3.32			
#2	Discardeo	64.00'		Exfiltration over Surface area			
Dia a and	Discourded OutFlow May-0.45 of @ 40.00 has 104-05.001 (Exc. Discharges)						

Discarded OutFlow Max=0.15 cfs @ 12.62 hrs HW=65.96' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.15 cfs)

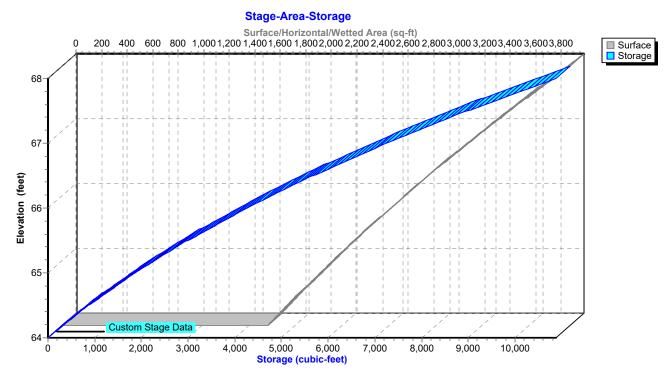
Primary OutFlow Max=0.72 cfs @ 12.62 hrs HW=65.96' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.72 cfs @ 1.12 fps)

Hydrograph Inflow
 Outflow
 Discarded 2.63 cfs Inflow Area=95,314 sf Primary Peak Elev=65.96' Storage=4,157 cf 2-Flow (cfs) 0.87 cfs 1 0.72 cfs 0 0 2 11 12 13 14 15 16 17 18 19 20 21 22 23 24 1 ż ģ 4 5 6 7 8 10 Time (hours) Pond 11P: BASIN 1 Stage-Discharge Total Discarded 68 Primary 67 Elevation (feet) 66-Broad-Crested Rectangular Weir 65 Exfiltration 64 5 10 15 20 25 30 35 40 Ó

Discharge (cfs)

Pond 11P: BASIN 1

Pond 11P: BASIN 1



Summary for Pond 13P: BASIN 2

Inflow Area =	80,249 sf, 24.63% Impervious,	Inflow Depth > 1.55" for 25-Year event
Inflow =	2.28 cfs @ 12.16 hrs, Volume=	10,378 cf
Outflow =	0.20 cfs @ 15.36 hrs, Volume=	8,336 cf, Atten= 91%, Lag= 192.4 min
Discarded =	0.20 cfs @ 15.36 hrs, Volume=	8,336 cf
Primary =	0.00 cfs $\overline{@}$ 0.50 hrs, Volume=	0 cf

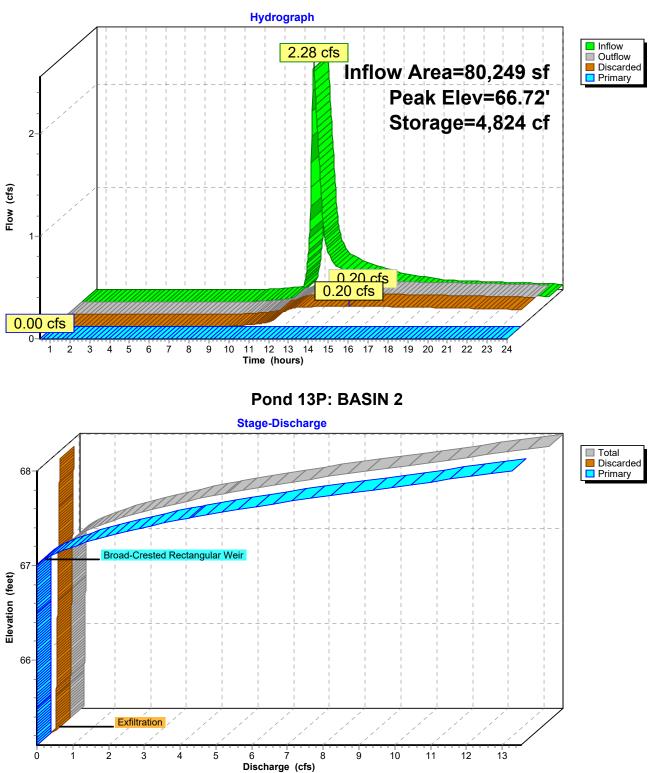
Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 66.72' @ 15.36 hrs Surf.Area= 3,516 sf Storage= 4,824 cf

Plug-Flow detention time= 266.5 min calculated for 8,336 cf (80% of inflow) Center-of-Mass det. time= 185.8 min (1,055.5 - 869.7)

Volume	Inver	t Avail.Sto	rage Storage	e Description				
#1	65.10	' 9,9'	10 cf Custor	n Stage Data (Pr	ismatic)Listed below			
Flovetic		unt Ana a	Inc. Ctore	Curra Chara				
Elevatio		urf.Area	Inc.Store	Cum.Store				
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)				
65.1	10	2,409	0	0				
65.5	50	2,714	1,025	1,025				
66.0	00	3,033	1,437	2,461				
66.5	50	3,366	1,600	4,061				
67.0	00	3,714	1,770	5,831				
67.5	50	4,075	1,947	7,778				
68.0	00	4,451	2,132	9,910				
Device	Routing	Invert	Outlet Device	es				
#1	Primary	67.00'	4.0' long x	0.5' breadth Broa	ad-Crested Rectangular Weir			
			Head (feet)	0.20 0.40 0.60	0.80 1.00			
				sh) 2.80 2.92 3.0				
#2	Discarded	65.10'						
Discourd	Discourded OutFlow Mover 0.20 of a a 15.26 hrs. LINIEG 721 (Free Discharge)							

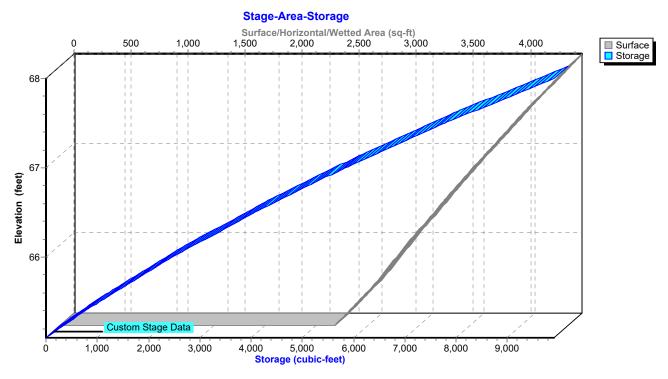
Discarded OutFlow Max=0.20 cfs @ 15.36 hrs HW=66.72' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.20 cfs)

Primary OutFlow Max=0.00 cfs @ 0.50 hrs HW=65.10' (Free Discharge) —1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)



Pond 13P: BASIN 2

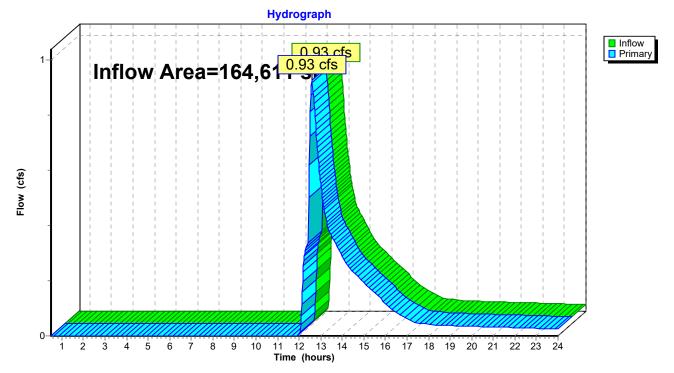
Pond 13P: BASIN 2



Summary for Link 12L: Southwest Wetland

Inflow Are	a =	164,611 sf,	13.58% Impervious,	Inflow Depth >	0.42"	for 25-Year event
Inflow	=	0.93 cfs @	12.59 hrs, Volume=	5,763 c	f	
Primary	=	0.93 cfs @	12.59 hrs, Volume=	5,763 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs

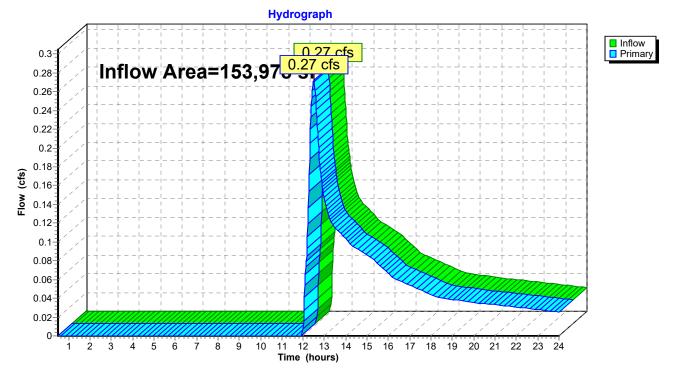


Link 12L: Southwest Wetland

Summary for Link 14L: Northwest Wetland

Inflow Area	a =	153,978 sf,	13.53% Impervious,	Inflow Depth >	0.22"	for 25-Year event
Inflow	=	0.27 cfs @	12.49 hrs, Volume=	2,780 c	f	
Primary	=	0.27 cfs @	12.49 hrs, Volume=	2,780 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 14L: Northwest Wetland

Post	Type III 24-hr	100
Prepared by {enter your company name here}		
HydroCAD® 10.00-21 s/n 10276 © 2018 HydroCAD Software Soluti	ons LLC	

Time span=0.50-24.00 hrs, dt=0.02 hrs, 1176 points Runoff by SCS TR-20 method, UH=SCS, Weighted-CN Reach routing by Stor-Ind method - Pond routing by Stor-Ind method

Subcatchment1: Subcat1	Runoff Area=20,844 sf 0.00% Impervious Runoff Depth>1.15" Flow Length=319' Tc=10.0 min CN=44 Runoff=0.40 cfs 1,999 cf
Subcatchment2: Subcat2	Runoff Area=25,588 sf 31.23% Impervious Runoff Depth>3.00" Flow Length=288' Tc=8.4 min CN=64 Runoff=1.87 cfs 6,388 cf
Subcatchment3: Subcat3	Runoff Area=58,660 sf 8.73% Impervious Runoff Depth>1.57" Flow Length=261' Tc=15.8 min CN=49 Runoff=1.55 cfs 7,678 cf
Subcatchment4: Subcat4	Runoff Area=48,453 sf 1.98% Impervious Runoff Depth>0.91" Flow Length=187' Tc=9.0 min CN=41 Runoff=0.63 cfs 3,693 cf
Subcatchment 5: Subcat 5	Runoff Area=53,176 sf 19.07% Impervious Runoff Depth>2.02" Flow Length=355' Tc=14.3 min CN=54 Runoff=2.05 cfs 8,963 cf
Subcatchment6: Subcat6	Runoff Area=67,481 sf 1.12% Impervious Runoff Depth>0.91" Flow Length=644' Tc=17.9 min CN=41 Runoff=0.73 cfs 5,125 cf
Subcatchment7: Subcat7	Runoff Area=12,907 sf 18.31% Impervious Runoff Depth>2.41" Tc=6.0 min CN=58 Runoff=0.80 cfs 2,588 cf
Subcatchment8: Subcat8	Runoff Area=6,248 sf 5.00% Impervious Runoff Depth>1.32" Tc=6.0 min CN=46 Runoff=0.17 cfs 686 cf
Subcatchment9: Subcat9	Runoff Area=14,166 sf 51.29% Impervious Runoff Depth>4.04" Flow Length=137' Tc=8.6 min CN=74 Runoff=1.41 cfs 4,764 cf
Subcatchment 10: Subcat 10	Runoff Area=11,067 sf 74.80% Impervious Runoff Depth>5.36" Tc=6.0 min CN=86 Runoff=1.54 cfs 4,944 cf
Reach 15R: CB 6 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.44' Max Vel=4.21 fps Inflow=1.41 cfs 4,764 cf L=10.4' S=0.0096 '/' Capacity=3.49 cfs Outflow=1.41 cfs 4,764 cf
Reach 16R: CB 5 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.85' Max Vel=2.89 fps Inflow=2.05 cfs 8,963 cf L=32.0' S=0.0031 '/' Capacity=1.99 cfs Outflow=2.05 cfs 8,961 cf
Reach 17R: DMH 7 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.54' Max Vel=6.34 fps Inflow=3.18 cfs 13,725 cf L=24.0' S=0.0167 '/' Capacity=8.34 cfs Outflow=3.18 cfs 13,724 cf
Reach 18R: CB 2 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.64' Max Vel=2.92 fps Inflow=1.54 cfs 4,944 cf L=17.3' S=0.0035 '/' Capacity=2.10 cfs Outflow=1.54 cfs 4,944 cf
Reach 19R: CB 1 12.0" Round Pipe n=0.013	Avg. Flow Depth=0.47' Max Vel=5.11 fps Inflow=1.87 cfs 6,388 cf 3 L=4.5' S=0.0133 '/' Capacity=4.11 cfs Outflow=1.87 cfs 6,388 cf
Reach 20R: DMH 3 15.0" Round Pipe n=0.013	Avg. Flow Depth=0.43' Max Vel=4.94 fps Inflow=1.87 cfs 6,388 cf L=32.0' S=0.0125 '/' Capacity=7.22 cfs Outflow=1.87 cfs 6,388 cf

Post Prepared by {enter your <u>HydroCAD® 10.00-21_s/n 1</u>	r company name here} 0276 © 2018 HydroCAD Software Solut	Type III 24-hr 100-Year Rainfall=7.00" Printed 4/30/2018 ions LLC Page 103
Pond 11P: BASIN 1		'' Storage=4,750 cf Inflow=4.28 cfs 19,009 cf 2.67 cfs 8,619 cf Outflow=2.82 cfs 15,749 cf
Pond 13P: BASIN 2		5' Storage=6,419 cf Inflow=3.80 cfs 16,312 cf 0.66 cfs 3,252 cf Outflow=0.87 cfs 12,592 cf
Link 12L: Southwest We	tland	Inflow=3.50 cfs 14,312 cf Primary=3.50 cfs 14,312 cf
Link 14L: Northwest We	tland	Inflow=1.13 cfs 9,063 cf Primary=1.13 cfs 9,063 cf

Total Runoff Area = 318,589 sf Runoff Volume = 46,829 cf Average Runoff Depth = 1.76" 86.45% Pervious = 275,405 sf 13.55% Impervious = 43,184 sf

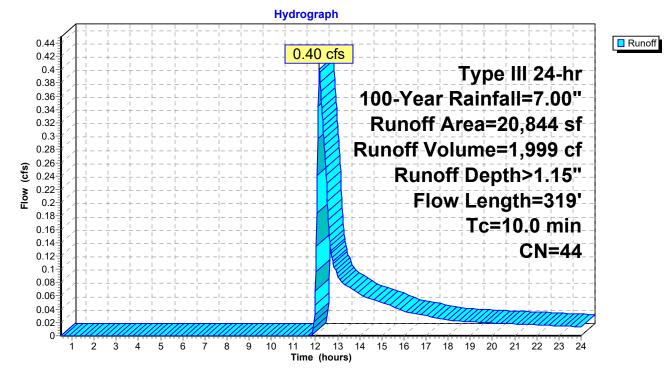
Summary for Subcatchment 1: Subcat 1

Runoff = 0.40 cfs @ 12.18 hrs, Volume= 1,999 cf, Depth> 1.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

_	A	rea (sf)	CN	CN Description						
		12,620	49	49 50-75% Grass cover, Fair, HSG A						
_		8,223	36	<u>Woods, Fai</u>	r, HSG A					
		20,844	44	44 Weighted Average						
		20,844		100.00% Pe	ervious Are	a				
	Тс	Length	Slope	,	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	8.4	50	0.0300	0.10		Sheet Flow,				
						Grass: Dense n= 0.240 P2= 2.20"				
	0.7	148	0.0510	3.64		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.9	121	0.0190	2.22		Shallow Concentrated Flow,				
_						Unpaved Kv= 16.1 fps				
	10.0	319	Total							

Subcatchment 1: Subcat 1



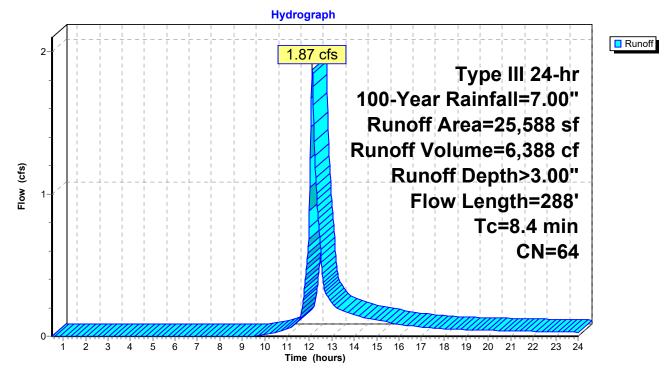
Summary for Subcatchment 2: Subcat 2

Runoff = 1.87 cfs @ 12.12 hrs, Volume= 6,388 cf, Depth> 3.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

/	Area (sf)	CN [N Description						
	17,077	49 5	49 50-75% Grass cover, Fair, HSG A						
	7,991	98 F	98 Paved roads w/curbs & sewers, HSG A						
	520	36 \	Woods, Fair, HSG A						
	25,588	64 \	Neighted A	verage					
17,597 68.77% Pervious Area									
	7,991	3	31.23% Imp	pervious Ar	ea				
Tc	5	Slope	,	Capacity	Description				
<u>(min)</u>	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.9	50	0.0500	0.12		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 2.20"				
0.4	100	0.0600	3.94		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
1.1	138	0.0110	2.13		Shallow Concentrated Flow,				
					Paved Kv= 20.3 fps				
8.4	288	Total							

Subcatchment 2: Subcat 2



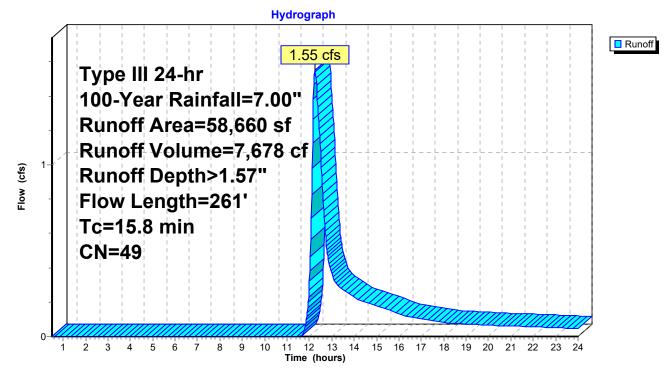
Summary for Subcatchment 3: Subcat 3

Runoff = 1.55 cfs @ 12.25 hrs, Volume= 7,678 cf, Depth> 1.57"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

A	rea (sf)	CN [Description						
	33,711	49 5	19 50-75% Grass cover, Fair, HSG A						
	3,296	98 F	Paved roads w/curbs & sewers, HSG A						
	1,826	98 F	Roofs, HSG A						
	19,827	36 \	6 Woods, Fair, HSG A						
	58,660	49 \	Veighted A	verage					
	53,538	91.27% Pervious Area							
	5,122	8	8.73% Impe	ervious Are	a				
Tc	Length	Slope	Velocity	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
14.9	50	0.0200	0.06		Sheet Flow,				
					Woods: Light underbrush n= 0.400 P2= 2.20"				
0.9	211	0.0580	3.88		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
15.8	261	Total							

Subcatchment 3: Subcat 3



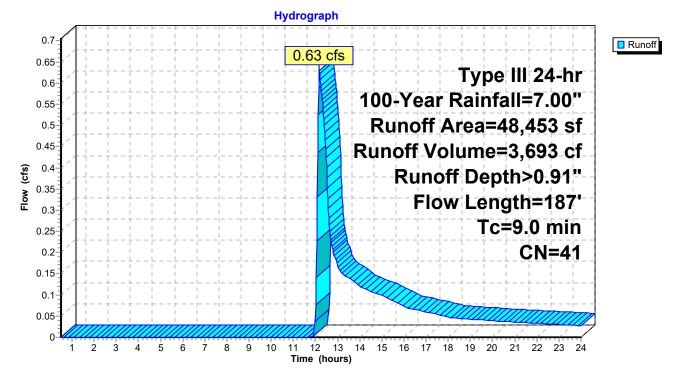
Summary for Subcatchment 4: Subcat 4

Runoff = 0.63 cfs @ 12.18 hrs, Volume= 3,693 cf, Depth> 0.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

 A	rea (sf)	CN I	CN Description						
	12,754	49 క	50-75% Gra	ass cover, F	Fair, HSG A				
	959	98 I	Roofs, HSG A						
	34,740	36 \	Woods, Fair, HSG A						
	48,453	41 \	Neighted A	verage					
	47,493	ę	98.02% Pei	vious Area					
	959		1.98% Impe	ervious Area	а				
Тс	Length	Slope	Velocity	Capacity	Description				
 (min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
8.4	50	0.0300	0.10		Sheet Flow,				
					Grass: Dense n= 0.240 P2= 2.20"				
0.0	26	0.3100	8.96		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
0.6	111	0.0410	3.26		Shallow Concentrated Flow,				
					Unpaved Kv= 16.1 fps				
9.0	187	Total							

Subcatchment 4: Subcat 4



Summary for Subcatchment 5: Subcat 5

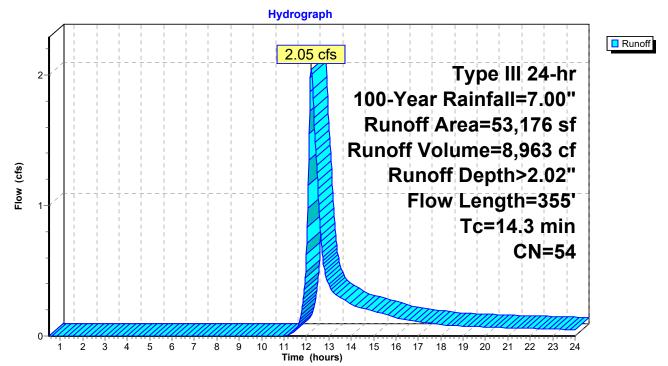
Runoff = 2.05 cfs @ 12.22 hrs, Volume= 8,963 cf, Depth> 2.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

	А	rea (sf)	CN	Description						
		27,303	49	9 50-75% Grass cover, Fair, HSG A						
		7,837	98	B Paved roads w/curbs & sewers, HSG A						
		2,301	98	Roofs, HSG A						
		15,734	36	6 Woods, Fair, HSG A						
	53,176 54 Weighted Average									
		43,037		80.93% Pe	rvious Area	l				
		10,138		19.07% Im	pervious Ar	ea				
	Тс	Length		,	Capacity	Description				
_	(min)	(feet)	(ft/f	t) (ft/sec)	(cfs)					
	12.3	50	0.032	0.07		Sheet Flow,				
						Woods: Light underbrush n= 0.400 P2= 2.20"				
	1.6	248	0.027	0 2.65		Shallow Concentrated Flow,				
						Unpaved Kv= 16.1 fps				
	0.4	57	0.012	2 2.24		Shallow Concentrated Flow,				
_						Paved Kv= 20.3 fps				
	44.0	0.5.5	— · · ·							

14.3 355 Total

Subcatchment 5: Subcat 5



Summary for Subcatchment 6: Subcat 6

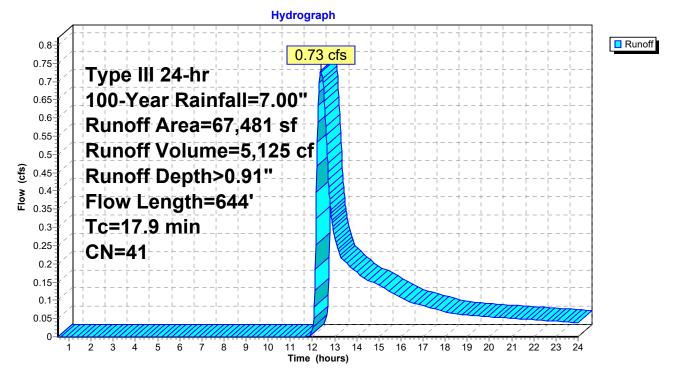
Runoff = 0.73 cfs @ 12.37 hrs, Volume= 5,125 cf, Depth> 0.91"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

	Area (sf)	CN E	Description							
	24,941	49 5	9 50-75% Grass cover, Fair, HSG A							
	754	98 F	Roofs, HSO	βA						
	41,787	36 V	<u>Voods, Fai</u>	r, HSG A						
	67,481	41 V	Veighted A	verage						
	66,727	ç	98.88% Pei	vious Area						
	754	1	.12% Impe	ervious Area	a					
_										
T	0	Slope	Velocity	Capacity	Description					
(min) (feet)	(ft/ft)	(ft/sec)	(cfs)						
14.9	9 50	0.0200	0.06		Sheet Flow,					
					Woods: Light underbrush n= 0.400 P2= 2.20"					
2.2	2 282	0.0170	2.10		Shallow Concentrated Flow,					
					Unpaved Kv= 16.1 fps					
0.0	6 245	0.1600	6.44		Shallow Concentrated Flow,					
-					Unpaved Kv= 16.1 fps					
0.2	2 67	0.2100	7.38		Shallow Concentrated Flow,					
					Unpaved Kv= 16.1 fps					

17.9 644 Total

Subcatchment 6: Subcat 6



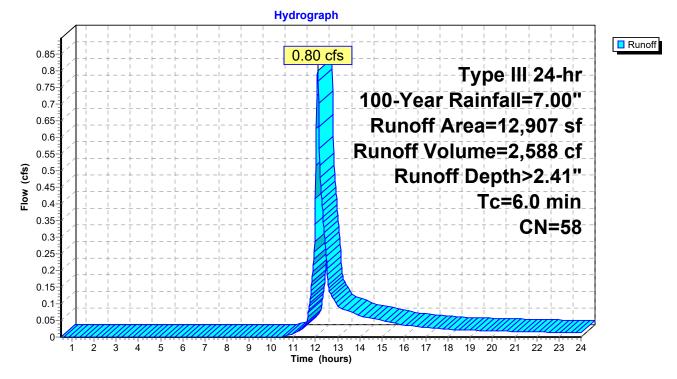
Summary for Subcatchment 7: Subcat 7

Runoff = 0.80 cfs @ 12.10 hrs, Volume= 2,588 cf, Depth> 2.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

A	rea (sf)	CN	Description						
	10,544	49	50-75% Grass cover, Fair, HSG A						
	1,337	98	Paved road	s w/curbs &	& sewers, HSG A				
	1,026	98	Roofs, HSO	βA					
	12,907	58	Weighted Average						
	10,544		81.69% Pervious Area						
	2,363		18.31% Impervious Area						
Tc	Length	Slope	,	Capacity	Description				
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
6.0					Direct Entry,				

Subcatchment 7: Subcat 7



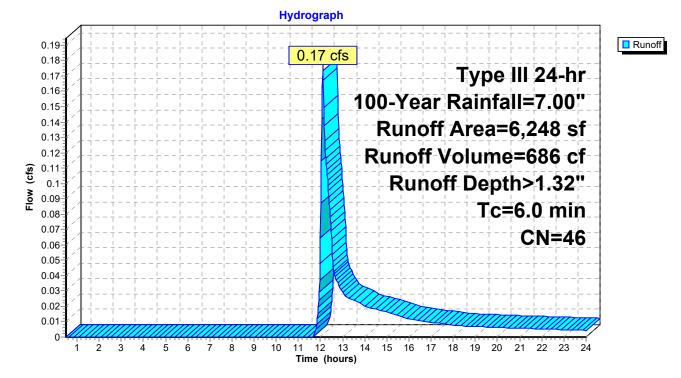
Summary for Subcatchment 8: Subcat 8

Runoff = 0.17 cfs @ 12.11 hrs, Volume= 686 cf, Depth> 1.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

A	rea (sf)	CN	Description				
	3,110	49	50-75% Gra	ass cover, F	Fair, HSG A		
	313	98	Roofs, HSG	βA			
	2,825	36	Woods, Fai	r, HSG A			
	6,248	46	Weighted A	verage			
	5,935	95.00% Pervious Area					
	313	:	5.00% Impervious Area				
Тс	Length	Slope		Capacity	Description		
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
6.0					Direct Entry,		
					-		

Subcatchment 8: Subcat 8



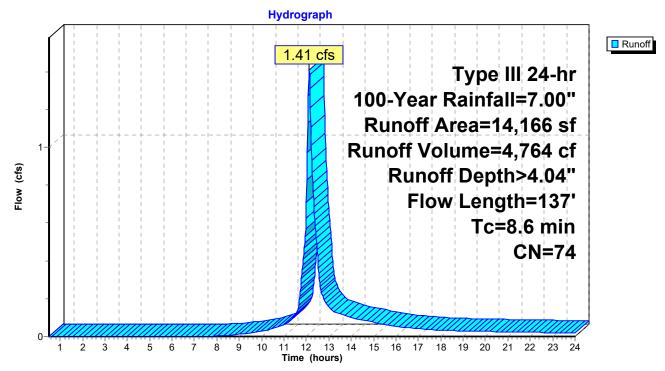
Summary for Subcatchment 9: Subcat 9

Runoff = 1.41 cfs @ 12.12 hrs, Volume= 4,764 cf, Depth> 4.04"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

 A	rea (sf)	CN [Description						
	6,698	49 5	49 50-75% Grass cover, Fair, HSG A						
	6,734	98 F	Paved road	s w/curbs &	& sewers, HSG A				
	532	98 F	Roofs, HSG	βA					
	202	36 \	Voods, Fai	r, HSG A					
	14,166	74 \	Veighted A	verage					
	6,900	2	8.71% Per	vious Area	l				
	7,266	5	51.29% Imp	pervious Ar	ea				
Тс	Length	Slope	Velocity	Capacity	Description				
Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description				
 			,		Description Sheet Flow,				
 (min)	(feet)	(ft/ft)	(ft/sec)						
 (min)	(feet)	(ft/ft)	(ft/sec)		Sheet Flow,				
 <u>(min)</u> 7.8	(feet) 50	(ft/ft) 0.0360	(ft/sec) 0.11		Sheet Flow, Grass: Dense n= 0.240 P2= 2.20"				

Subcatchment 9: Subcat 9



0

2 3

4 5 6 7 8 9

1

CN=86

11 12 13 14 15 16 17 18 19 20 21 22 23 24 Time (hours)

Summary for Subcatchment 10: Subcat 10

Runoff = 1.54 cfs @ 12.09 hrs, Volume= 4,944 cf, Depth> 5.36"

10

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Type III 24-hr 100-Year Rainfall=7.00"

Area (sf)	CN Description									
2,766	49 50-75% Grass cover, Fair, HSG A									
8,278	98 Paved roads w/curbs & sewers, HSG A									
23	36 Woods, Fair, HSG A 86 Weighted Average									
2,789	25.20% Pervious Area									
8,278	74.80% Impervious Area									
Tc Length (min) (feet)	Slope Velocity Capacity Description (ft/ft) (ft/sec) (cfs)									
6.0	Direct Entry,									
	Subcatchment 10: Subcat 10 Hydrograph									
Flow (cfs)	100-Year Rainfall=7.00" Runoff Area=11,067 sf Runoff Volume=4,944 cf Runoff Depth>5.36" Tc=6.0 min									

Summary for Reach 15R: CB 6

 Inflow Area =
 14,166 sf, 51.29% Impervious, Inflow Depth > 4.04" for 100-Year event

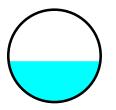
 Inflow =
 1.41 cfs @ 12.12 hrs, Volume=
 4,764 cf

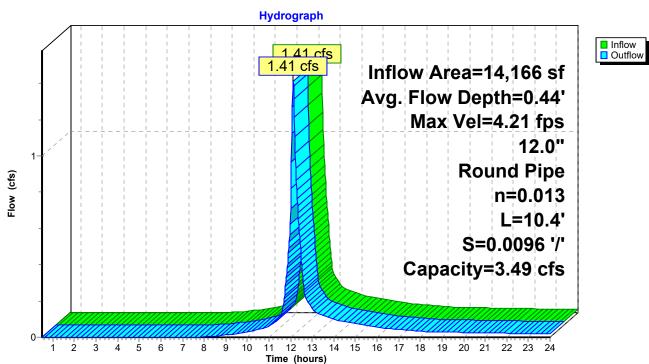
 Outflow =
 1.41 cfs @ 12.12 hrs, Volume=
 4,764 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.21 fps, Min. Travel Time= 0.0 min Avg. Velocity = 1.55 fps, Avg. Travel Time= 0.1 min

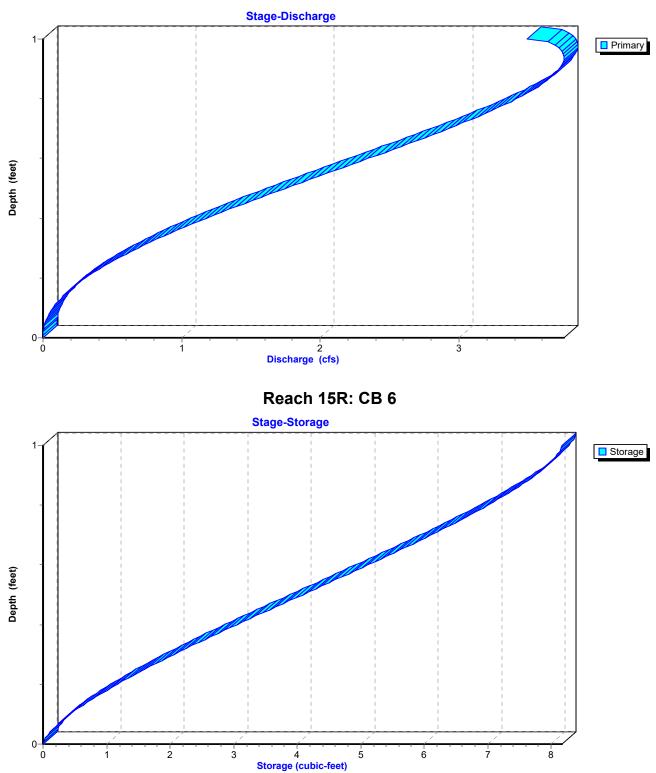
Peak Storage= 3 cf @ 12.12 hrs Average Depth at Peak Storage= 0.44' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 3.49 cfs

12.0" Round Pipe n= 0.013 Length= 10.4' Slope= 0.0096 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 15R: CB 6



Reach 15R: CB 6

Summary for Reach 16R: CB 5

 Inflow Area =
 53,176 sf, 19.07% Impervious, Inflow Depth > 2.02" for 100-Year event

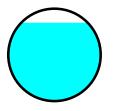
 Inflow =
 2.05 cfs @ 12.22 hrs, Volume=
 8,963 cf

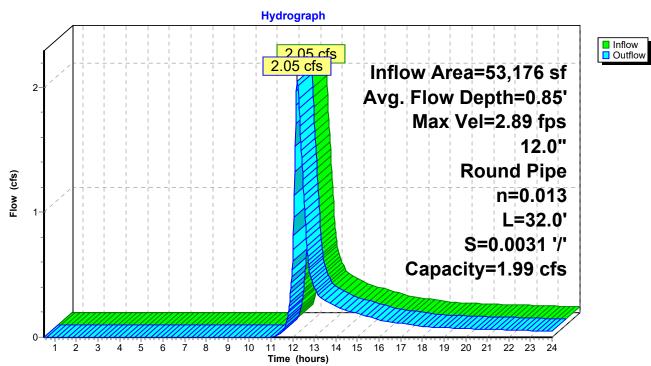
 Outflow =
 2.05 cfs @ 12.22 hrs, Volume=
 8,961 cf, Atten= 0%, Lag= 0.2 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.89 fps, Min. Travel Time= 0.2 min Avg. Velocity = 1.40 fps, Avg. Travel Time= 0.4 min

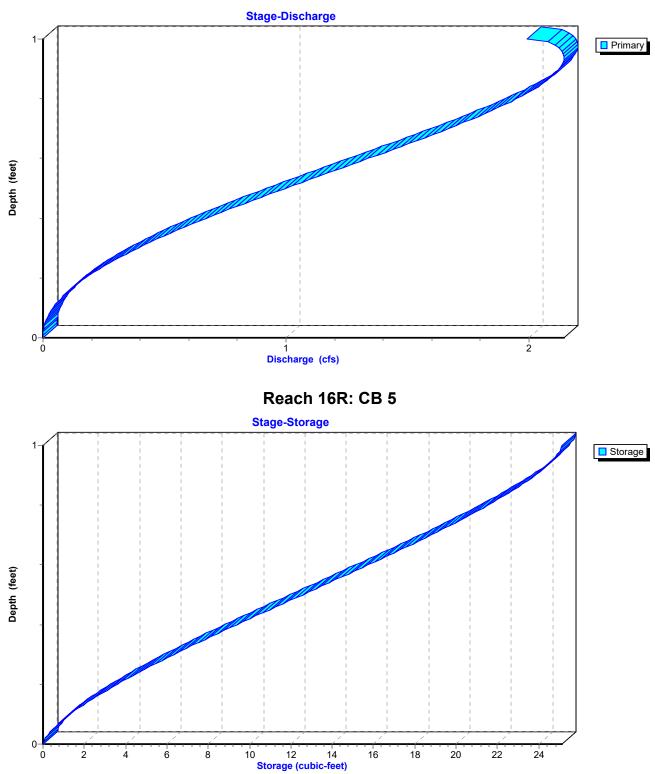
Peak Storage= 23 cf @ 12.22 hrs Average Depth at Peak Storage= 0.85' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 1.99 cfs

12.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0031 '/' Inlet Invert= 67.50', Outlet Invert= 67.40'





Reach 16R: CB 5



Reach 16R: CB 5

Summary for Reach 17R: DMH 7

 Inflow Area =
 67,342 sf, 25.85% Impervious, Inflow Depth > 2.45" for 100-Year event

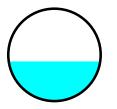
 Inflow =
 3.18 cfs @ 12.17 hrs, Volume=
 13,725 cf

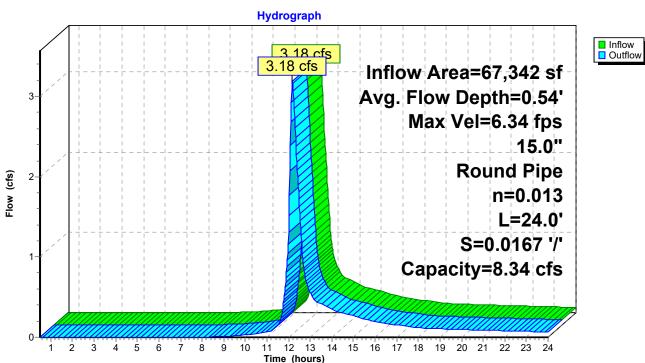
 Outflow =
 3.18 cfs @ 12.17 hrs, Volume=
 13,724 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 6.34 fps, Min. Travel Time= 0.1 min Avg. Velocity = 2.48 fps, Avg. Travel Time= 0.2 min

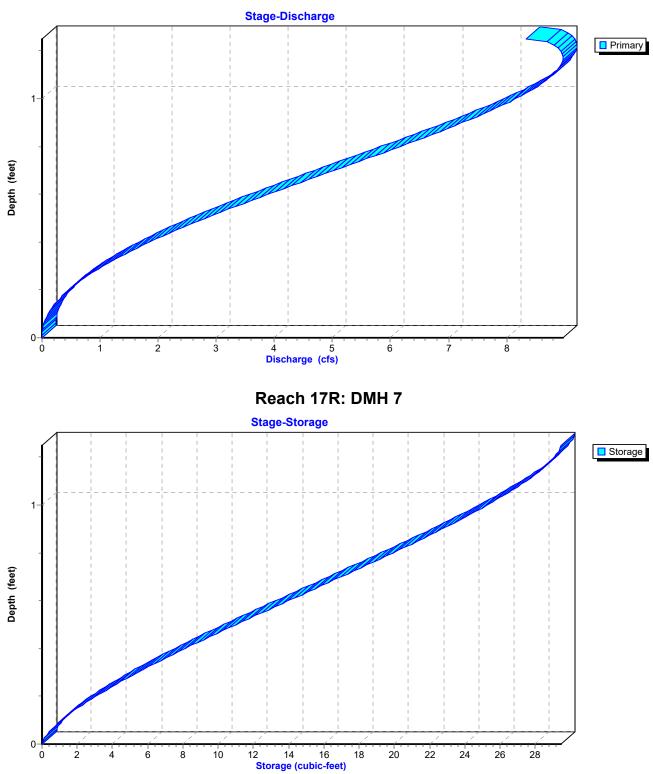
Peak Storage= 12 cf @ 12.17 hrs Average Depth at Peak Storage= 0.54' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 8.34 cfs

15.0" Round Pipe n= 0.013 Length= 24.0' Slope= 0.0167 '/' Inlet Invert= 67.40', Outlet Invert= 67.00'





Reach 17R: DMH 7



Reach 17R: DMH 7

Summary for Reach 18R: CB 2

 Inflow Area =
 11,067 sf, 74.80% Impervious, Inflow Depth > 5.36" for 100-Year event

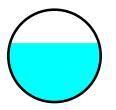
 Inflow =
 1.54 cfs @
 12.09 hrs, Volume=
 4,944 cf

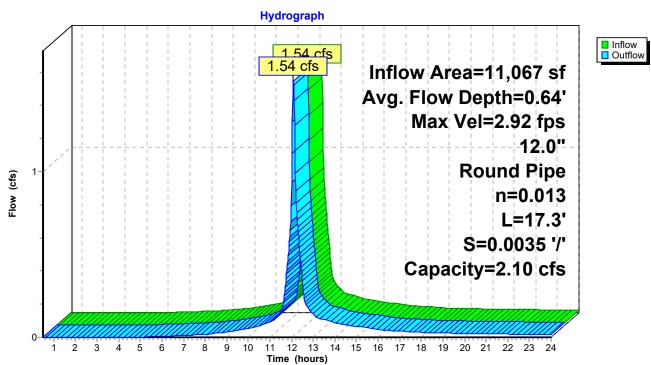
 Outflow =
 1.54 cfs @
 12.09 hrs, Volume=
 4,944 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 2.92 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.02 fps, Avg. Travel Time= 0.3 min

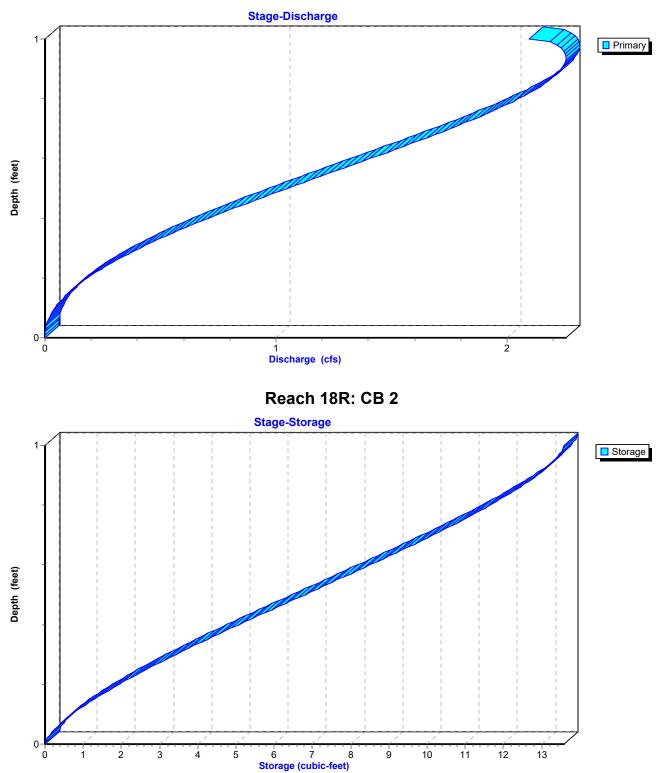
Peak Storage= 9 cf @ 12.09 hrs Average Depth at Peak Storage= 0.64' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 2.10 cfs

12.0" Round Pipe n= 0.013 Length= 17.3' Slope= 0.0035 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 18R: CB 2



Reach 18R: CB 2

Summary for Reach 19R: CB 1

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 3.00" for 100-Year event

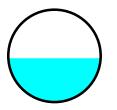
 Inflow =
 1.87 cfs @
 12.12 hrs, Volume=
 6,388 cf

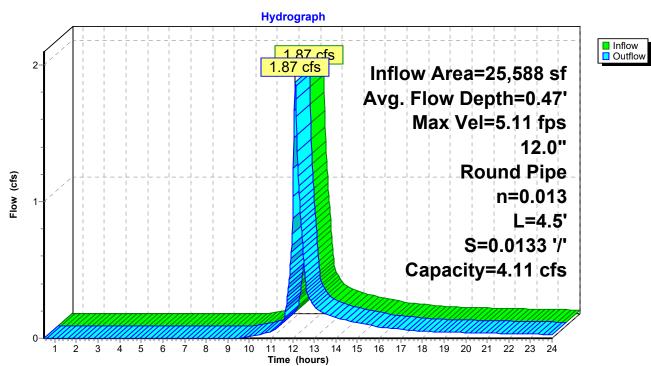
 Outflow =
 1.87 cfs @
 12.12 hrs, Volume=
 6,388 cf, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 5.11 fps, Min. Travel Time= 0.0 min Avg. Velocity = 2.00 fps, Avg. Travel Time= 0.0 min

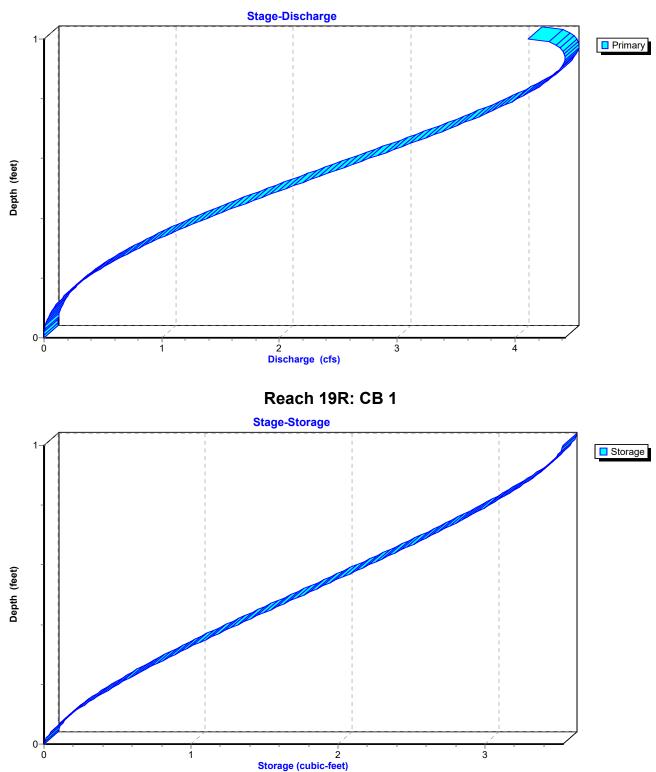
Peak Storage= 2 cf @ 12.12 hrs Average Depth at Peak Storage= 0.47' Bank-Full Depth= 1.00' Flow Area= 0.8 sf, Capacity= 4.11 cfs

12.0" Round Pipe n= 0.013 Length= 4.5' Slope= 0.0133 '/' Inlet Invert= 66.46', Outlet Invert= 66.40'





Reach 19R: CB 1



Reach 19R: CB 1

Summary for Reach 20R: DMH 3

 Inflow Area =
 25,588 sf, 31.23% Impervious, Inflow Depth > 3.00" for 100-Year event

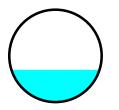
 Inflow =
 1.87 cfs @
 12.12 hrs, Volume=
 6,388 cf

 Outflow =
 1.87 cfs @
 12.13 hrs, Volume=
 6,388 cf, Atten= 0%, Lag= 0.1 min

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Max. Velocity= 4.94 fps, Min. Travel Time= 0.1 min Avg. Velocity = 1.90 fps, Avg. Travel Time= 0.3 min

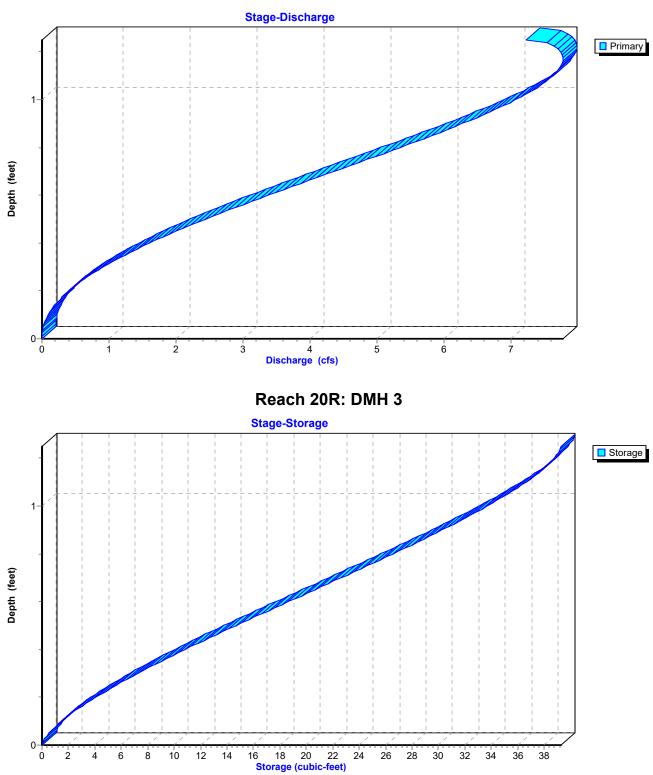
Peak Storage= 12 cf @ 12.13 hrs Average Depth at Peak Storage= 0.43' Bank-Full Depth= 1.25' Flow Area= 1.2 sf, Capacity= 7.22 cfs

15.0" Round Pipe n= 0.013 Length= 32.0' Slope= 0.0125 '/' Inlet Invert= 66.40', Outlet Invert= 66.00'



Hydrograph Inflow Outflow 1 87 cfs 2 1.87 cfs Inflow Area=25,588 sf Avg. Flow Depth=0.43' Max Vel=4.94 fps 15.0" **Round Pipe** Flow (cfs) n=0.013 L=32.0' S=0.0125 '/' Capacity=7.22 cfs 2 ġ. 5 6 8 ġ 10 12 13 14 15 16 17 18 19 20 21 22 23 24 1 4 7 11 Time (hours)

Reach 20R: DMH 3



Reach 20R: DMH 3

Summary for Pond 11P: BASIN 1

Inflow Area =	95,314 sf, 22.44% Impervious,	Inflow Depth > 2.39" for 100-Year event
Inflow =	4.28 cfs @ 12.13 hrs, Volume=	19,009 cf
Outflow =	2.82 cfs @ 12.36 hrs, Volume=	15,749 cf, Atten= 34%, Lag= 14.1 min
Discarded =	0.16 cfs @ 12.36 hrs, Volume=	7,130 cf
Primary =	2.67 cfs @ 12.36 hrs, Volume=	8,619 cf

Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 66.17' @ 12.36 hrs Surf.Area= 2,787 sf Storage= 4,750 cf

Plug-Flow detention time= 125.8 min calculated for 15,749 cf (83% of inflow) Center-of-Mass det. time= 52.7 min (902.4 - 849.7)

Volume	Inve	rt Avail.Sto	rage Sto	age Storage Description				
#1	64.00	0' 10,88	30 cf Cu	stom Stage Data (P	rismatic)Listed below			
Elevatio		Surf.Area	Inc.Sto					
(fee	et)	(sq-ft)	(cubic-fee	et) (cubic-feet)				
64.0	00	1,611		0 0				
64.5	50	1,857	8	67 867				
65.0	00	2,118	99	94 1,861				
65.5	50	2,392	1,1:	28 2,988				
66.0	00	2,681	1,20	68 4,257				
66.5	50	2,984	1,4	16 5,673				
67.0	00	3,301	1,5	71 7,244				
67.5	50	3,632	1,7;	33 8,977				
68.0	00	3,977	1,90	02 10,880				
		,	,	,				
Device	Routing	Invert	Outlet D	evices				
#1	Primary	65.80'	4.0' lond	x 0.5' breadth Bro	oad-Crested Rectangular Weir			
	,			et) 0.20 0.40 0.60				
			· ·	nglish) 2.80 2.92 3				
#2	Discardeo	64.00'						
	#2 Discarded 64.00' 2.410 in/hr Exfiltration over Surface area							
		NA 0.40 C	~ 40.00					

Discarded OutFlow Max=0.16 cfs @ 12.36 hrs HW=66.17' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.16 cfs)

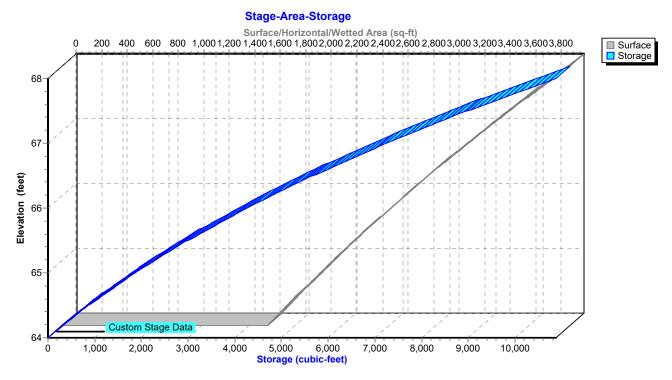
Primary OutFlow Max=2.66 cfs @ 12.36 hrs HW=66.17' (Free Discharge) —1=Broad-Crested Rectangular Weir (Weir Controls 2.66 cfs @ 1.78 fps)

Hydrograph Inflow
 Outflow
 Discarded 4.28 cfs Inflow Area=95,314 sf Primary Peak Elev=66.17' Storage=4,750 cf 4 2.82 cfs 2.67 cfs 3 Flow (cfs) 2 0 0 11 12 13 14 15 16 17 18 19 20 21 22 23 24 Time (hours) 2 1 ż ģ 4 5 6 7 8 10 Pond 11P: BASIN 1 Stage-Discharge Total Discarded 68 Primary 67 Elevation (feet) 66-Broad-Crested Rectangular Weir 65 Exfiltration 64 5 10 15 20 25 30 35 40 Ó Discharge (cfs)

Pond 11P: BASIN 1

Type III 24-hr 100-Year Rainfall=7.00" Printed 4/30/2018 ons LLC Page 128

Pond 11P: BASIN 1



Summary for Pond 13P: BASIN 2

Inflow Area =	80,249 sf, 24.63% Impervious,	Inflow Depth > 2.44" for 100-Year event
Inflow =	3.80 cfs @ 12.15 hrs, Volume=	16,312 cf
Outflow =	0.87 cfs @ 12.77 hrs, Volume=	12,592 cf, Atten= 77%, Lag= 36.8 min
Discarded =	0.21 cfs @ 12.77 hrs, Volume=	9,341 cf
Primary =	0.66 cfs @ 12.77 hrs, Volume=	3,252 cf

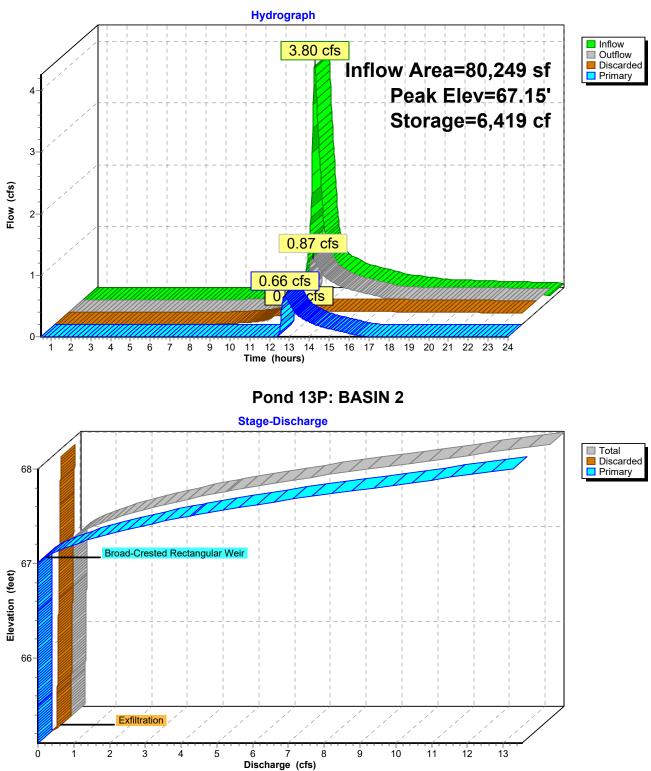
Routing by Stor-Ind method, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs Peak Elev= 67.15' @ 12.77 hrs Surf.Area= 3,823 sf Storage= 6,419 cf

Plug-Flow detention time= 218.6 min calculated for 12,592 cf (77% of inflow) Center-of-Mass det. time= 131.3 min (988.3 - 857.0)

Volume	Inver	t Avail.Sto	age Storage Description				
#1	65.10	' 9,9^	10 cf Custo	om Stage Data (Prismatic)Listed below			
	_						
Elevatio		Surf.Area	Inc.Store				
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
65.´	10	2,409	0	0			
65.5	50	2,714	1,025	1,025			
66.0	00	3,033	1,437	2,461			
66.5	50	3,366	1,600	4,061			
67.0	00	3,714	1,770	5,831			
67.5	50	4,075	1,947	7,778			
68.0	00	4,451	2,132	9,910			
Device	Routing	Invert	Outlet Device	ices			
#1	Primary	67.00'	4.0' long x	x 0.5' breadth Broad-Crested Rectangular Weir			
	2		Head (feet)) 0.20 0.40 0.60 0.80 1.00			
				, lish) 2.80 2.92 3.08 3.30 3.32			
#2	Discarded	65.10'	· · ·	r Exfiltration over Surface area			
D'		Mar. 0.04 af		$(1) \Lambda = 0.7 \Lambda \Gamma = (\Gamma_{\text{max}} \circ \Omega)$			

Discarded OutFlow Max=0.21 cfs @ 12.77 hrs HW=67.15' (Free Discharge) **2=Exfiltration** (Exfiltration Controls 0.21 cfs)

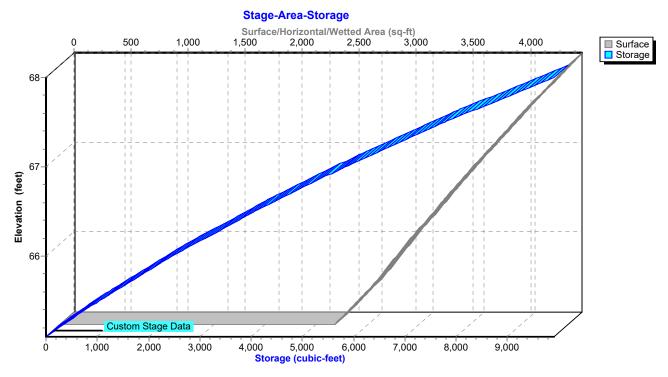
Primary OutFlow Max=0.66 cfs @ 12.77 hrs HW=67.15' (Free Discharge) **1=Broad-Crested Rectangular Weir** (Weir Controls 0.66 cfs @ 1.09 fps)



Pond 13P: BASIN 2

Type III 24-hr 100-Year Rainfall=7.00" Printed 4/30/2018 ons LLC Page 131

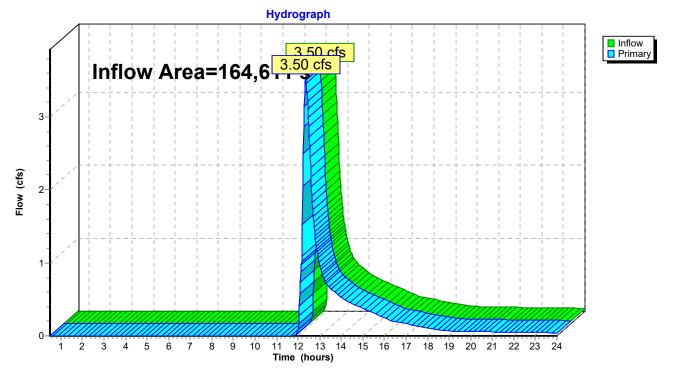
Pond 13P: BASIN 2



Summary for Link 12L: Southwest Wetland

Inflow Area	a =	164,611 sf,	13.58% Impervious,	Inflow Depth >	1.04"	for 100-Year event
Inflow	=	3.50 cfs @	12.35 hrs, Volume=	14,312 c	f	
Primary	=	3.50 cfs @	12.35 hrs, Volume=	14,312 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs

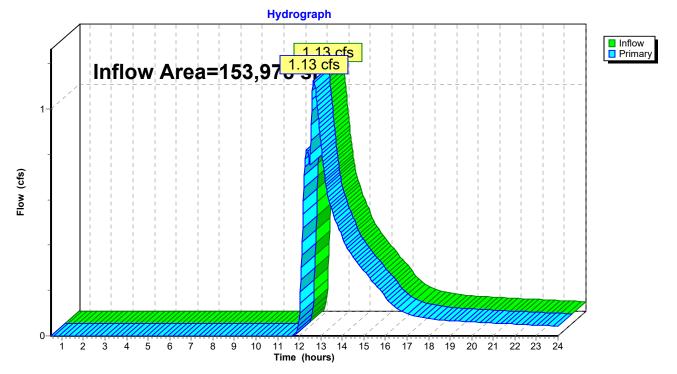


Link 12L: Southwest Wetland

Summary for Link 14L: Northwest Wetland

Inflow Area	a =	153,978 sf,	13.53% Impervious,	Inflow Depth >	0.71"	for 100-Year event
Inflow	=	1.13 cfs @	12.68 hrs, Volume=	9,063 c	f	
Primary	=	1.13 cfs @	12.68 hrs, Volume=	9,063 c	f, Atter	n= 0%, Lag= 0.0 min

Primary outflow = Inflow, Time Span= 0.50-24.00 hrs, dt= 0.02 hrs



Link 14L: Northwest Wetland

Section III

OPERATION AND MAINTENANCE PLAN

PROPOSED DRAINAGE SYSTEM – DURING CONSTRUCTION Old Cart Path Lane Ext. (70 Old Cart Path Lane) Pembroke, MA 02359

Owner:

Stephen Saia 70 Old Cart Path lane Pembroke, MA 02359 Contact: Stephen Saia (781-826-8401)

Party Responsible for Operation and Maintenance:

Stephen Saia 70 Old Cart Path lane Pembroke, MA 02359 Contact: Stephen Saia (781-826-8401)

Source of Funding:

Operation and Maintenance of this stormwater management system will be the responsibility of the property owner to include its successor and/or assigns, as the same may appear on record with the appropriate register of deeds.

During Construction:

Construction activities shall follow the Construction Sequence shown on the approved plan. During periods of active construction the stormwater management system shall be inspected on a weekly basis and within 24 hours of a storm event of greater than ¹/₂". Maintenance tasks shall be performed monthly or after significant rainfall events of 1" of rain or greater. During construction, silt-laden runoff shall be prevented from entering the drainage system and off-site properties. Temporary swales shall be constructed as needed during construction to direct runoff to sediment traps. Infiltration systems shall not be placed in service until after the installation of base course pavement and vegetative stabilization of the areas contributing to the systems.

During dewatering operations, all water pumped from the dewatering shall be directed to a "dirt bag" pumped sediment removal system (or approved equal) as manufactured by ACF Environmental. The unit shall be placed on a crushed stone blanket. Disposal of such "dirt bag" shall occur when the device is full and can no longer effectively filter sediment or allow water to pass at a reasonable flow rate. Disposal of this unit shall be the responsibility of the contractor and shall be as directed by the owner in accordance with applicable local, state, and federal guidelines and regulations.

Stabilized construction entrances shall be placed at the entrances and shall consist of $1\frac{1}{2}$ " to 2" stone and be constructed as shown on the approved plans.

All erosion and sedimentation control measures shall be in place prior to the commencement of any site work or earthwork operations, shall be maintained during construction, and shall remain in place until all site work is complete and ground cover is established.

Heavy equipment shall not be used on basin bottoms.

All exposed soils not to be paved shall be stabilized as soon as practical. Seed mixes shall only be applied during appropriate periods as recommended by the seed supplier, typically May 1 to October 15. Any exposed soils that can not be stabilized by vegetation during these dates shall be stabilized with hay bales, hay mulch, check dams, jute netting or other acceptable means.

Once each structure is in place, it should be maintained in accordance with the procedures described in the post-construction Operations and Maintenance Plan.

During dry periods where dust is created by construction activities the following control measures should be implemented.

- Sprinkling The contractor may sprinkle the ground along haul roads and traffic areas until moist.
- Vegetative cover Areas that are not expected to be disturbed regularly may be stabilized with vegetative cover.
- Mulch Mulching can be used as a quick and effective means of dust control in recently disturbed areas.
- Spray on chemical soil treatments may be utilized. Application rates shall conform to manufacturers recommendations.

Inspections

The Owner shall be responsible to secure the services of a Professional Engineer to perform inspections as required. Inspections during periods of active construction shall be weekly and within 24 hours of a storm event of greater than ½ ". The Professional Engineer shall perform inspections to insure that the approved plan is being followed with particular attention to the Planning Board Approval and the Construction Sequencing. The Engineer shall be responsible for inspecting the roadway construction and the construction of the stormwater management system. The Engineer shall prepare and submit to the Planning Board, the Inspection Schedule and Evaluation Checklist (see attached) and, if necessary, request the required maintenance and/or repair of the necessary items. This form shall be stamped by the Engineer and the Owner shall be notified that specific changes and/or repairs are necessary.

For additional information, refer to <u>Performance, Standards and Guidelines for Stormwater</u> <u>Management in Massachusetts</u>, published by the Department of Environmental Protection.

STORMWATER MANAGEMENT BEST MANAGEMENT PRACTICES INSPECTION SCHEDULE AND EVALUATION CHECKLIST – CONSTRUCTION PHASE

PROJECT LOCATION: Old Cart Path Lane Ext. (70 Old Cart Path Lane) – Pembroke, MA Latest Revision: 4/30/18

Stormwater Control Manager: ____

Stamp

Best Management Practice	Inspection Frequency (1)	Date Inspec ted	Inspector	Minimum Maintenance and Key Items to Check	Cleaning / Repair Needed yes/no List items	Date of Cleaning/Repair	Performed By	Water Level in Detention System
Silt fence & swales and silt traps	After every major storm event							
Temporary Constructio n Entrance	Daily or as needed.							
Outlet control structure + Flow dissipator	After every major storm event							

(1) Refer to the Massachusetts Stormwater Management, Volume Two: Stormwater Technical Handbook for recommendations regarding frequency for inspection and maintenance of specific BMPs.

Limited or no use of sodium chloride salts, fertilizers or pesticides recommended. Slow release fertilizer recommended. Other notes:(Include deviations from: Con Com Order of Conditions, PB Approval, Construction Sequence and Approved Plan)

PROPOSED DRAINAGE SYSTEM – DURING CONSTRUCTION Old Cart Path Lane Ext. (70 Old Cart Path Lane) Pembroke, MA 02359

Owner:

Stephen Saia 70 Old Cart Path lane Pembroke, MA 02359 Contact: Stephen Saia (781-826-8401)

Party Responsible for Operation and Maintenance:

During construction until roadway is accepted by Town Stephen Saia

After roadway is completed and accepted by Town Meeting Department of Public Works Pembroke, MA 02359

Source of Funding:

Operation and Maintenance of this stormwater management system will be the responsibility of the owners until the road and drainage system are accepted by Town Meeting and conveyed to the Town of Pembroke. Once accepted by the Town, funding for operation and maintenance of the stormwater management system will be the responsibility of the Department of Public Works.

Post Construction Inspection and Maintenance:

Street Sweeping

Streets shall be swept at least twice per year. Sweeping shall be completed during the early spring, no later than May 1st, before sediment from winter sanding operations is washed into the drainage system. Disposal of the accumulated sediment shall be in accordance with applicable local, state, and federal guidelines and regulations.

Deep Sump Catch Basins

Deep sump catch basins shall become part of the roadway system and shall be inspected after every major storm event during construction and cleaned when sediment exceeds 18" depth. After construction when all slopes have been stabilized, basins shall be cleaned a minimum of twice per year. Disposal of the accumulated sediment shall be in accordance with applicable local, state, and federal guidelines and regulations.

Stormceptor Unit(s)

New Installations

The condition of each unit shall be checked after every runoff event for the first 30 days. The visual inspection shall ascertain that the unit is functioning properly (weir structure is not blocked) and shall measure the amount of sediment that has accumulated in the sump and floating trash and debris in the separation chamber. This can be done with a calibrated "dip stick" so that the depth of deposition can be tracked. Schedules for inspections and cleanout shall be based on storm events and pollutant accumulation.

Ongoing Operation

During the rainfall season, the unit shall be inspected at least once every 30 days. The floatables shall be removed and the sump cleaned when the sump is 85% full. If floatables accumulate more rapidly than the settleable solids, the floatables shall be removed using a vactor truck or dip net when the layer is two feet thick.

Cleanout of the Stormceptor units shall be performed no later than May 1st because of the nature of pollutants collected and the potential for odor generation from the decomposition of material collected and retained. This end of season cleanout will assist in preventing the discharge of pore water for the Stormceptor units during periods of low rainfall. The Stormceptor unit shall be cleaned at least twice yearly.

Cleanout and Disposal

Standard vactoring operations shall be employed in the cleanout of the Stormceptor units. Disposal of material from the Stormceptor units shall be in accordance with applicable local, state, and federal guidelines and regulations. Disposal of the decant material to a POTW is recommended. Field decanting to the storm drainage system shall not be permitted. Solids can be disposed similar to normal practices for materials collected from catch basin cleaning.

Infiltration Basin(s)

After construction, the infiltration basins should be inspected for standing water 1-2 days after any significant rainfall exceeding 1" of rainfall in 24 hours. If the infiltration basin is continuing to hold standing water after 2 days the owner should have outlet structure inspected and repaired. The basin should also be inspected to verify whether infiltration function has been lost. If infiltration capacity has become degraded, it should be restored under the direction of a qualified professional.

The infiltration basins should be inspected quarterly and at least once per year to ensure that the system is operating as intended. If accumulated sediment is observed within the basin it should be removed from the basin as necessary. Any sediment removed from the infiltration systems should be disposed of in accordance with Town, State and Federal Regulations. The system including the stormwater discharge locations should also be inspected for growth of any invasive species and removed if found.

The embankments of the basin shall be mowed periodically, to prevent the establishment of woody vegetation on the berms. Embankments and spillways shall be inspected annually for general structural integrity, with immediate corrective action as warranted by inspection.

Lawn Fertilization

Lawn fertilizer shall be slow release and limited to 3 lbs per 1000 s.f. per year.

STORMWATER MANAGEMENT BEST MANAGEMENT PRACTICES

INSPECTION SCHEDULE AND EVALUATION CHECKLIST – POST CONSTRUCTION PHASE

PROJECT LOCATION: Old Cart Path Lane Ext. (70 Old Cart Path Lane) – Pembroke, MA Latest Revision: 4/30/18

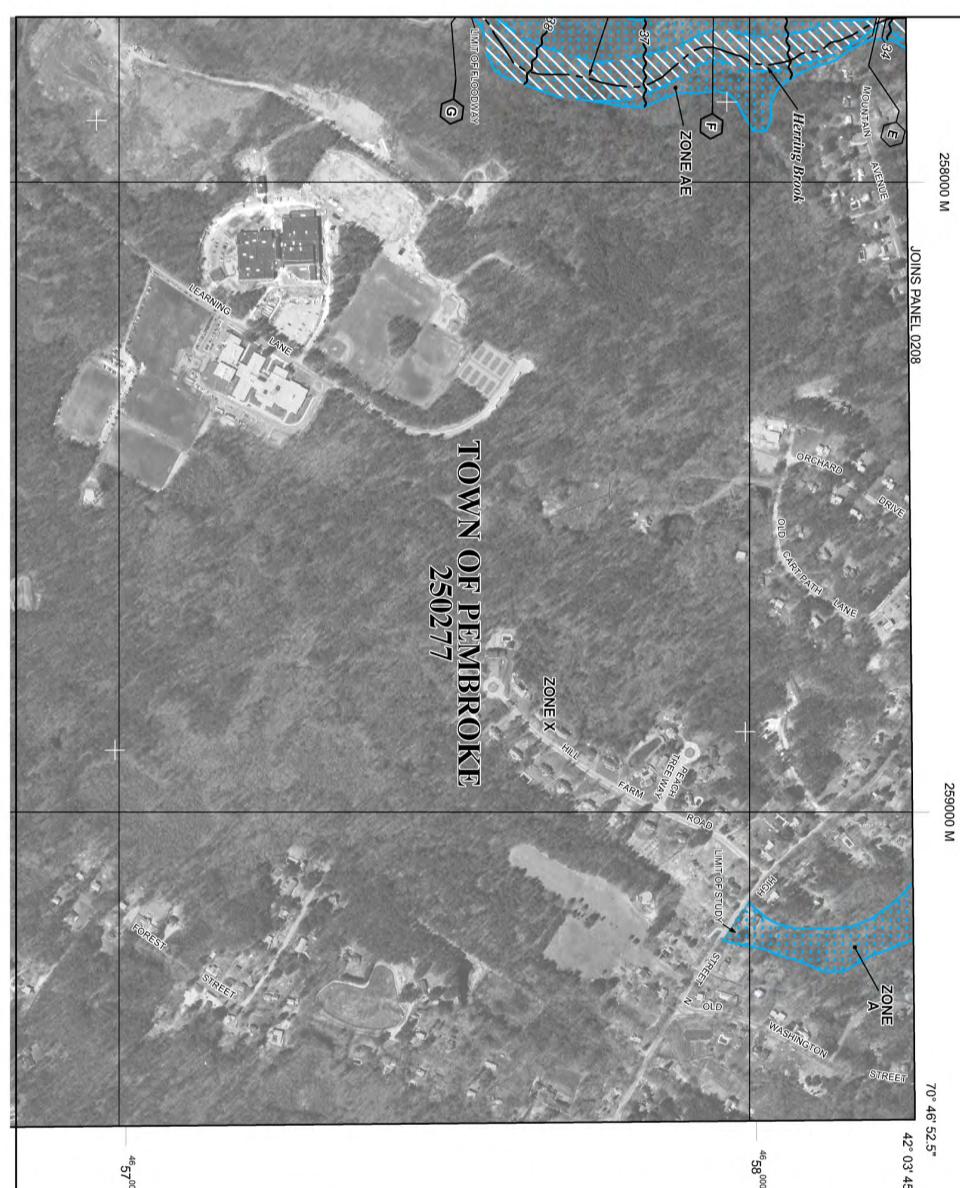
Best	Inspection	Date	Inspector	Minimum	Cleaning/	Date of	Performed	Water
Management	Frequency	Inspected		Maintenance and	Repair	Cleaning/Repair	By	Level in
Practice	(1)	-		Key Items to	Needed		-	Detention
				Check	yes/no			System
					List items			-
Deep Sump	Twice per							
Catch	year							
Basins								
Stormceptor	Twice per							
_	year							
Infiltration	Once per							
Basin	year							
	-							

(1) Refer to the Massachusetts Stormwater Management, Volume Two: Stormwater Technical Handbook for recommendations regarding frequency for inspection and maintenance of specific BMPs.

Limited or no use of sodium chloride salts, fertilizers or pesticides recommended. Slow release fertilizer recommended. Other notes:(Include deviations from: Con Com Order of Conditions, PB Approval, Construction Sequence and Approved Plan)

Stormwater Control Manager: _____

Stamp



This is an official cop was extracted using or amendments with title block. For the I Program flood maps	NATIONAL FLOOD	INSURANCE PROGRAM	
copy of a portion of the above referenced flood map. ing F-MIT On-Line. This map does not reflect change which may have been made subsequent to the date o re latest product information about National Flood Ins aps check the FEMA Flood Map Store at www.msc.fi	Notice to User. The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community. MAP NUMBER 25023C0216J EFFECTIVE DATE JULY 17, 2012 Federal Emergency Management Agency	FICOD INSURANCE RATE MAP PLYMOUTH COUNTY, MASSACHUSETTS (ALL JURISDICTIONS) PANEL 216 OF 650 (SEE MAP INDEX FOR FIRM PANEL LAYOUT) (SEE MAP INDEX FOR FIRM PANEL LAYOUT) CONTAINS COMMUNITY NUMBER PANE SUFFIX DURBURGE TOWN OF 25023 0216 J	MAP SCALE 1" = 500' 500 1000 FEET METER:



United States Department of Agriculture



Natural Resources Conservation Service A product of the National Cooperative Soil Survey, a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local participants

Custom Soil Resource Report for Plymouth County, Massachusetts



Preface

Soil surveys contain information that affects land use planning in survey areas. They highlight soil limitations that affect various land uses and provide information about the properties of the soils in the survey areas. Soil surveys are designed for many different users, including farmers, ranchers, foresters, agronomists, urban planners, community officials, engineers, developers, builders, and home buyers. Also, conservationists, teachers, students, and specialists in recreation, waste disposal, and pollution control can use the surveys to help them understand, protect, or enhance the environment.

Various land use regulations of Federal, State, and local governments may impose special restrictions on land use or land treatment. Soil surveys identify soil properties that are used in making various land use or land treatment decisions. The information is intended to help the land users identify and reduce the effects of soil limitations on various land uses. The landowner or user is responsible for identifying and complying with existing laws and regulations.

Although soil survey information can be used for general farm, local, and wider area planning, onsite investigation is needed to supplement this information in some cases. Examples include soil quality assessments (http://www.nrcs.usda.gov/wps/portal/nrcs/main/soils/health/) and certain conservation and engineering applications. For more detailed information, contact your local USDA Service Center (https://offices.sc.egov.usda.gov/locator/app?agency=nrcs) or your NRCS State Soil Scientist (http://www.nrcs.usda.gov/wps/portal/nrcs/detail/soils/contactus/? cid=nrcs142p2_053951).

Great differences in soil properties can occur within short distances. Some soils are seasonally wet or subject to flooding. Some are too unstable to be used as a foundation for buildings or roads. Clayey or wet soils are poorly suited to use as septic tank absorption fields. A high water table makes a soil poorly suited to basements or underground installations.

The National Cooperative Soil Survey is a joint effort of the United States Department of Agriculture and other Federal agencies, State agencies including the Agricultural Experiment Stations, and local agencies. The Natural Resources Conservation Service (NRCS) has leadership for the Federal part of the National Cooperative Soil Survey.

Information about soils is updated periodically. Updated information is available through the NRCS Web Soil Survey, the site for official soil survey information.

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How Soil Surveys Are Made

Soil surveys are made to provide information about the soils and miscellaneous areas in a specific area. They include a description of the soils and miscellaneous areas and their location on the landscape and tables that show soil properties and limitations affecting various uses. Soil scientists observed the steepness, length, and shape of the slopes; the general pattern of drainage; the kinds of crops and native plants; and the kinds of bedrock. They observed and described many soil profiles. A soil profile is the sequence of natural layers, or horizons, in a soil. The profile extends from the surface down into the unconsolidated material in which the soil formed or from the surface down to bedrock. The unconsolidated material is devoid of roots and other living organisms and has not been changed by other biological activity.

Currently, soils are mapped according to the boundaries of major land resource areas (MLRAs). MLRAs are geographically associated land resource units that share common characteristics related to physiography, geology, climate, water resources, soils, biological resources, and land uses (USDA, 2006). Soil survey areas typically consist of parts of one or more MLRA.

The soils and miscellaneous areas in a survey area occur in an orderly pattern that is related to the geology, landforms, relief, climate, and natural vegetation of the area. Each kind of soil and miscellaneous area is associated with a particular kind of landform or with a segment of the landform. By observing the soils and miscellaneous areas in the survey area and relating their position to specific segments of the landform, a soil scientist develops a concept, or model, of how they were formed. Thus, during mapping, this model enables the soil scientist to predict with a considerable degree of accuracy the kind of soil or miscellaneous area at a specific location on the landscape.

Commonly, individual soils on the landscape merge into one another as their characteristics gradually change. To construct an accurate soil map, however, soil scientists must determine the boundaries between the soils. They can observe only a limited number of soil profiles. Nevertheless, these observations, supplemented by an understanding of the soil-vegetation-landscape relationship, are sufficient to verify predictions of the kinds of soil in an area and to determine the boundaries.

Soil scientists recorded the characteristics of the soil profiles that they studied. They noted soil color, texture, size and shape of soil aggregates, kind and amount of rock fragments, distribution of plant roots, reaction, and other features that enable them to identify soils. After describing the soils in the survey area and determining their properties, the soil scientists assigned the soils to taxonomic classes (units). Taxonomic classes are concepts. Each taxonomic class has a set of soil characteristics with precisely defined limits. The classes are used as a basis for comparison to classify soils systematically. Soil taxonomy, the system of taxonomic classification used in the United States, is based mainly on the kind and character of soil properties and the arrangement of horizons within the profile. After the soil

scientists classified and named the soils in the survey area, they compared the individual soils with similar soils in the same taxonomic class in other areas so that they could confirm data and assemble additional data based on experience and research.

The objective of soil mapping is not to delineate pure map unit components; the objective is to separate the landscape into landforms or landform segments that have similar use and management requirements. Each map unit is defined by a unique combination of soil components and/or miscellaneous areas in predictable proportions. Some components may be highly contrasting to the other components of the map unit. The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The delineation of such landforms and landform segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, onsite investigation is needed to define and locate the soils and miscellaneous areas.

Soil scientists make many field observations in the process of producing a soil map. The frequency of observation is dependent upon several factors, including scale of mapping, intensity of mapping, design of map units, complexity of the landscape, and experience of the soil scientist. Observations are made to test and refine the soil-landscape model and predictions and to verify the classification of the soils at specific locations. Once the soil-landscape model is refined, a significantly smaller number of measurements of individual soil properties are made and recorded. These measurements may include field measurements, such as those for color, depth to bedrock, and texture, and laboratory measurements, such as those for content of sand, silt, clay, salt, and other components. Properties of each soil typically vary from one point to another across the landscape.

Observations for map unit components are aggregated to develop ranges of characteristics for the components. The aggregated values are presented. Direct measurements do not exist for every property presented for every map unit component. Values for some properties are estimated from combinations of other properties.

While a soil survey is in progress, samples of some of the soils in the area generally are collected for laboratory analyses and for engineering tests. Soil scientists interpret the data from these analyses and tests as well as the field-observed characteristics and the soil properties to determine the expected behavior of the soils under different uses. Interpretations for all of the soils are field tested through observation of the soils in different uses and under different levels of management. Some interpretations are modified to fit local conditions, and some new interpretations are developed to meet local needs. Data are assembled from other sources, such as research information, production records, and field experience of specialists. For example, data on crop yields under defined levels of management are assembled from farm records and from field or plot experiments on the same kinds of soil.

Predictions about soil behavior are based not only on soil properties but also on such variables as climate and biological activity. Soil conditions are predictable over long periods of time, but they are not predictable from year to year. For example, soil scientists can predict with a fairly high degree of accuracy that a given soil will have a high water table within certain depths in most years, but they cannot predict that a high water table will always be at a specific level in the soil on a specific date.

After soil scientists located and identified the significant natural bodies of soil in the survey area, they drew the boundaries of these bodies on aerial photographs and

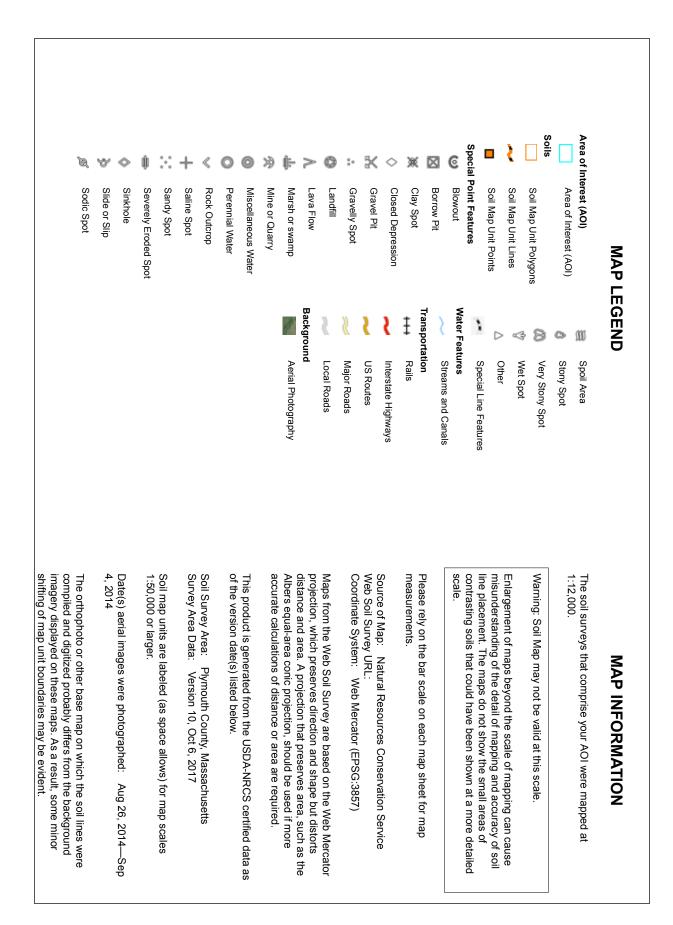
identified each as a specific map unit. Aerial photographs show trees, buildings, fields, roads, and rivers, all of which help in locating boundaries accurately.

Soil Map

The soil map section includes the soil map for the defined area of interest, a list of soil map units on the map and extent of each map unit, and cartographic symbols displayed on the map. Also presented are various metadata about data used to produce the map, and a description of each soil map unit.

Custom Soil Resource Report Soil Map





Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI
37A	Massasoit - Mashpee complex, 0 to 3 percent slopes	9.3	11.2%
253B	Hinckley loamy sand, 3 to 8 percent slopes	53.9	65.4%
253C	Hinckley loamy sand, 8 to 15 percent slopes	3.9	4.8%
253E	Hinckley loamy sand, 15 to 35 percent slopes	1.1	1.3%
255A	Windsor loamy sand, 0 to 3 percent slopes	5.7	6.9%
256B	Deerfield fine sand, 3 to 8 percent slopes	1.2	1.5%
289C	Hinckley gravelly sandy loam, 8 to 15 percent slopes, bouldery	4.8	5.8%
704A	Freetown and Swansea coarse sands, 0 to 3 percent slopes, sanded surface and inactive	2.5	3.0%
Totals for Area of Interest		82.4	100.0%

Map Unit Legend

Map Unit Descriptions

The map units delineated on the detailed soil maps in a soil survey represent the soils or miscellaneous areas in the survey area. The map unit descriptions, along with the maps, can be used to determine the composition and properties of a unit.

A map unit delineation on a soil map represents an area dominated by one or more major kinds of soil or miscellaneous areas. A map unit is identified and named according to the taxonomic classification of the dominant soils. Within a taxonomic class there are precisely defined limits for the properties of the soils. On the landscape, however, the soils are natural phenomena, and they have the characteristic variability of all natural phenomena. Thus, the range of some observed properties may extend beyond the limits defined for a taxonomic class. Areas of soils of a single taxonomic class rarely, if ever, can be mapped without including areas of other taxonomic classes. Consequently, every map unit is made up of the soils or miscellaneous areas for which it is named and some minor components that belong to taxonomic classes other than those of the major soils.

Most minor soils have properties similar to those of the dominant soil or soils in the map unit, and thus they do not affect use and management. These are called noncontrasting, or similar, components. They may or may not be mentioned in a particular map unit description. Other minor components, however, have properties and behavioral characteristics divergent enough to affect use or to require different management. These are called contrasting, or dissimilar, components. They generally are in small areas and could not be mapped separately because of the

scale used. Some small areas of strongly contrasting soils or miscellaneous areas are identified by a special symbol on the maps. If included in the database for a given area, the contrasting minor components are identified in the map unit descriptions along with some characteristics of each. A few areas of minor components may not have been observed, and consequently they are not mentioned in the descriptions, especially where the pattern was so complex that it was impractical to make enough observations to identify all the soils and miscellaneous areas on the landscape.

The presence of minor components in a map unit in no way diminishes the usefulness or accuracy of the data. The objective of mapping is not to delineate pure taxonomic classes but rather to separate the landscape into landforms or landform segments that have similar use and management requirements. The delineation of such segments on the map provides sufficient information for the development of resource plans. If intensive use of small areas is planned, however, onsite investigation is needed to define and locate the soils and miscellaneous areas.

An identifying symbol precedes the map unit name in the map unit descriptions. Each description includes general facts about the unit and gives important soil properties and qualities.

Soils that have profiles that are almost alike make up a *soil series*. Except for differences in texture of the surface layer, all the soils of a series have major horizons that are similar in composition, thickness, and arrangement.

Soils of one series can differ in texture of the surface layer, slope, stoniness, salinity, degree of erosion, and other characteristics that affect their use. On the basis of such differences, a soil series is divided into *soil phases*. Most of the areas shown on the detailed soil maps are phases of soil series. The name of a soil phase commonly indicates a feature that affects use or management. For example, Alpha silt loam, 0 to 2 percent slopes, is a phase of the Alpha series.

Some map units are made up of two or more major soils or miscellaneous areas. These map units are complexes, associations, or undifferentiated groups.

A *complex* consists of two or more soils or miscellaneous areas in such an intricate pattern or in such small areas that they cannot be shown separately on the maps. The pattern and proportion of the soils or miscellaneous areas are somewhat similar in all areas. Alpha-Beta complex, 0 to 6 percent slopes, is an example.

An association is made up of two or more geographically associated soils or miscellaneous areas that are shown as one unit on the maps. Because of present or anticipated uses of the map units in the survey area, it was not considered practical or necessary to map the soils or miscellaneous areas separately. The pattern and relative proportion of the soils or miscellaneous areas are somewhat similar. Alpha-Beta association, 0 to 2 percent slopes, is an example.

An *undifferentiated group* is made up of two or more soils or miscellaneous areas that could be mapped individually but are mapped as one unit because similar interpretations can be made for use and management. The pattern and proportion of the soils or miscellaneous areas in a mapped area are not uniform. An area can be made up of only one of the major soils or miscellaneous areas, or it can be made up of all of them. Alpha and Beta soils, 0 to 2 percent slopes, is an example.

Some surveys include *miscellaneous areas*. Such areas have little or no soil material and support little or no vegetation. Rock outcrop is an example.

Plymouth County, Massachusetts

37A—Massasoit - Mashpee complex, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: bd1q Elevation: 0 to 400 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Massasoit and similar soils: 55 percent Mashpee and similar soils: 35 percent Minor components: 10 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Massasoit

Setting

Landform: Depressions, terraces, drainageways Landform position (two-dimensional): Toeslope, footslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy and gravelly glaciofluvial deposits

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material *Oa - 1 to 3 inches:* highly decomposed plant material *A - 3 to 5 inches:* fine sand *Eg1 - 5 to 11 inches:* fine sand *Eg2 - 11 to 13 inches:* fine sand *Bhs - 13 to 17 inches:* fine sand *Bsm - 17 to 23 inches:* fine sand *Bs - 23 to 26 inches:* fine sand *BC - 26 to 43 inches:* fine sand *Cg - 43 to 80 inches:* loamy very fine sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: 7 to 20 inches to ortstein
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Very low to moderately low (0.00 to 0.01 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: Occasional
Available water storage in profile: Very low (about 1.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w

Hydrologic Soil Group: D *Hydric soil rating:* Yes

Description of Mashpee

Setting

Landform: Depressions, terraces, drainageways Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy and gravelly glaciofluvial deposits

Typical profile

Oe1 - 0 to 2 inches: moderately decomposed plant material Oe2 - 2 to 4 inches: moderately decomposed plant material Oa - 4 to 5 inches: highly decomposed plant material AE - 5 to 7 inches: loamy fine sand Eg - 7 to 11 inches: fine sand Bh1 - 11 to 13 inches: fine sand Bh2 - 13 to 17 inches: fine sand Bs - 17 to 24 inches: loamy fine sand C1 - 24 to 39 inches: fine sand C2 - 39 to 65 inches: fine sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Poorly drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to high (1.42 to 5.95 in/hr)
Depth to water table: About 0 to 12 inches
Frequency of flooding: None
Frequency of ponding: Occasional
Available water storage in profile: Low (about 4.8 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4w Hydrologic Soil Group: A/D Hydric soil rating: Yes

Minor Components

Deerfield

Percent of map unit: 5 percent Landform: Deltas, outwash plains, terraces Landform position (two-dimensional): Footslope, summit Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: No

Rainberry

Percent of map unit: 3 percent Landform: Depressions, kettles

Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: Yes

Squamscott

Percent of map unit: 2 percent Landform: Lake terraces, lake plains Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

253B—Hinckley loamy sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: 2svm8 Elevation: 0 to 1,430 feet Mean annual precipitation: 36 to 53 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 250 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Hinckley and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Hinckley

Setting

- *Landform:* Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas
- Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread. riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Convex, linear, concave

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand

- Bw2 11 to 16 inches: gravelly loamy sand
- BC 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Very low (about 3.0 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3s Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 8 percent

- *Landform:* Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas
- Landform position (two-dimensional): Summit, shoulder, backslope, footslope Landform position (three-dimensional): Nose slope, side slope, base slope, crest,
 - tread, riser
- Down-slope shape: Linear, convex, concave
- Across-slope shape: Convex, linear, concave
- Hydric soil rating: No

Sudbury

Percent of map unit: 5 percent

Landform: Kame terraces, outwash plains, outwash terraces, moraines, outwash deltas

Landform position (two-dimensional): Backslope, footslope

Landform position (three-dimensional): Side slope, base slope, head slope, tread *Down-slope shape:* Concave, linear

Across-slope shape: Linear, concave

Hydric soil rating: No

Agawam

Percent of map unit: 2 percent
Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas
Landform position (two-dimensional): Summit, shoulder, backslope, footslope
Landform position (three-dimensional): Nose slope, side slope, base slope, crest, tread, riser
Down-slope shape: Linear, convex, concave
Across-slope shape: Convex, linear, concave

Hydric soil rating: No

253C—Hinckley loamy sand, 8 to 15 percent slopes

Map Unit Setting

National map unit symbol: 2svm9 Elevation: 0 to 1,480 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Hinckley and similar soils: 85 percent Minor components: 15 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley

Setting

Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas

Landform position (two-dimensional): Shoulder, toeslope, footslope, backslope Landform position (three-dimensional): Crest, head slope, nose slope, side slope, riser

Down-slope shape: Convex, concave, linear

Across-slope shape: Concave, linear, convex

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material

A - 1 to 8 inches: loamy sand

Bw1 - 8 to 11 inches: gravelly loamy sand

Bw2 - 11 to 16 inches: gravelly loamy sand

BC - 16 to 19 inches: very gravelly loamy sand

C - 19 to 65 inches: very gravelly sand

Properties and qualities

Slope: 8 to 15 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 5 percent Landform: Eskers, kames, outwash plains, outwash terraces, moraines Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Side slope, head slope, nose slope, crest, riser Down-slope shape: Convex

Across-slope shape: Convex

Hydric soil rating: No

Windsor

Percent of map unit: 5 percent

Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas

Landform position (two-dimensional): Shoulder, backslope, footslope, toeslope Landform position (three-dimensional): Nose slope, side slope, crest, head slope, riser

Down-slope shape: Convex, concave, linear *Across-slope shape:* Concave, linear, convex *Hydric soil rating:* No

Sudbury

Percent of map unit: 5 percent
Landform: Kame terraces, outwash plains, outwash terraces, moraines, outwash deltas
Landform position (two-dimensional): Backslope, footslope
Landform position (three-dimensional): Base slope, tread
Down-slope shape: Concave, linear
Across-slope shape: Linear, concave
Hydric soil rating: No

253E—Hinckley loamy sand, 15 to 35 percent slopes

Map Unit Setting

National map unit symbol: 2svmd Elevation: 0 to 860 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Hinckley and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Hinckley

Setting

Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces, moraines, outwash deltas

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Crest, nose slope, side slope, head slope, riser

Down-slope shape: Linear, convex, concave

Across-slope shape: Linear, concave, convex

Parent material: Sandy and gravelly glaciofluvial deposits derived from gneiss and/or granite and/or schist

Typical profile

Oe - 0 to 1 inches: moderately decomposed plant material *A - 1 to 8 inches:* loamy sand *Bw1 - 8 to 11 inches:* gravelly loamy sand *Bw2 - 11 to 16 inches:* gravelly loamy sand *BC - 16 to 19 inches:* very gravelly loamy sand *C - 19 to 65 inches:* very gravelly sand

Properties and qualities

Slope: 15 to 35 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Very low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 6e Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Windsor

Percent of map unit: 10 percent

Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces,

moraines, outwash deltas

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Crest, nose slope, side slope, head slope, riser

Down-slope shape: Concave, convex, linear

Across-slope shape: Linear, concave, convex

Hydric soil rating: No

Merrimac

Percent of map unit: 3 percent

Landform: Eskers, kames, kame terraces, outwash plains, outwash terraces,

moraines

Landform position (two-dimensional): Backslope

Landform position (three-dimensional): Side slope, head slope, nose slope, crest, riser

Down-slope shape: Convex, linear, concave

Across-slope shape: Linear, convex, concave

Hydric soil rating: No

Sudbury

Percent of map unit: 2 percent
Landform: Kame terraces, outwash plains, outwash terraces, moraines, outwash deltas
Landform position (two-dimensional): Backslope, footslope, toeslope
Landform position (three-dimensional): Base slope, tread
Down-slope shape: Linear, concave
Across-slope shape: Concave, linear
Hydric soil rating: No

255A—Windsor loamy sand, 0 to 3 percent slopes

Map Unit Setting

National map unit symbol: 2svkg Elevation: 0 to 990 feet Mean annual precipitation: 36 to 71 inches Mean annual air temperature: 39 to 55 degrees F Frost-free period: 140 to 240 days Farmland classification: Farmland of statewide importance

Map Unit Composition

Windsor, loamy sand, and similar soils: 85 percent *Minor components:* 15 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Windsor, Loamy Sand

Setting

Landform: Deltas, dunes, outwash plains, outwash terraces Landform position (three-dimensional): Riser, tread Down-slope shape: Linear, convex Across-slope shape: Linear, convex Parent material: Loose sandy glaciofluvial deposits derived from granite and/or

loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from schist and/or loose sandy glaciofluvial deposits derived from gneiss

Typical profile

O - 0 to 1 inches: moderately decomposed plant material

A - 1 to 3 inches: loamy sand

Bw - 3 to 25 inches: loamy sand

C - 25 to 65 inches: sand

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 99.90 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Salinity, maximum in profile: Nonsaline (0.0 to 1.9 mmhos/cm)
Available water storage in profile: Low (about 3.6 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 2s Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Deerfield, loamy sand

Percent of map unit: 10 percent Landform: Deltas, outwash plains, terraces Landform position (two-dimensional): Footslope Landform position (three-dimensional): Tread, talf Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: No

Hinckley, loamy sand

Percent of map unit: 5 percent Landform: Deltas, eskers, kames, outwash plains Landform position (two-dimensional): Summit, shoulder, backslope Landform position (three-dimensional): Nose slope, side slope, crest, head slope, rise Down-slope shape: Convex Across-slope shape: Convex, linear Hydric soil rating: No

256B—Deerfield fine sand, 3 to 8 percent slopes

Map Unit Setting

National map unit symbol: bcwx Elevation: 0 to 400 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F *Frost-free period:* 145 to 240 days *Farmland classification:* Farmland of statewide importance

Map Unit Composition

Deerfield and similar soils: 80 percent Minor components: 20 percent Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Deerfield

Setting

Landform: Deltas, outwash plains, terraces Landform position (two-dimensional): Footslope, shoulder Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave Parent material: Sandy and gravelly glaciofluvial deposits

Typical profile

Oi - 0 to 1 inches: slightly decomposed plant material *Oe - 1 to 2 inches:* moderately decomposed plant material *Oa - 2 to 3 inches:* highly decomposed plant material *E1 - 3 to 5 inches:* fine sand *E2 - 5 to 8 inches:* fine sand *Bs - 8 to 11 inches:* fine sand *Bw1 - 11 to 15 inches:* fine sand *Bw2 - 15 to 20 inches:* fine sand *BC - 20 to 26 inches:* fine sand *C1 - 26 to 39 inches:* fine sand *C2 - 39 to 61 inches:* fine sand

Properties and qualities

Slope: 3 to 8 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Moderately well drained
Runoff class: Very high
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 14.17 in/hr)
Depth to water table: About 18 to 36 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Low (about 4.1 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 3w Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 4 percent Landform: Kames, outwash plains, terraces Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Carver

Percent of map unit: 4 percent Landform: Outwash plains, moraines, pitted outwash plains Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Tread Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Mashpee

Percent of map unit: 4 percent Landform: Depressions, terraces, drainageways Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Massasoit

Percent of map unit: 4 percent Landform: Depressions, terraces, drainageways Landform position (two-dimensional): Footslope, toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Concave Hydric soil rating: Yes

Sudbury

Percent of map unit: 4 percent Landform: Depressions, outwash plains, terraces Landform position (two-dimensional): Footslope, shoulder Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Concave Hydric soil rating: No

289C—Hinckley gravelly sandy loam, 8 to 15 percent slopes, bouldery

Map Unit Setting

National map unit symbol: bd1l Elevation: 0 to 400 feet Mean annual precipitation: 41 to 54 inches Mean annual air temperature: 43 to 54 degrees F Frost-free period: 145 to 240 days Farmland classification: Not prime farmland

Map Unit Composition

Hinckley, bouldery, and similar soils: 80 percent

Minor components: 20 percent

Estimates are based on observations, descriptions, and transects of the mapunit.

Description of Hinckley, Bouldery

Setting

Landform: Eskers, kames, terraces, outwash deltas Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Riser Down-slope shape: Linear Across-slope shape: Convex Parent material: Sandy and gravelly glaciofluvial deposits

Typical profile

Oe - 0 to 2 inches: moderately decomposed plant material

A - 2 to 3 inches: gravelly sandy loam

Bw - 3 to 19 inches: very gravelly loamy coarse sand

C1 - 19 to 33 inches: very gravelly coarse sand

C2 - 33 to 60 inches: very gravelly coarse sand

Properties and qualities

Slope: 8 to 15 percent
Percent of area covered with surface fragments: 0.1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Excessively drained
Runoff class: Low
Capacity of the most limiting layer to transmit water (Ksat): Moderately high to very high (1.42 to 28.34 in/hr)
Depth to water table: More than 80 inches
Frequency of flooding: None
Frequency of ponding: None
Available water storage in profile: Very low (about 1.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 4e Hydrologic Soil Group: A Hydric soil rating: No

Minor Components

Merrimac

Percent of map unit: 10 percent Landform: Kames, outwash plains, terraces Landform position (two-dimensional): Shoulder, backslope Landform position (three-dimensional): Riser Down-slope shape: Linear Across-slope shape: Convex Hydric soil rating: No

Gloucester, bouldery

Percent of map unit: 7 percent Landform: Ground moraines, hills Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

Barnstable, bouldery

Percent of map unit: 3 percent Landform: Moraines Landform position (two-dimensional): Summit, shoulder Landform position (three-dimensional): Interfluve Down-slope shape: Convex Across-slope shape: Convex Hydric soil rating: No

704A—Freetown and Swansea coarse sands, 0 to 3 percent slopes, sanded surface and inactive

Map Unit Setting

National map unit symbol: 2tx05 Elevation: 0 to 140 feet Mean annual precipitation: 40 to 52 inches Mean annual air temperature: 48 to 55 degrees F Frost-free period: 190 to 250 days Farmland classification: Farmland of unique importance

Map Unit Composition

Freetown, sanded surface, inactive, and similar soils: 45 percent *Swansea, sanded surface, inactive, and similar soils:* 45 percent *Minor components:* 10 percent *Estimates are based on observations, descriptions, and transects of the mapunit.*

Description of Freetown, Sanded Surface, Inactive

Setting

Landform: Bogs, depressions, kettles Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Concave Parent material: Sandy human transported material over organic material

Typical profile

^*Ap - 0 to 15 inches:* coarse sand 20*a - 15 to 79 inches:* muck

Properties and qualities

Slope: 0 to 3 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Frequent

Frequency of ponding: None *Available water storage in profile:* Very high (about 20.9 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: B/D Hydric soil rating: Yes

Description of Swansea, Sanded Surface, Inactive

Setting

Landform: Bogs, depressions, kettles Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Talf Down-slope shape: Concave Across-slope shape: Concave Parent material: Highly decomposed organic material over loose sandy and gravelly glaciofluvial deposits

Typical profile

[^]Ap - 0 to 15 inches: coarse sand Oa - 15 to 36 inches: muck 2Cg - 36 to 79 inches: coarse sand

Properties and qualities

Slope: 0 to 1 percent
Depth to restrictive feature: More than 80 inches
Natural drainage class: Very poorly drained
Runoff class: Negligible
Capacity of the most limiting layer to transmit water (Ksat): Moderately low to high (0.14 to 14.17 in/hr)
Depth to water table: About 0 to 6 inches
Frequency of flooding: Rare
Frequency of ponding: Frequent
Available water storage in profile: High (about 11.3 inches)

Interpretive groups

Land capability classification (irrigated): None specified Land capability classification (nonirrigated): 5w Hydrologic Soil Group: B/D Hydric soil rating: Yes

Minor Components

Rainberry, sanded surface

Percent of map unit: 5 percent Landform: Depressions, kettles Landform position (two-dimensional): Toeslope Landform position (three-dimensional): Tread Down-slope shape: Concave Across-slope shape: Linear Hydric soil rating: Yes

Tihonet

Percent of map unit: 5 percent Landform: Outwash plains Landform position (two-dimensional): Toeslope

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Landform position (three-dimensional): Tread Down-slope shape: Linear Across-slope shape: Linear Hydric soil rating: Yes

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